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SEPTEMBER 1955

# RADIO-ELECTRONICS

TELEVISION · SERVICING · HIGH FIDELITY

HUGO GERNSBACK, Editor

In this issue:

Tube-and-Transistor Radio

More Efficiency with Multiple Speakers

More on the Color Matrix

Demodulator Probe with Transistor

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Scientific Record
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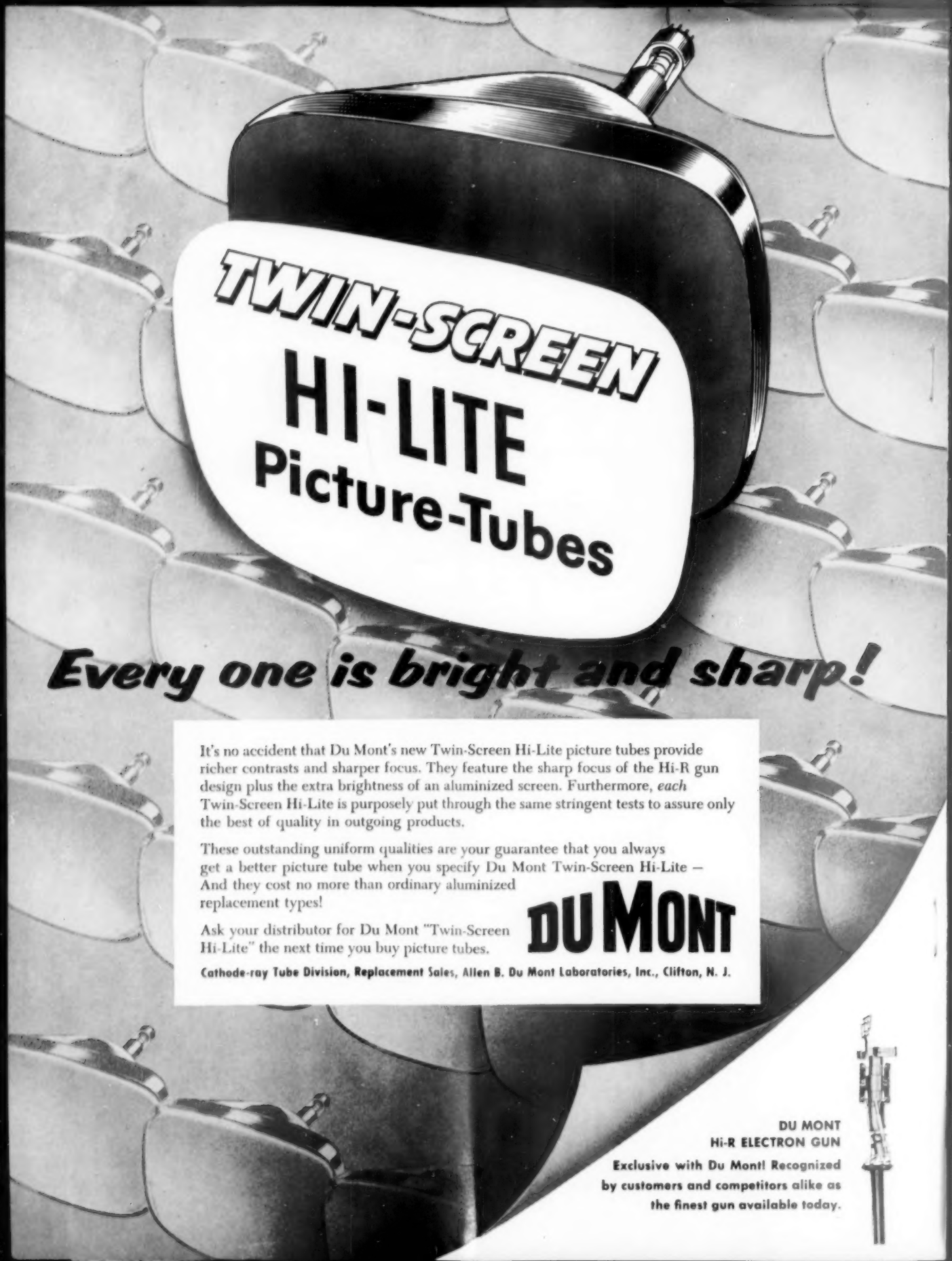


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ON THE COVER:

(Story on page 64) Oceanographer Marie Poland Fish records the sounds made by a deep-water fish, at the Narragansett Marine Laboratory in Kingston, R. I.

*Color original by Dan Rubin*

**SEPTEMBER 1955** **Vol. XXVI, No. 9**

**Editorial (Page 33)**

The Giant Electronics Industry ..... 33

**Radio (Pages 34–43)**

Making Printed Circuits Is Easy ..... by Tom Jaski 34
Common-Collector Transistor Amplifiers ..... by Rufus P. Turner 37
Flexible Radio Control System, Part II—
The radio receiver and control system ..... by Richard H. Dorf 38
Contact Potential ..... by H. P. Manly 41
Tube and Transistor Radio ..... by Irving Gottlieb 42
A.C. Voltbox ..... by Rufus Turner 43

**Test Instruments (Pages 44–50)**

New Test for Capacitor Leakage ..... by Robert G. Middleton 44
Transistor Demodulator Probe ..... by Homer L. Davidson 47
Transistor Performance ..... by Edward D. Padgett 48

**Television (Pages 51–63)**

Convergence . . . Not Impossible but Difficult,
Part I—Rainbows in black-and-white picture;
author suspects convergence troubles ..... by Harold Davis 51
More on the Matrix ..... by Robert G. Middleton 53
Television . . . it's a Cinch, Eighteenth conversation, first half:
The trichromatic principle; transmission problems;
simultaneous or sequential; saving the fine detail;
how to carry the color inside the 6-mc band ..... by E. Aisberg 56
Converting 630 Receivers to Intercarrier Operation ..... by Howard Bierman 59
TV Service Clinic ..... Conducted by Jerry Kass 62

**Audio—High Fidelity (Pages 64-108)**

Noisy Fishes (Cover Feature) ..... by Eric Leslie 64
Transplanting Amplifiers ..... by Charles L. Hansen 65
Circuit Features in Hi-Fi Power Amplifiers ..... by Robert F. Scott 79
For Golden Ears Only: National's Criterion FM-AM tuner;
Heathkit audio analyzer; new records review ..... by Monitor 84
Designing an Ultra-Linear Amplifier ..... by Edward S. Miller 92
Multiple Speakers for High Fidelity ..... by Joseph Marshall 100

**Electronics (Pages 112–129)**

Boat Electrolysis ..... by Elbert Robberson 112
Giant Paraboloid Detects Radio Stars ..... by R. Hanbury Brown 120

**DEPARTMENTS**

| | | | |
|---|---|---|---|
| Books | 162 | People | 154 |
| Business | 157 | Question Box | 142 |
| Corrections | 156, 161 | Radio Month | 6 |
| Correspondence | 14 | Radio-Electronics Circuits | 139 |
| Miscellany | 151 | Technical Literature | 161 |
| New Devices | 132 | Technicians' News | 147 |
| New Tubes and Transistors | 137 | Technotes | 145 |
| Patents | 149 | Try This One | 152 |

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# the Radio month

**TV STATION SATURATION** in the U. S. was placed at 673 by CBS researchers. This includes the approximately 430 stations now in operation as well as prospective ones that now possess construction permits or have applications on file before the FCC. CBS says this is due to economic limitations, the high cost of installation and operation making it too costly to function in small towns and sparsely settled areas. This adds up to an expectancy of fewer than 250 more stations.

**TRANSISTORIZED** phonograph has been demonstrated recently by Philco. The unit, using three transistors, will play up to 3,000 standard 45-r.p.m. records using the power supplied by 4 flashlight cells. Because of the extremely low current drain, 150 hours of continuous operation are possible. Fresh cells can be quickly inserted through a trapdoor at the bottom of the cabinet.

The phonograph uses the smallest turntable motor on the market, a 4-volt unit weighing less than 3 ounces and approximately one-fifth the size of a conventional motor. A printed wire chassis is used (see photo) and the tone arm acts as the on–off switch, stopping the turntable and turning off the phonograph after each record.

This transistorized phonograph follows shortly the Philco announcement of a transistorized auto radio (Radio Month, July, 1955).

**PROJECT TINKERTOY,** code name for a system of automatic mass production of electronic devices (RADIO-ELECTRONICS December, 1953) developed jointly by the Navy Bureau of Aeronautics and the National Bureau of Standards about 2 years ago, will shortly make its appearance in Du Mont TV receivers. The Compac module made by A. C. F. Industries, Alexandria, Va., is presently undergoing engineering tests at Du Mont. A. C. F. says its module is of a stacked wafer design and will, as a single unit, replace about two-thirds of the components within a TV set at about the same cost.

**ELECTRONIC FISHING** aid has been invented in Japan that has the professional fishermen agog. The device, based on the theory that an underwater radio beam will be followed to its source by fish, consists of a small "radio-beam generator" in the center of a large Y-shaped net.

Professor Ando of Ehime University, Japan, inventor of the unit, said its first tryout was highly successful, "We just dropped the net into the water and the fish swam into it in droves."

**The Philco transistorized phonograph—component parts are shown at right.**

As always, Electro-Voice is FIRST! Now E-V sponsors this unique and exciting contest. For a lifetime after this glorious listening experience you will judge music reproduction equipment by its ability to approach the perfection already achieved by E-V sound matched high fidelity components and loudspeaker systems!

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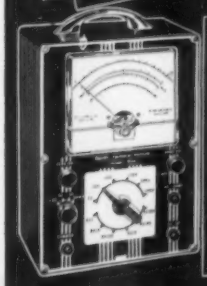

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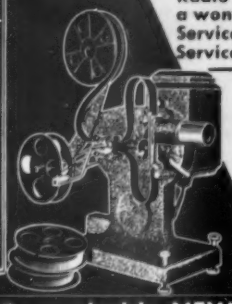

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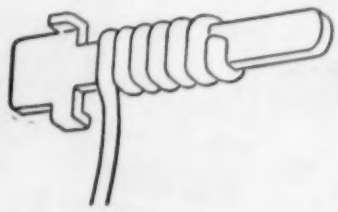
**SOLDERLESS CONNECTIONS** are being used in current RCA television chassis. The connections consist of six or seven turns of wire tightly wrapped on a "stake" or terminal (see diagram). The wire is wrapped with a power tool similar to an electric hand drill. The machine spins the wire on the terminal



with such force that the corners of the terminal bite into the copper wire, forming a positive contact held in place by the tension of the many turns of wire.

These connections are used in many locations in the receiver, but most frequently on the printed-circuit boards. RCA recommends that should this wire-wrap joint be disconnected, it should be reconnected by soldering, not by rewrapping. The wrapped connection is said to be mechanically and electrically equal to soldered connections.

**EDUCATIONAL TV AUDIENCE** will reach almost 46 million when the 13 educational television stations now under construction are completed. This estimate is based on a survey conducted by the National Citizens Committee for Educational Television. About 100 additional cities have shown sufficient interest in educational TV to appoint ways and means committees.

Of the new stations under construction, 6 are community type, owned and operated by nonprofit corporations; 3 will be under the control of educational institutions and 4 will become part of state networks.

Of the 13 stations under construction, 11 will be v.h.f., the other 2 u.h.f. At present, there are 13 educational TV stations on the air; 10 are v.h.f. and 3 are u.h.f.

**TV ON ASIATIC MAINLAND** has swung into action as a powerful supporter of freedom in Asia. The station, located in Bangkok, Thailand, is the first of its kind on the Asia mainland (Japan and the Philippine Islands have TV) and is a Government-sponsored agency known as the Thai Television Co. The Government plans to use TV as a mass-scale education medium.

As announced by Meade Brunet, managing director of the RCA International Division, more than a year ago the Thai Government sent seven Thai engineers to the United States for training with RCA Institutes and the National Broadcasting Co. The Asian station uses modern apparatus, including the latest type RCA 11-kw transmitter, and mobile TV unit for remote telecasts.

**TWO NEW TV STATIONS** began operation and one left the air since last month's report. KRNT-TV, Des Moines, Iowa, began operation June 20, on channel 8. A new Canadian starter, CBOFT, channel 9, Ottawa, Ont., is the only North American station with an unhyphenated five-letter call. It will broadcast in French exclusively.

The station leaving the air is WNET, Providence, R. I., channel 16.

WWLP, Springfield, Mass., changed frequency from channel 61 to channel 22 on July 2.

**VERSATILITY** is the design keynote of a transistorized portable radio demonstrated by Capehart-Farnsworth. The tiny unit, no larger than a pack of king-size cigarettes and weighing only 6.4 ounces, can be operated with a miniature earphone, with a matching speaker about its own size, or installed in an ashtray base with a larger speaker (see photo) and powered by a.c. When used with the "ashtray speaker," the volume and sensitivity compare with that of a five-tube radio.

**RADAR SPEED CHECK** has been held admissible in court. In a recent decision by the New Jersey Supreme Court against a bus company, the jurists ruled that evidence of speeding obtained by properly operated radar equipment may be used in court and "may readily support a finding of guilt."

Attorneys for the bus company argued that a recording device attached to the bus showed the speed limit was not exceeded, and that the radar equipment was not calibrated properly.

**FLOATING TV STATION** is the plan of television experts and businessmen for providing video signals for South Africa's four biggest ports. Operated 3 miles offshore, in international waters, the sea-going transmitter will beam programs to Durban, Capetown, Port Elizabeth and East London.

A member of the group planning the project said that it has been proved in the United States that an independent TV station can be an economical proposition in a city with about 50,000 inhabitants. He said further, "Such a station could give excellent service to any of the four cities in turn, and two 'floating stations' could give each of these ports a daily service.

"Operating 3 miles out to sea would also do away with a number of technical difficulties, for there would be no mountains or other such obstacles." END

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| A/1C Ronald H. Person<br>St. Louis 20, Mo. | 1st | 25 weeks |
| Carl Verboomen<br>Wrightstown, Wis. | 1st | 18 weeks |
| Marvin F. Kimball<br>Lafeyette, Ind. | 2nd | 21 weeks |
| L. M. Bonino<br>Harlingen AFB, Tex. | 2nd | 16 weeks |
| John E. Hutchison<br>Bluefield, W. Va. | 1st | 27 weeks |

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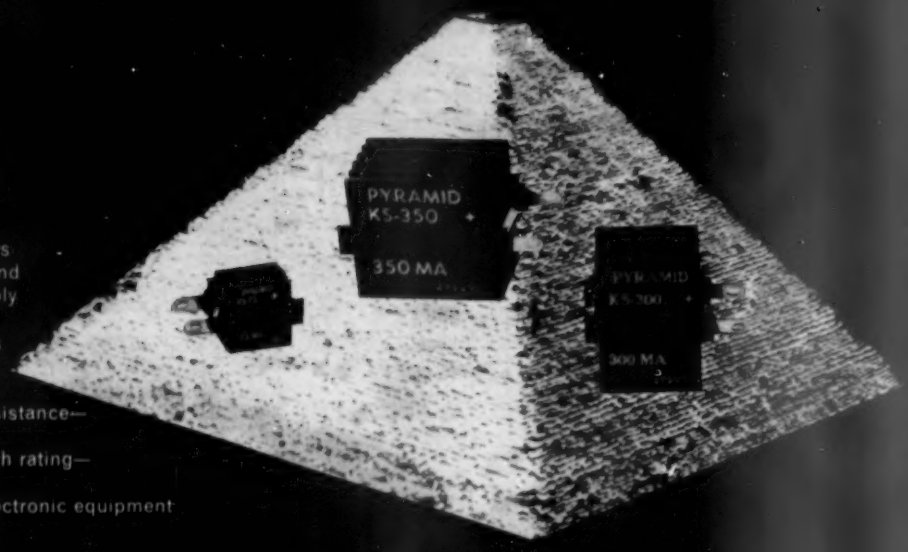


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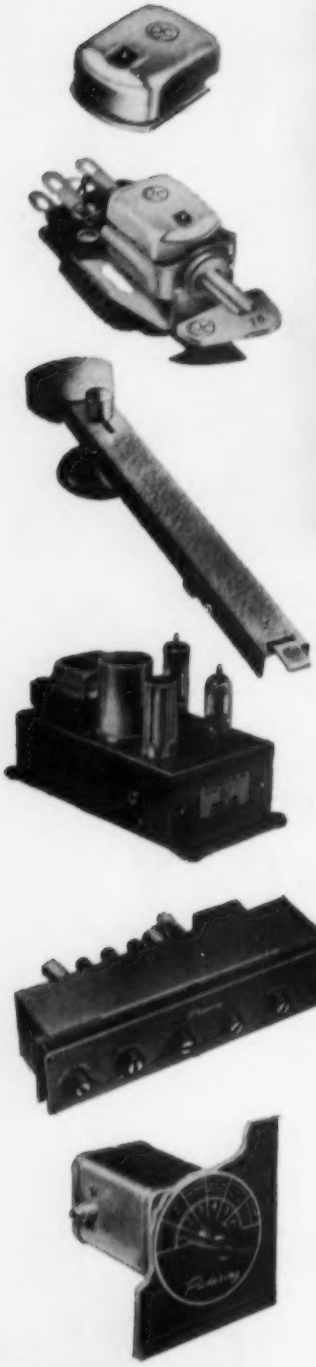

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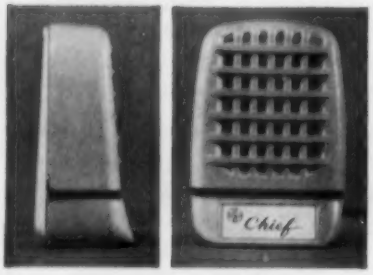


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# Correspondence

### AUTHOR'S ALTERATIONS

*Dear Editor:*

In answering readers' letters concerning my article "Improving Low-Priced Tape Recorders" (April, May), I came across the question as to whether I made changes other than those disclosed in the article. I did recently obtain a considerable reduction in hum (6 db or better) by disconnecting the heater center tap from ground and connecting one side of the heater to 70 volts d.c., obtained at the junction of 47,000-ohm resistor and the 15-μf capacitor supplying plate and screen current to the playback 6AU6. Try each side of the heater supply to see which gives better results. I had previously tried d.c. heater bias but had given it up because of the frying noises. This used a voltage divider constructed for the purpose, but my later effort requires nothing more than a piece of wire for satisfactory results.

HERMAN BURSTEIN

*Wantagh, N. Y.*

### FIRE INSURANCE

*Dear Editor:*

I recently suffered a heavy financial loss as a result of a fire in my home. My radio-TV repair shop, which was in my home, was completely destroyed. The contents of my shop—Rider manuals 1 to 14, Photofact folders 1 to 205, RADIO-CRAFT magazines from 1932 to the present issue of RADIO-ELECTRONICS, several hundred dollars' worth of service data and reference books on radio and television, a complete set of test equipment, welding equipment and a complete set of radio and woodworking tools—were worth about $6,000. Only about $2,500 of this loss is recoverable by insurance.

I'm telling you all this for a purpose. Possibly you'd write an article on insurance that would save someone else the headaches I am experiencing. *No one ever carries enough insurance.* It took everything I had to replace the TV sets that were in the shop for repair.

V. K. VANCE

*Little Rock, Ark.*

(The above seems to us one of the most effective "articles" that could be written.—*Editor*)

### TECHNICAL EDUCATION

*Dear Editor:*

I would like to comment on the letter by E. I. Eastwood on technical education, appearing in the May Correspondence column. Perhaps some of us read-


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The popular Royal 8—your best value in a hi-fi speaker. Outperforms many larger speakers. Features a slotted, treated, blue cone; high-flux, slug-type magnet; clean reproduction of audio range.

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ers may misinterpret Mr. Eastwood's idea of the term "technical education" or the opportunities it might offer to various age brackets.

Where the paths of Mr. Eastwood and I divided was when I enrolled in a technical trade school and for a sum somewhat in excess of $100 received a very thorough radio, TV and electronics course. Not content, I recently enrolled in another school to study television servicing exclusively.

I, too, am a family man with two youngsters to look out for, but I was willing to gamble over $300 and almost all my evenings for the future.

KENNETH C. BUSH

*Buffalo, N. Y.*

## THE WHY OF THE SUBJECT

*Dear Editor:*

I found the article "How Much Will a Resistor Take" (July, 1955) by H. P. Manly very thought-provoking. The author gets at the *why* of the subject.

Entirely too many technicians of my acquaintance find themselves completely helpless to cope with a service problem unless someone can supply them with the schematic with all values shown. They simply have never learned the *why*. They consider Ohm's law to be some sort of obscure legislation, not to mention the many useful equations directly or indirectly based upon it.

Mr. Manly has supplied a very handy graph. If the technician knows Ohm's law, he can also use the graph to find how much voltage can be dropped across a given resistor without exceeding the wattage rating ($E = IR$).

H. B. CONANT

*Conant Laboratories*
*Lincoln, Neb.*

## TUBE TESTER

*Dear Editor:*

There is described on page 47 of the April issue of RADIO-ELECTRONICS "A Laboratory Type Tube Tester." The author states in the first paragraph, which I quote in part, "transconductance is read directly by applying a *1-volt r.m.s.* signal on the grid and measuring the output in a.c. milliamperes."

With a grid signal of this magnitude, the a.c. output current will be a measure of the average transconductance over a grid swing of 2.828 volts peak to peak. This may cause a discrepancy between the measured transconductance and the transconductance values which appear in the published ratings as found, for example, in tube manuals. The grid signal used for obtaining the published values is 10 millivolts, and the instrument used is a General Radio vacuum-tube bridge.

This discrepancy between published and measured transconductance values may be the cause for rejection of good tubes in the field by persons who are not aware of the differing measurement conditions.

G. L. QUINT

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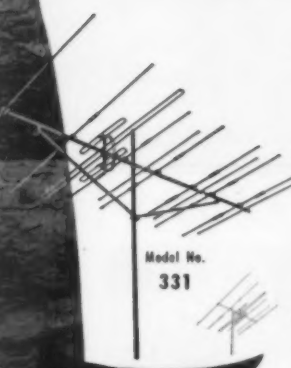


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## Extra elements, extra performance!

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## Advanced design — and "Super-Sembled"

Look to the LANCERS for Channel Master "extras": extra elements and extra gain — at no extra cost. Completely "Super-Sembled." The SUPER LANCER gives 1½ db more gain on both the Low Band and the High Band than similar types. The LANCER, Model No. 333, has an extra director that provides 1½ db more Low Band gain. Count the elements . . . then compare the prices!

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# CABINART '56

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MODEL 11
MODEL 21
MODEL 22
MODEL 27 ●
MODEL 28 ●
MODEL 27U ●
MODEL 28U ●
MODEL 65 ●
MODEL 70
MODEL 7112
MODEL 7115
MODEL 90
MODEL 91
MODEL 90U
MODEL 91U
MODEL 800 ●
MODEL 800U ●
MODEL KR-3
MODEL KR-3U
MODEL KR-4-12
MODEL KR-4-15
MODEL KR-5
MODEL KR-5-U
MODEL KR-5-P
MODEL ST-1 ●
MODEL ST-2 ●
MODEL ST-3 ●
MODEL ST-4 ●
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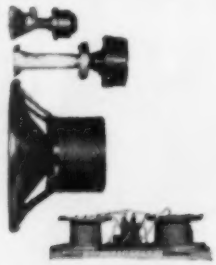

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THE Rebel 4 SPEAKERS

THE Rebel 5 SPEAKERS

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KIT K-4-12
KIT K-4-15
KIT KST-1 ●
KIT KST-2 ●
KIT KST-3 ●
KIT KST-4 ●
KIT KST-5 ●
KIT KST-6 ●
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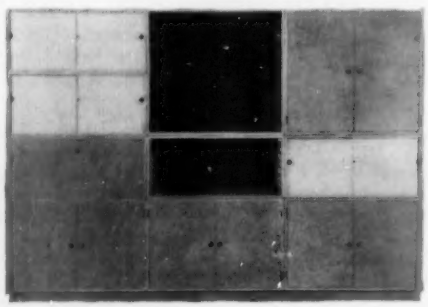
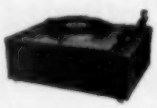
MODEL 27K
MODEL 28K

• TWELVE NEW HI-FI KITS



. . . EVEN A HI-FI STORAGEWALL

ACC-1
ACC-2
ACC-2U
ACC-3
ACC-4
ACC-5
ACC-6
ACC-7
ACC-7A



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National Radio
Institute
Washington, D.C.
40 years of success
training men at
home in spare time.

# I Will Train You at Home
## *for Good Pay Jobs, Success in*
# RADIO-TELEVISION

## Practice Broadcasting with Equipment I Send

It's practical to train at home for good Radio-TV jobs and a brighter future. As part of my Communications Course I send you kits of parts to build the low-power Broadcasting Transmitter shown at the left. You use it to get practical experience performing procedures demanded of Broadcasting Station Operators. An FCC Commercial Operator's License can be your ticket to a better job and a bright future; my Communications Course gives you the training you need to get your license. Mail card below and see in my book other valuable equipment you build. Get FREE sample lesson.

## Practice Servicing with Equipment I Send

Self-confidence, security, earning power come from knowing-how and from experience. Nothing takes the place of PRACTICAL EXPERIENCE. That's why NRI training is based on LEARNING BY DOING. You use parts I furnish to build many circuits common to Radio and Television. With my Servicing Course you build a modern Radio (shown at right). You build a Multitester, use it in conducting experiments, fixing sets in spare time starting a few months after enrolling. All equipment is yours to keep. Card below will bring book showing other equipment you build. Judge for yourself whether you can learn at home in your spare time.

## Television Is Growing Fast Making New Jobs, Prosperity

More than 30 million homes now have Television sets and thousands more are being sold every week. Well trained men are needed to make, install, service TV sets and to operate hundreds of Television stations. Think of the good job opportunities here for qualified technicians, operators, etc. If you're looking for opportunity, get started now learning Radio-Television at home in spare time. Cut out and mail postage-free card. J. E. Smith, President, National Radio Institute, Washington, D. C. Over 40 years' experience training men at home.

AVAILABLE TO VETERANS UNDER G.I. BILL

Good Jobs Good Pay **See Other Side**

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This card entitles you to Actual Lesson on Servicing, shows how you learn Radio-Television at home. You'll also receive my 64-page Book, "How to Be a Success in Radio-Television." Mail card now!

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**National Radio Institute, Washington 9, D. C.**

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VETS write in date of discharge .....

K L M O P R S T U W

# Train at Home to Jump Your Pay as a RADIO-TV Technician

**J. E. Smith, *President***
**National Radio Institute**

The men whose messages are published below were not born successful. Not so long ago they were doing exactly as you are now . . . reading my ad! They decided they should KNOW MORE . . . so they could EARN MORE . . . so they acted! Mail card below now.

## Get a Better Job—Be Ready for a Brighter Future in America's Fast Growing Industry

Training PLUS opportunity is the PERFECT COMBINATION for job security, good pay, advancement. When times are good, the trained man makes the BETTER PAY, GETS PROMOTED. When jobs are scarce, the trained man enjoys GREATER SECURITY. NRI training can help assure more of the better things of life.

Radio-Television is today's opportunity field. Even without Television, Radio is bigger than ever before. Over 3,000 Radio Broadcasting Stations on the air; more than 115 million home and Automobile Radios are in use. Television Broadcast Stations extend from coast to coast now with over 30 million Television sets already in use. Over 400 Television stations are on the air and there are channels for hundreds more. Use of Aviation and Police Radio, Micro-Wave Relay, Two-way Radio communication for buses, taxis, trucks, etc., is expanding. New uses for Radio-Television principles coming in Industry, Government, Communications and Homes.

## My Training Is Up-to-Date You Learn by Doing

Get the benefit of our 40 years' experience training men. My well-illustrated lessons give you the basic principles you must have to assure continued success. Skillfully developed kits of parts I furnish "bring to life" the principles you learn from my lessons. Read more about equipment you get on other side of this page.

More and more Television information is being added to my courses. The equipment I furnish students gives experience on circuits common to BOTH Radio and Television.

## Find Out About this Tested Way to Better Pay

Read at the right how fellows who acted to get the better things of life are making out now. Read how NRI students earn $10, $15 a week extra fixing Radios in spare time starting soon after enrolling. Read how my graduates start their own businesses. Then take the next step—mail card below.

You take absolutely no risk. I even pay postage. I want to put an Actual Lesson in your hands to prove NRI home training is practical, thorough. I want you to see my 64-page book, "How to Be a Success in Radio-Television," because it tells you about my 40 years of training men and important facts about present and future Radio-Television job opportunities. You can take NRI training for as little as $5 a month. Many graduates make more than the total cost of my training in two weeks. Mailing postage-free card can be an important step in becoming successful. J. E. Smith, President, National Radio Institute, Washington 9, D. C. Training Men for Over 40 years. Approved Member, National Home Study Council.

## Start Soon to Make $10 to $15 a Week Extra Fixing Sets

Keep your job while training. Many NRI students make $10, $15 and more a week extra fixing neighbors' Radios in spare time, starting a few months after enrolling. The day you enroll I start sending you special booklets that show you how to fix sets. The multitester you build with parts I furnish helps discover and correct troubles.

SEE OTHER SIDE

## I TRAINED THESE MEN

**Lots of Spare-Time Jobs**

"I do a lot of spare-time Radio and TV servicing. It was fun learning and I don't know how to thank you." B. Goede, Plainview, Minn.

**Now TV Trouble Shooter**

"I had only gone to 7th grade when I started course. Now have job as TV trouble shooter, also fix sets spare time." M. R. Lindemuth, Fort Wayne, Ind.

**Engineer with WHPE**

"Thanks to NRI, I operated a successful Radio repair store. Then I got a job with WPAQ and now am an engineer for WHPE." V. W. Workman, High Point, N. C.

**NRI Course Can't Be Beat**

"Am with WCOC. NRI Course can't be beat. No trouble passing 1st class Radiophone license examination." Jesse W. Parker, Meridian, Mississippi.

**Quit Job for Own Business**

"I decided to quit my job and do TV work full time. I love my work and am doing all right financially." William F. Kline, Cincinnati, Ohio.

**Extra Money In Spare Time**

"I am a police captain and also have good spare-time service business. Just opened my new showrooms and shop." C. W. Lewis, Pensacola, Fla.

## My Training Leads to Jobs Like These

**BROADCASTING:** Chief Technician, Chief Operator, Power Monitor, Recording Operator, Remote Control Operator. **SERVICING:** Home and Auto Radios, P.A. Systems, Television Receivers, Electronic Controls, FM Radios. **IN RADIO PLANTS:** Design Assistant, Transmitter Design Technician, Service Manager, Tester, Serviceman, Research Assistant. **SHIP AND HARBOR RADIO:** Chief Operator, Assistant Operator, Radiotelephone Operator. **GOVERNMENT RADIO:** Operator in Army, Navy, Marine Corps, Coast Guard, Forestry Service Dispatcher, Airways Radio Operator. **AVIATION RADIO:** Plane Radio Operator, Transmitter Technician, Receiver Technician, Airport Transmitter Operator. **TELEVISION:** Pick-Up Operator, Voice Transmitter Operator, Television Technician, Remote Control Operator, Service and Maintenance Technician. **POLICE RADIO:** Transmitter Operator, Receiver Serviceman.

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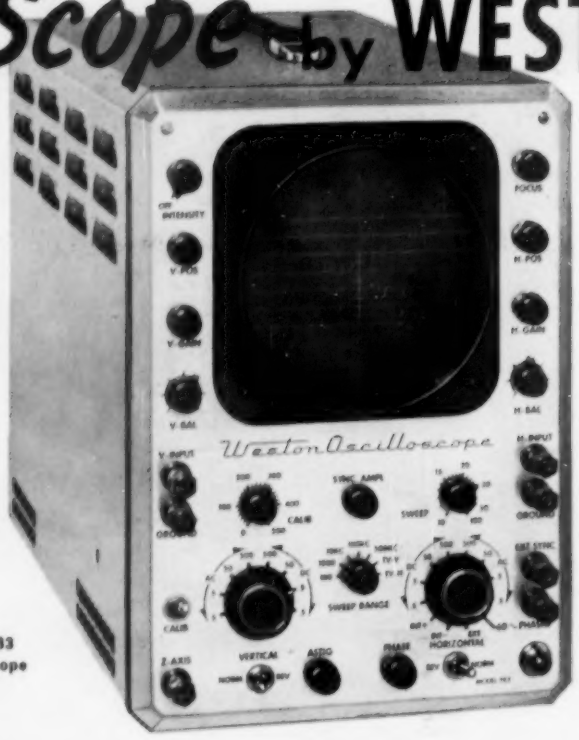



Weston
Model 983
Oscilloscope

Model 983 is a high gain, wideband Oscilloscope designed to accurately reproduce waveforms comprising a wide band of frequencies. High sensitivity of 15 millivolts per inch RMS makes this "scope ideal for — SETTING RESONANT TRAPS... SIGNAL TRACING IN LOW LEVEL STAGES... AS A GENERAL NULL INDICATOR... for PHASE CHARACTERISTIC MEASUREMENT IN INDUSTRIAL APPLICATIONS... and for SWEEP FREQUENCY VISUAL ANALYSIS.

The 'scope contains identical vertical and horizontal push-pull amplifiers with a choice of AC or DC coupling without affecting either sensitivity or band width. Both amplifiers have compensated step attenuators and cathode follower input. *It has excellent square wave reproduction with overshoot of only 2 to 5%, with a rise time of 0.1 microsecond. The 'scope response is essentially flat throughout the specified range of 4.5 mc and is usable to 6 mc.*

The unit has provisions for internal calibration, internal phased sine wave, and Z-axis intensity modulation. Reversal of polarity of both horizontal and vertical signals is easily accomplished by means of toggle switching. *Tube replacements are non critical, and etched circuitry facilitates quick and rapid maintenance.*

The Model 983 Oscilloscope is now available through local distributors. For complete literature write WESTON Electrical Instrument Corporation, 614 Frelinghuysen Avenue, Newark 5, New Jersey.

**WESTON** *Instruments*

### WAVEFORM ANALYSIS

Response curves accurately displayed. Ideal for use with Weston intensity marker display. A fast, retrace sweep circuit with cathode follower output prevents pattern distortion.

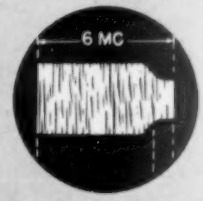
### SQUARE WAVE RESPONSE

Overshoot is only 2 to 5%. Rise Time is 0.1 Microsecond. Square wave depicted 250 kc.

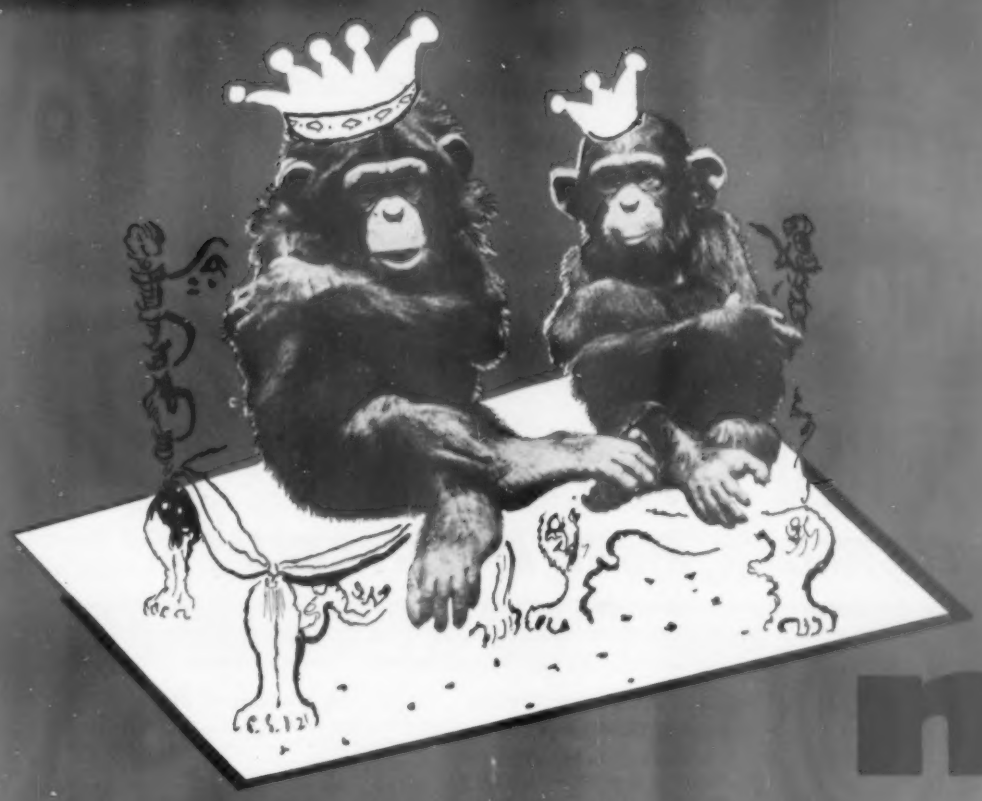
### PHASE MEASUREMENTS

Phase shift between horizontal-vertical amplifiers, 0-500 kc-0°, to 1 mc within 2°; by internal adjustment with gain controls at max 0° phase shift possible on any specific frequency to 6 mc.

### RESPONSE CHARACTERISTIC




Note flatness throughout specified range; to 3.6 mc down 1.5 db, at 4.5 mc down 3 db, at 6 mc down 6 db.



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**Catering to his wishes is the way to bigger servicing profits.**

Set owners depend upon you as a "specialist" to install top-quality replacement parts that will give long, satisfactory service . . . for this reason, Astron developed "*Staminized*" capacitors . . . a special process imparts extra-ruggedness to each unit . . . it's the protection that lets you install with complete confidence.

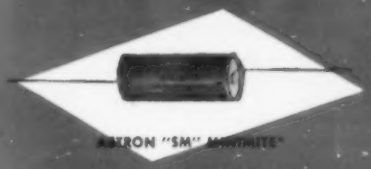
This royal quality gained immediate and widespread acceptance among service technicians . . . it's why Astron "SM"* Safety Margin Electrolytics can successfully withstand surge voltages and overloads without permanent damage . . . their reputation for durability is the sure key to increased consumer satisfaction and faster, more profitable servicing for you

Easy-to-install, exact replacement Astron "SM" Electrolytics are available in a wide range of styles . . . one for every servicing requirement . . . meticulously assembled by contamination-free techniques for dependable 85°C operation, low leakage and long shelf life.

They're backed by the famous Astron guarantee—result of *TEN* individual production tests and 100% final inspection.

See your local jobber for Astron capacitors—Today!

**FREE SERVICING AID**—Write for your copy of *NEW* handy pocket-sized replacement capacitor and pricing guide — Now!



ASTRON "SM" MINIMITE*

ASTRON "SM" [illegible]-PRONG

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PHOTOFACT Service Data is the *only* service information based upon first-hand examination of the actual production-run receivers and equipment. It is authentic, uniform data developed through actual study and analysis by service engineers in the Howard W. Sams Laboratories. PHOTOFACT is the *only data* prepared from the practical point of view of the Service Technician.

Thousands of Service Technicians use PHOTOFACT daily for time-saving, profit-boosting service operations. If you've never used PHOTOFACT, you've never realized your full earning power—you've never given such complete customer satisfaction. So get the proof for yourself. Try PHOTOFACT—use it on any job. Your Parts Distributor has the Folder Sets you need for any of the 17,000 TV and radio receivers, changers, recorders, etc., covered in PHOTOFACT. Once you use this great service, we know you'll want the complete PHOTOFACT Library.

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**1.** Famous "Standard Notation" uniform symbols are used in every schematic.

**2.** The same standard, uniform layout is used for each schematic.

**3.** Diagrams are clear, large, easy to read, easy to handle.

**4.** Wave forms are shown right on the TV schematics for quick analysis by 'scope.

**5.** Voltages appear on the schematics for speedy voltage analysis.

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**8.** Schematics are keyed to photos and parts lists.

### FULL PHOTOGRAPHIC COVERAGE

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**11.** Photo coverage provides quicker parts identifications and location.

### ALIGNMENT INSTRUCTIONS

**12.** Complete, detailed alignment data is standard and uniformly presented in all Folders.

**13.** Alignment frequencies are shown on radio photos adjacent to adjustment number—adjustments are keyed to schematic and photos.

### TUBE PLACEMENT CHARTS

**14.** Top and bottom views are shown. Top view is positioned as chassis would be viewed from back of cabinet.

**15.** Blank pin or locating key on each tube is shown on placement chart.

**16.** Tube charts include fuse location for quick service reference.

### TUBE FAILURE CHECK CHARTS

**17.** Shows common trouble symptoms and indicates tubes generally responsible for such troubles.

**18.** Series filament strings are schematically presented for quick reference.

### COMPLETE PARTS LISTS

**19.** A complete and detailed parts list is given for each receiver.

**20.** Proper replacement parts are listed, together with installation notes where required.

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*After initial adjustments are made, as in photograph, "Mr. Meticulous" automatically performs critical operations in making junction tetrode transistors—tiny experimental devices which may find important uses in the telephone system.*

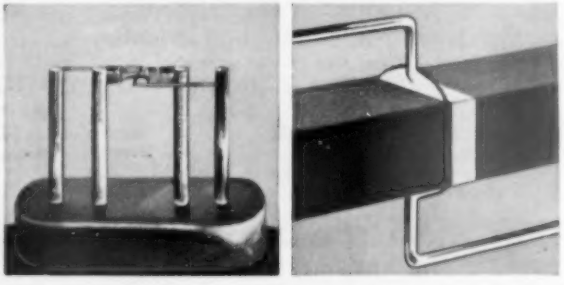
# The machine we call "Mr. Meticulous"

Bell Laboratories scientists, who invented the junction transistor, have now created an automatic device which performs the intricate operations required for the laboratory production of experimental model transistors.

It takes a bar of germanium little thicker than a hair and tests its electrical characteristics. Then, in steps of 1/20,000 of an inch, it automatically moves a fine wire along the bar in search of an invisible layer of positive germanium to which the wire must be connected. This layer may be as thin as 1/10,000 of an inch!

When the machine finds the layer, it orders a surge of current which bonds the wire to the bar. Then it welds the wire's other end to a binding post. Afterward, it flips the bar over and does the same job with another wire on the opposite side!

Once only the most skilled technicians could do this work, and even their practiced hands became fatigued. This development demonstrates again how Bell Telephone Laboratories scientists work in every area of telephony to make service better.



*Transistor made by new machine is shown in sketch at left above, magnified 6 times. At right is sketch of area where wires are bonded. The wires are 2/1000 inch in diameter, with ends crimped to reduce thickness.*

BELL TELEPHONE LABORATORIES

*IMPROVING TELEPHONE SERVICE FOR AMERICA PROVIDES CAREERS FOR CREATIVE MEN IN MECHANICAL ENGINEERING*

# MR. SERVICE DEALER: you're ridin' high, wide an' handsome

in this RAYTHEON **LIFE** ad September 12th

LIFE
It takes a heap of Know-How to ride herd on 36,000,000 TV Sets
In only a few short years, America has created a new guild of skilled craftsmen . . . the electronic technicians who service the nation's 36 million television receivers. It's a big job—one that calls for a high order of technical know-how and a substantial investment in training and equipment.
Your neighborhood radio and television serviceman takes pride in his ability to serve you with skill and integrity.
He takes special pride when he has qualified as a member of the select group of Raytheon Bonded Electronic Technicians. As such he displays the Raytheon Bonded Seal and adheres to this Code of Ethics:
1. Guarantee all radio and television repair work for 90 days.
2. Use only parts of recognized quality.
3. Charge not over established prices for parts.
4. Test customers' tubes as accurately as possible.
5. Keep labor charges at a reasonable level.
6. Perform only such work as is necessary.
7. Maintain proper equipment for good repair work.
8. Maintain the highest quality service.
He has the ability and equipment to solve your TV service problems, whatever the make or model of your sets. His work is backed by a bond issued through one of America's largest insurance companies and his standing as a Raytheon Bonded Electronic Technician is your guarantee of satisfaction.
RAYTHEON Bonded ELECTRONIC TECHNICIANS CCC
LOOK FOR THIS SEAL
It's the symbol of Satisfactory Service
YOUR TV-RADIO SERVICEMAN
RAYTHEON

## MAKE THE MOST OF IT!

Once again, Raytheon is telling your story, this time to the 26,450,000 readers of LIFE Magazine (September 12 issue) and, once again, you have a golden opportunity to cash in on this great, national promotion. All *you* need to do is *tie in* with this dramatic, colorful, full page advertisement. Use Raytheon decals, blow-ups of the ad, displays and local advertising to show customers *you* are the capable service dealer we're talking about. You'll increase your volume and profit and boost your neighborhood prestige to an all-time high.

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These two pocket-size manuals are the hottest radio-TV servicing guides ever produced. Both contain the most complete—and the most up-to-date—capacitor replacement information available ANYWHERE!

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Here is the latest capacitor replacement information for every capacitor in 4,664 model TV sets made by 85 set manufacturers. Every manufacturer is listed alphabetically, with Sprague replacement capacitors—available everywhere—fully described and cross-referenced to the original part numbers. The manual also shows the number of models each capacitor is used in—a valuable guide for stocking popular ratings. Handy . . . convenient . . . pocket-size—for use in the shop or from your tool kit. Make sure you have the newest one. Ask your distributor for the 7th Edition.
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CERAMIC CAPACITOR
REPLACEMENT MANUAL K-200
This handy little guide is the most informative, the most complete manual of its kind ever published. Pocket-size, like Sprague's TV replacement Capacitor Manual K-101, it lists every conceivable ceramic capacitor and printed circuit replacement . . . for every television set made . . . during the past five years. All told, more ceramic capacitor values than can be found in any other manufacturer's line, including discs and tubulars. And each capacitor or printed circuit listed is one you can depend on for a no-call-back replacement. Ask your distributor for it today. It's new!
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## pre-selling...

# C·D·R Rot

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## the complete line...a model

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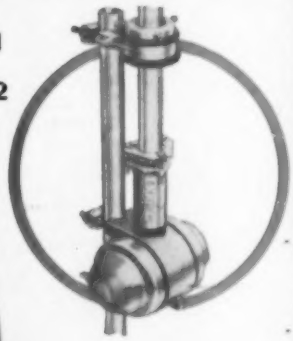
**TR-2** the heavy duty rotor with plastic cabinet featuring "compass control" illuminated perfect pattern dial, uses 8 wire cable.

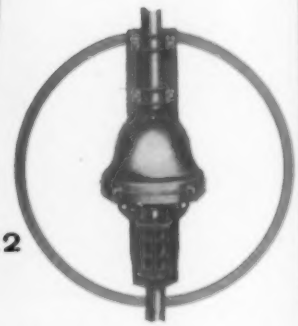
**TR-12** a special combination value consisting of complete rotor, including thrust bearing. Handsome new modern cabinet with meter control dial, uses 4 wire cable.

**TR-11** same as TR-12 without thrust bearing.

AR-1

AR-2





AR-22

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THE RADIART CORP.
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to
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every week
We are going to make this the BIGGEST rotor year you've ever had! The CDR ROTOR line is COMPLETE in every detail... featuring SEVEN MODELS.... A TYPE FOR EVERY NEED! And backing up this is the BIGGEST and most extensive consumer campaign in all our history! Millions of TV viewers will see the CDR rotor announcements on TV, pre-selling them for you. And a complete promotional kit of dealer aids to help you sell and feature CDR ROTORS! Plan now... for the BIGGEST CDR ROTOR year ever!

HARRY R. ASHLEY
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**You build *EICO KITS* in one evening — but . . . *THEY LAST A LIFETIME!***

**GET THE MOST FOR YOUR MONEY!** Don't buy ANY test instrument until you put the EICO INSTRUMENT (kit or wired) equivalent before you— and . . .

★ Compare ADVANCED ELECTRONIC DESIGN

★ Examine the QUALITY PARTS

★ Notice ease of construction

★ Check EICO's 5-WAY GUARANTEE on components, instructions, performance, lifetime service and calibration

★ Compare FEATURE for FEATURE, DOLLAR for DOLLAR

Then YOU decide who's giving you the MOST for YOUR MONEY.

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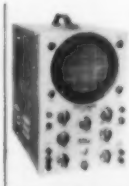
NEW RF SIGNAL GENERATOR #324



NEW
DC WIDE BAND
5" OSCILLOSCOPE
#460
KIT $79.95
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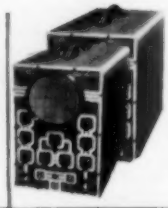

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RADIO – ELECTRONICS
Hugo Gernsback, Editor

# THE GIANT ELECTRONICS INDUSTRY

*. . . Facts and figures of our incredible industry . . .*

**The future of electronics was discussed recently by W. Benton Harrison, vice president of Sylvania Electric Products, Inc., before the Financial Analysts of Philadelphia. Highly interesting facts and figures were cited. A condensed version of Mr. Harrison's address follows:**

ELECTRONICS is such an enormous subject that it would require a good many men a good many days to speak on all its aspects. It is relatively new and growing very rapidly. Since electronics encompasses a vast multitude of products and systems and new ones are being developed and introduced almost daily, and since new companies are entering the field all the time, just producing sales-volume figures has been a monumental task.

We are extremely fortunate in having Radio–Electronics–Television Manufacturers Association (RETMA), which compiles most exact and reliable industry reports. Our predictions can come to within at least 85 to 90% of accuracy, and possibly better.

One of the two major fields within the industry today is entertainment electronics. To illustrate, let us consider what trade gossip once had to say about prospects for television in 1954. Dealers sold 6,400,000 sets to the public in 1953. This was an all-time record. When a period of rather severe inventory adjustment began in late 1953, "the trade" mistakenly attributed the setback to a decline in buying by the public. So when 1954 approached, this same "trade" glumly forecast that television set sales in 1954 would be somewhere around 5,000,000. What happened? The public bought approximately 7,300,000 sets last year, once again establishing an industry all-time high.

We expect that some day there will be just as great a percentage of television homes as there are radio homes today, and today there are 46,600,000 radio homes in the United States. Of those radio-set homes, nearly 70% also have television. This high figure, coupled with the fact that by the end of 1955 virtually the entire country will be within range of a good television signal, means that television is rapidly approaching the saturation point—the point at which virtually every home that is going to have a set already *has* one. But don't let that word "saturation" mislead you.

In fact, we believe that the public will purchase 6,300,000 black-and-white television sets in 1955, in addition to approximately 100,000 color receivers. Let's analyze that figure of 6,300,000 black-and-white sets. If only 4% of those now in use are replaced for wear or obsolescence, that means a sale of 1,300,000 sets. If population growth and establishment of new homes this year proceeds as expected, this might mean the sale of another 600,000 more sets than if the population and number of homes remain static.

The growth of the second-set idea might mean the sale of another 300,000 units. These figures—and I should like to say that in each category the estimate is *very* conservative—add up to a sales potential of 2,200,000 sets in 1955. Subtracting this from the predicted figure of 6,300,000 black-and-white sets, that leaves 4,100,000 to be marketed to established homes that never have had a television set before. *As of right now, there are approximately 15,600,000 homes in the United States without a television set.* This means the industry will have to sell one in every four existing homes currently without television in order to achieve our estimate of 6,300,000 black-and-white sets for 1955. The average cost of a black-and-white television set is $140 factory price. Therefore, if we sell a quarter-million more sets than we have estimated, that will mean an additional $35,000,000 to the industry. If we sell a half-million more sets than those predictions, that will mean an additional $70,000,000. And an extra million sets would add a whopping $140,000,000 to the industry's overall volume.

Even though the number of nontelevision homes declines appreciably each year, these factors indicate to me that the long-term potential for television certainly will range between 6,000,000 to 7,500,000 sets per year through the next decade. At the end of the decade, in 1964, it is likely that somewhere in the neighborhood of 7,300,000 sets will be sold and that annual dollar volume will be around $1,500,000,000.

In other words, dollar volume of television sets a decade hence will be 40 to 50% greater than it is today. The increase will of course be attributable to a steadily expanding number of color sets. While it is probable, we think, that no more than 150,000 color sets will be produced this year (and only 100,000 of them sold to the public), it is expected that something like 34% of sales will be color sets in the 1958–60 period and that by 1964 color will account for about 61% of all sets produced. As you can see, color is on the way, but it will be some time before color sets will be marketed in large quantities, and at least six years before production for color catches up with black-and-white.

Has television crowded home radio off the map? Hardly. The manufacturers sold 6,400,000 home radios last year for a total volume of about $136,500,000, and it is expected another 7,000,000 sets, at approximately $147,000,000, will be sold in 1955. Market surveys show that more people than ever before are listening to radio and that during the daylight hours when the housewife can't stay in one room, the radio is turned on more frequently than the television set. It seems indicated that over the 1958–60 period, nearly 7,800,000 radio sets, grossing over $148,000,000, will be sold each year and that by 1964, 8,500,000 home radio units will be sold, at a total of nearly $162,000,000.

The sale of entertainment radios for automobiles will be linked very closely, of course, to automobile production. It seems a certainty that virtually three of every four pleasure cars will be equipped with a radio. Our researches show that 4,100,000 auto sets, totaling nearly $103,000,000, were sold in 1954 and that another 4,300,000, aggregating $107,500,000, will be sold this year. Auto-set sales in the 1958–60 period should average 4,800,000 annually at an average volume of $120,000,000. In 1964, it is expected 5,600,000 auto units will be sold at a dollar volume of about $140,000,000.

Before the war, the receiving-tube business carried along at a rate ranging from $10,000,000 to $12,000,000 a year. But that market has expanded into a business, including both receiving and picture tubes, that exceeded $170,000,000 last year, is expected to be above $400,000,000 in the next five or six years and will go to $575,000,000 or higher by the end of the decade ahead.

The last factor in entertainment electronics devices is records and phonographs, which should maintain a fairly level volume of sales of between $120,000,000 and $140,000,000 a year, at a minimum, over the next decade. I have heard the high-fidelity market alone described as potentially a $200,000,000 business. (*Continued on page* 160)

# Making Printed Circuits Is Easy

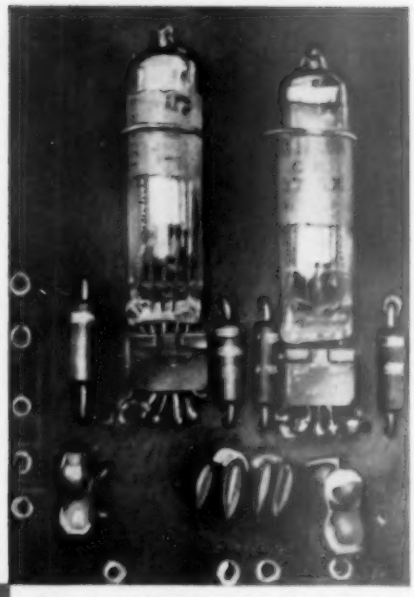


Fig. 1—Subminiature push-pull oscillator parts mounted on circuit board.

*All your needs for this type of wiring are easily available.*

By TOM JASKI

FOR commercial, industrial and military purposes printed circuits and printed-circuit wiring are well established. Some reach the experimenter and the amateur as small encased coupling plates or as major parts in the latest instrument kits.

For most of our work however we struggle along with clusters of wires, components and mounting strips, often difficult to lay out, particularly in shallow chassis. After building a few instruments with printed-circuit wiring one begins to wonder why the advantages it presents could not be obtained for most equipment. With components available in smaller sizes, transistors becoming more available and lower in cost, this would be a very desirable advance.

At least one company has put on the market a $10 kit of conducting and resistance paints. Another firm sells a 6 x 6-inch sheet of copper bonded to plastic, and the covering and etching material to make your own printed circuits.

The paints, although capable of producing a printed circuit in the true sense of the word, are costly and not easy to use.

Conductor lines are very easily damaged by the heat from even a very small soldering iron. The resistors are not particularly stable and change drastically in value with an application of the insulating lacquer. Figs. 1 and 2 show circuit wiring formed with conducting paints from a kit.

The people selling the bonded sheets offer more hope to the experimenter. The printed-circuit wiring which can be made with these kits, however, can just as well be produced with a few cents' worth of materials from the local hardware and drug stores.

## Constructing printed circuits

One type of printed-circuit board consists of some .001 to .003 inch thick brass shimstock, any type of plastic sheet and a small quantity of suitable adhesive. Professionally, an adhesive film using pressure and heat for bonding can be obtained. But most hardware stores or hobby shops carry some adhesive which will do just as well. I use a cement with the name of GOO which did a fine job without either heat or pressure so long as the directions were followed exactly. The thermosetting plastics such as Bakelite or Micarta will do a better job than most others, but even fishpaper can be used. The thermoplastics may give some trouble by melting locally when attaching connections. The brass and plastic are cleaned thoroughly before gluing, and roughening the surface with 8/0 cabinet paper may be helpful.

The circuit is carefully laid out on paper. If you have ever done maze puzzles, this part should be easy. The main trick is to avoid crossovers. Otherwise conventional circuit layout methods are used—placing the parts so that no undesirable coupling takes place and using the shortest possible connections. Provide small holes for component leads. For ½-watt resistors these should be spaced ½ inch apart. For capacitors they will vary greatly with size and voltage rating. Generally the ceramic capacitors will be the most compact.

If a crossover becomes unavoidable, two small holes in the circuit board and a short wire on the other side will turn the trick. For circuits where shielding is desirable and intercapacitances are not critical, as little metal as possible should be removed. For high-frequency circuits or low-level amplifiers requiring very high insulation values, most of the metal should be removed.

To complete the circuit board after bonding the brass and plastic, transfer the design to the brass with carbon paper or pressure with a hard drafting pencil. With a sharp pointed knife remove the metal as required. For

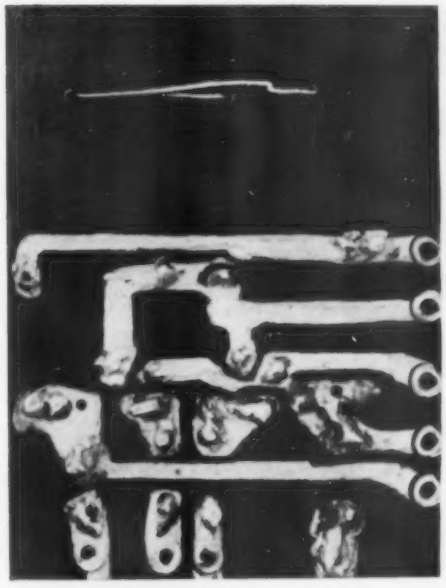
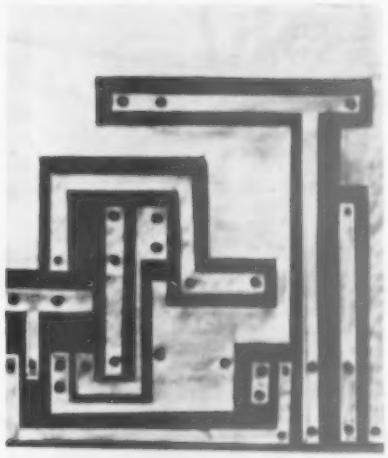


Fig. 2—Rear view of Fig. 1—conductors made with silver conducting paint.



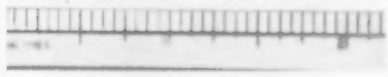
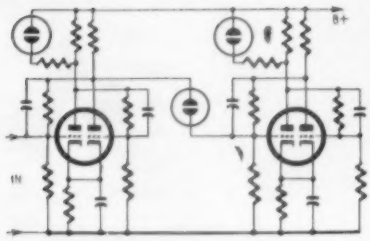


Fig. 3—Circuit board for two-stage amplifier made with knife and drill.



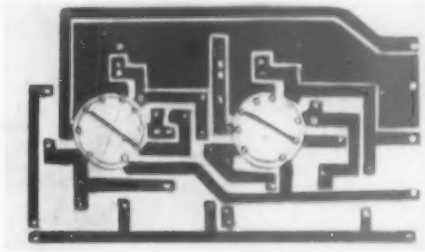


Fig. 4—Schematic diagram and circuit layout for two-step counting circuit

appearances' sake remove excess glue with a solvent recommended by the glue manufacturer. The small lead holes are made with a No. 50 drill and the circuit board is ready for installing components. With reasonable care no damage from soldering iron heat will occur. If the glue should soften locally, it will soon set again. In the meantime the component lead will hold the brass firmly in place.

You will soon learn to keep circuit lines straight and simple if the knife is to be your tool. Fig. 3 shows a circuit board for a two-stage subminiature amplifier produced with no other tools than a knife and a No. 50 drill.

A second method, a little closer to industrial practices, offers advantages for more complicated circuits. It also lends itself very well to repetitive manufacture such as the two-step counting circuit shown in Fig. 4. Start again by bonding a sheet of shimstock to plastic as before. Depending on whether you have to make one or many, either paint on the brass directly all those pieces which are to *remain* or make a stencil showing the same pieces. With a stencil a small spray gun is helpful but not essential. The paint used can be enamel or lacquer. If desired, various colors may be used for clarity. Fig. 5 shows a stencil and the painted board. A stencil to be used frequently might well be made from the same shimstock.

Prepare an etching bath consisting of water and a small quantity of sulfuric acid. Submerge the circuit board in it as the anode and any electrode will do as the cathode. Apply a 6-volt direct current, and in a few minutes the brass in the unpainted areas will begin to eat away. If a more lively bath is desired, more sulfuric acid can be added or even a few drops of nitric acid. But a fast etching bath is much harder to control.

All parts of the brass should disappear at about the same rate if it was properly cleaned, and a layer only a few molecules thick will remain which can be wiped off with the glue solvent. However, if brass islands should persist, these can be removed by momentarily connecting them to the positive side of the voltage source. Proper etching may require a little practice, but it is not difficult. Cleanliness of the brass is the single most important factor. A sheet cathode parallel to the circuit board and at least of the same size will give an evenly etched job across the whole area.

After etching, very thorough washing and rinsing, all that remains to complete the circuit board is removal of the lacquer or paint and the drilling of holes for component leads. Tube sockets are easily installed by bending the lugs forward and removing the metal mounting ring, if any. No special sockets are required. Fig. 6 shows the etched circuit board with one socket installed. It is sometimes desirable to drill the large socket holes before bonding the brass. This avoids serious stress on the brass around the holes.

In a third method the etching bath with the addition of a small quantity of copper sulfate and Rochelle salts is used. These chemicals can be obtained in virtually all drug stores. The copper sulfate can be produced by allowing diluted sulfuric acid to react with some copper in the presence of air, but it takes a long while. The process can be speeded by applying d.c. and two copper electrodes, but that requires careful filtering of the solution. This third method, perhaps the most commonly used, consists of literally growing the circuit by electroplating (Fig. 7) or electroforming. The latter term applies when we provide form walls for the metal to deposit in to the desired thickness.

Start with a very clean piece of plastic and on this paint or draw the desired circuit lines. Paint only those parts which are to *remain*, using a

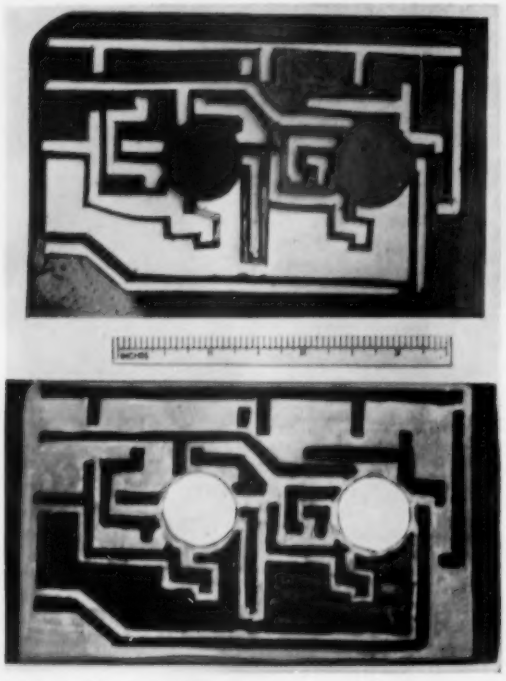


Fig. 5—Top, stencil made from layout. Bottom, the painted circuit board.

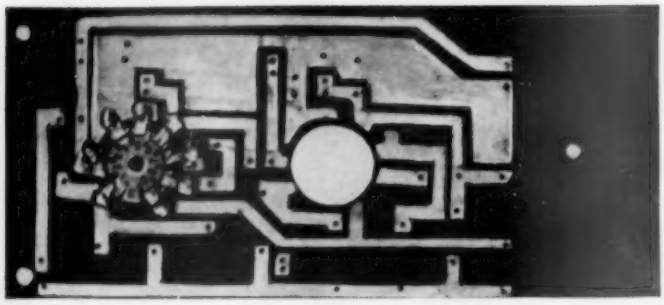


Fig. 6—The etched circuit board.

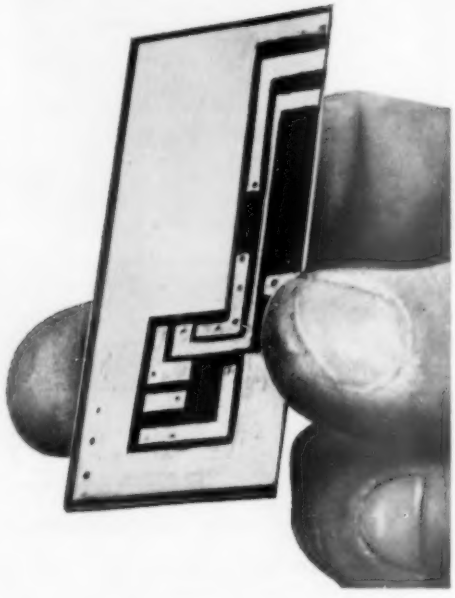


Fig. 7—Plated circuit board — plating is copper, base is Plexiglas.

conducting paint. If no conducting paint is available, it can quickly be made by removing the carbon rod from a used flashlight cell, powdering it and mixing the powder with some drafting fixative. This makes a conducting paint which shows very excellent bonding and plating characteristics. However, even a soft drafting pencil or an electrographic scoring pencil could be used. They will produce lines which can be plated, but it takes a little longer.

In drawing the circuit, the electrode must be connected to all parts. For this purpose small bridges can be drawn which can be removed later. Connecting bridges drawn on the edge of the plastic are particularly easy to remove. Immerse the circuit board in the bath, connecting it this time to the negative side of the power supply, with a copper electrode connected to the positive side. Only 1 volt is used. More voltage would make the copper porous, resulting in poor adhesion. Lower voltage would not provide "throwing power"—the copper particles would not reach their destination on the board. The bath should be about 100° F. for best results. A hot bath will provide better-quality copper and better bonding. The top limit is about 140° F. These values should provide about .001-inch plating in 45 minutes. Several thousandths thickness is desirable since it permits sanding and polishing of the circuit lines.

Electroforming is not much different from plating. In this case circuit lines are scribed in the plastic with heat. Narrow and shallow grooves can be made with a plastic cutting tool such as the Ungar type 540 marking tip. Sand the surface of the board smooth and scrape the grooves to remove loose particles. Then paint the grooves with conducting paint. At this point it would be well to check for continuity with an ohmmeter. The next step is the same as plating, with the same ingredients and current values. The formed circuit will be entirely below the surface of the plastic and thus well protected from damage.

Other methods of producing similar circuit boards, such as embedding and casting, have been experimented with but seem to have no great advantages for the experimenter. The processes involved are more complicated and more adaptable to large-scale production.

For those not entirely familiar with the advantages of printed circuits, here is a brief summary: Printed circuit wiring is neat and compact. It is not subject to mechanical shock or vibration and provides a very rigid mounting for component parts as well. It is very constant in intercapacitance relations and stable with temperature variations, important factors in critical high-frequency circuits.

The following is a list of manufacturers currently producing equipment used in the various methods of making printed circuits. This list is representative of available products and is by no means complete:

*Conducting paints*

General Cement Co., 919 Taylor Ave., Rockford, Ill. (silver $4.70 net, per ounce)
Microcircuits Co., New Buffalo, Mich. (silver and copper, parts of kits)
Handy & Harman, 82 Fulton St., New York 38, N. Y. (silver)

*Resistance paints*

Microcircuits Co., New Buffalo, Mich. (in kit form, approximately $10)
Inter Electronics Corp., 2432 Grand Concourse, New York 58, N. Y.

*Bonded-sheet kits*

Tele-Diagnosis Co., 155 W. 72 St., New York 23, N. Y. (kits $19.95)
Techniques Inc., 135 Belmont St., Englewood, N. J. (kits, $4.95–$25)
Consultants for Industry, 273 E. 175 St., New York, N. Y.
Harcon Electronikits, Brandywine, Md.

*Bonded sheets*

Mica Insulator Co., Schenectady 1, N. Y.
Continental Diamond Fibre Co., Newark 16, Del.

END

# Common-Collector Transistor Amplifiers

By RUFUS P. TURNER

THE input impedance of the familiar common-base and common-emitter junction transistor amplifiers is notoriously low when compared with the high input impedance of tube type amplifiers. Typical values are 60 ohms for the common base and 1,000 ohms for the common emitter.

The *common-collector* amplifier circuit, least familiar of all three transistor circuit configurations, *does* have high input impedance and can be used as the input stage of transistorized instruments such as multistage amplifiers, signal tracers, a.c. electronic voltmeters, Geiger counters and similar devices. It is useful also, in lieu of a stepdown coupling transformer, between transistor amplifier stages as an interstage impedance-matching device. Unlike the transformer, the common-collector stage provides power gain.

The common-collector amplifier resembles the tube type cathode follower in the following respects: It has high input and low output impedance, voltage gain of less than 1, power gain, excellent frequency response and no phase reversal. The common collector differs from the cathode follower, however, in that its input resistance is not independent of its output resistance, being highest for high output values and vice versa. Also, its output resistance increases as the resistance of the signal source (generator) increases. Another important property is that, for fixed generator and output resistances, the input resistance of the common collector decreases with increasing signal frequency. In spite of these uncommon characteristics, the common collector is quite satisfactory as a source of high input impedance, along with power gain, in the input stage of many transistorized circuits.

In a common-collector circuit, the input signal is applied between the base and collector of the transistor (Fig. 1). The internal base resistance $r_b$ and collector resistance $r_c$ thus are in series with the signal source. It is $r_c$ that gives the common-collector circuit its high input value, since $r_c$ for a junction transistor is very high with respect to $r_b$.

In surveying the characteristics of commercial transistors, the CK725 seemed to have particular merits for common-collector operation, since its collector resistance is 2 megohms and its alpha high. The base resistance of this unit is 1,500 ohms, so offhand one might expect to obtain an input resistance ($r_c + r_b$) of 2,000,000 + 1,500, or 2,001,500 ohms in a common-collector circuit. Actually, however, this value could not be attained practically, since $r_c + r_b$ must be multiplied by a decimal equal to $\frac{r_c + R_L}{r_c - r_m + r_c + R_L}$. For the CK725, the maximum calculated input resistance thus will be something less than 2 megohms.

The resistance-capacitance-coupled circuit shown in Fig. 1 was assembled for test. In this arrangement, the base of the transistor "floats" without bias to provide the highest possible input resistance. (A bias-stabilizing resistance network would lower the impedance.) A *low-voltage* d.c. source (1.5) was chosen since the resulting low d.c. emitter current helps keep the input resistance high.

Using a 600-ohm signal generator, the following performance data were accumulated: **1.** Input impedance at 20 cycles is 1.2 megohms and decreases to 160,000 ohms at 50 kc. This falloff is shown by the curve in Fig. 2. Individual CK725's might supply higher input impedance. **2.** Voltage gain is constant at 0.96 from 20 cycles to 10 kc (Fig. 3) and falls slowly to 0.88 at 50 kc. **3.** The maximum input signal voltage $E_{in}$ before positive-peak clipping appears in the output signal is 0.52 volt r.m.s. **4.** The corresponding maximum output signal voltage $E_{out}$ is 0.499 volt r.m.s. **5.** Power gain is 30.74 (14.87 db.).

These data were taken with a high-impedance a.c. vacuum-tube voltmeter and oscilloscope connected in parallel across the signal output terminals. The minimum load which might be connected directly to the output terminals of the circuit in Fig. 1 without upsetting its operation would be approximately 10 times R1, or 300,000 ohms.

When this common-collector circuit is used as the input stage of a system, its output should be transformer-coupled to the next stage for satisfactory impedance matching and to maintain the very high input impedance. For example, the circuit in Fig. 1 may be transformer-coupled to the input of a common-emitter voltage amplifier stage (input impedance = 1,000 ohms) with a 30,000-to-1,000-ohm coupling transformer. This transformer would have a turns ratio of approximately 5.5 to 1. The high-impedance winding of the transformer is connected in series with the emitter and the positive terminal of the battery, R1 and C1 being omitted. If no transformer were used and R1 were made 1,000 ohms, the input impedance of the common-collector circuit would drop to approximately 20,000 ohms at low frequencies and still lower at high frequencies.

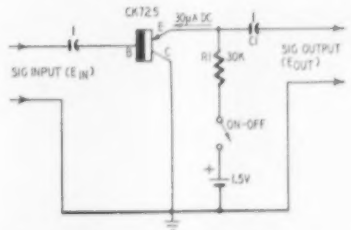



**Fig. 1—Schematic diagram of common-collector transistor amplifier circuit.**

The curve in Fig. 3, showing falloff of input impedance with increasing frequency, indicates that this particular common-collector circuit might be useful only with a signal source which would not be loaded badly by the lowest amplifier input impedance (160,000 ohms at 50 kc). Low- and medium-impedance transducers, pickups and microphones would fall into this category. In applications where the operating frequency is either fixed or extends over only a narrow band, the common-collector input impedance is fairly constant. Such applications include bridge null detectors and other single-frequency a.f., r.f., and i.f. amplifiers; signal tracers in which the transistor audio amplifier is preceded by a diode detector and the r.f. test signal is amplitude-modulated at a single audio frequency; Geiger counters; code-signaling circuits.

The common-collector circuit merits attention and exploitation by the experimenter, who up to this time seems to have overlooked its important possibilities while grasping for the higher voltage gain and power gain of the two other common circuits. END

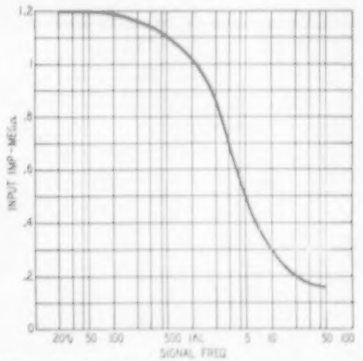



**Fig. 2—Variation in the common-collector input impedance with frequency.**

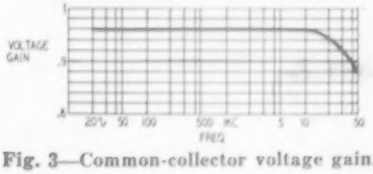



**Fig. 3—Common-collector voltage gain.**

# Flexible Radio Control System

By RICHARD H. DORF*

*Part II—The radio receiver and control system*

Top view of boat with cabin removed. Antenna jack is in forward hatch cover.

WITH the boat's removable cabin off (see photo) the electric components can be seen. Toward the bow, immediately behind a 90-volt battery, is the 6-meter superregenerative receiver, which includes audio voltage amplifiers and a power output stage. A little aft of midships is the control chassis containing eight relays. Four of these are resonant-reed relays, which operate only when energized by a.c. of the correct frequency. The frequencies used are 416.3, 442.6, 470.5 and 500.2 cycles. They can be so close without any possibility of control errors because the sensitive spectrum of each relay extends over a range equivalent to only 1% of its nominal frequency.

The resonant relays cannot control power directly so they are made to energize auxiliary relays which can. The auxiliary relays control rudder motion and drive. One 90- and one 45-volt B battery are used, plus a 1.5-volt cell for filament heating and a 6-volt miniature storage battery for the drive and steering motors.

Fig. 1 is a schematic diagram of the boat receiver. Isolating stage VI helps prevent superregenerator radiation from causing trouble. The superregenerator is V2-a, with R1 the regeneration control. Stages V2-b and V3-a are voltage amplifiers, and V3-b is the power output stage which feeds the control chassis and the resonant relays.

Fig. 2 shows the top of the receiver chassis. A Bud Minibox 3 x 4 x 5 inches was used for both receiver and control chassis. The receiver chassis is simply the unflanged part of the Minibox, with the tubes mounted underneath (Fig. 3). This was necessary because, when the cabin is replaced on the boat, there is no room for tubes on top. (There is an extra tube socket which later was not needed but was left in place out of laziness.) This method of construction has the advantage that the circuitry is accessible even when the chassis is in operating position, so that adjustments and tests can be made.

*Electronics consultant, New York.

Fig. 4 is a diagram of the control chassis. This is the flanged part of the Minibox, with two sides removed by the simple process of bending them until they fall off. The result appears in Fig. 5. The legs are angles. The alteration was made so that the control chassis could straddle the propeller drive shaft to conserve space. As Fig. 5 shows there is very little under the chassis so this is no problem.

The relay connections require a little explanation. RY5 and RY6 (which are energized by resonant relays RY1 and RY2) have single-pole double-throw contacts and control the polarity of voltage applied to a small steering motor (of which more later). Tracing the connections, it is seen that if RY5 and RY6 are unenergized, contacts 1 and 2 of J4 go to ground. If RY5 is energized, contact 2 of J4 remains at ground potential while contact 1 goes 6 volts positive. When RY6 is energized, just the reverse happens.

The drive-motor circuit could have been made just the same, and in fact constructors will probably do it that way. However, I just happened to have a double-pole double-throw relay in stock, with only three of the others, so it was used. Here RY8 does the polarity-reversing in the standard way, while the contacts of RY7 stop current from passing to the motor when they are open. With RY8 unenergized polarity is such as to cause the boat to go astern and when RY7 closes that happens.

The relays used for RY5, 6 and 7 were 2,000-ohm G-E surplus units. It is much better for the life of the resonant relays to use 10,000-ohm relays throughout, in which case the values for R1 and C1 should be used with all relays rather than the simple 1-$\mu$f capacitors necessary to make the less sensitive ones work. The value of R1 can be increased, depending on trial.

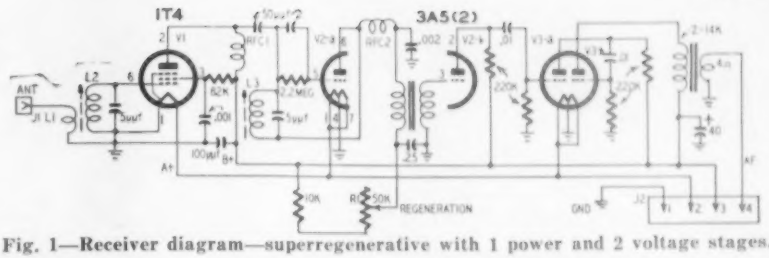



**Fig. 1—Receiver diagram—superregenerative with 1 power and 2 voltage stages.**

Fig. 6 is a diagram of the wiring installed in the boat. All permanent wires are threaded through small holes made in the boat frame supports to keep them in place. The boat photo shows the battery locations. To get the 1.5-volt cell in place in this model, a couple of the frame supports must be cut away, but remaining strength is sufficient.

Connectors of any kind can be used. The ones used in this boat were made up from an Elco Varicon kit, which permits making connectors of any size. Insulated hookup wire is used.

## The rudder

This arrangement (Fig. 7) is somewhat special and works out very well, even as constructed by an individual who dislikes mechanical work.

The motor which drives the rudder is a small 4–6-volt d.c. unit with a transparent plastic housing. It rests on its side in the left rear compartment of the boat and is set in place with Duco cement. Its shaft holds a worm which extends in the direction of the bow. A vertical shaft supported in holes in a small metal dual angle has a small pinion gear on each end. The lower gear contacts the worm; the upper gear can be seen in the photo.

The rudder post goes through a small tube and is soldered to the rudder. The upper part is bent so that it forms a sort of tiller. A section of rack is bent into a quarter-circle and a hole drilled in it to take the end of the tiller, which is fastened in place with solder. The circular rack section contacts the upper pinion gear.

When the motor rotates, the gears are rotated and the rack is swung back and forth taking the rudder with it. The rack section is short enough so that it goes off the gear at the limits of rudder travel. There is thus no problem of

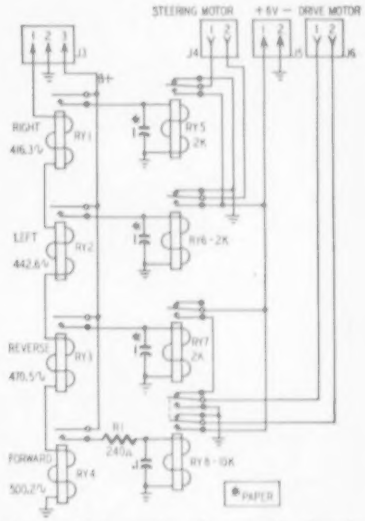



**Fig. 4—Schematic of control chassis.**

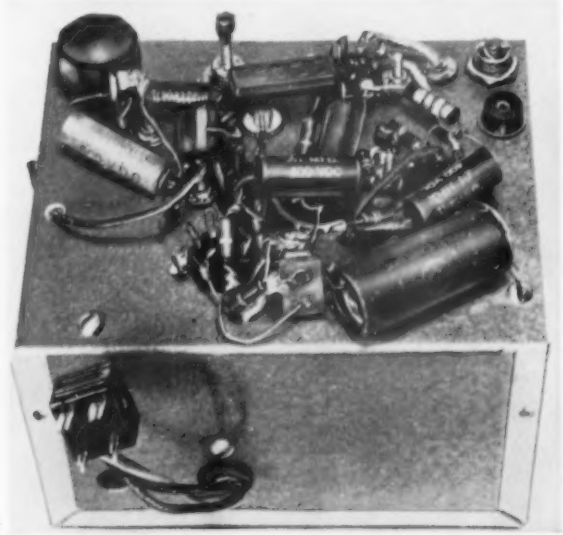


**Fig. 2—Topside of the receiver chassis.**

**Fig. 3—Underchassis view of receiver.**

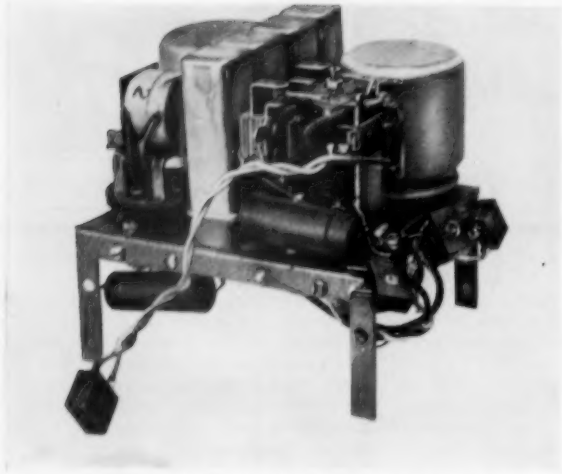


Fig. 5—Control chassis holds relays. It is a modified Minibox (see text).

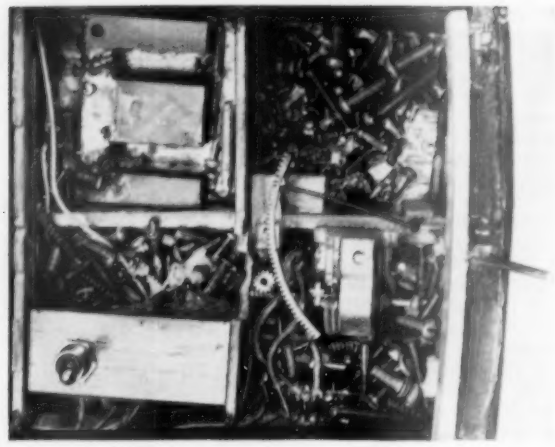


Fig. 7—Rudder drive system under rear deck. Screws and bolts provide ballast.

mechanical binding and there need be no limit switches to stop the rudder motor. Small pieces of foam rubber press the ends of the rack lightly against the gear at the rudder limits so that the rudder immediately starts to move when the steering motor is reversed after overtravel.

The worm, gears and shaft are available in hobby shops where the motor can be bought. They are approximately 48 pitch and the rack is 48 pitch, obtained in 2-foot lengths from Boston Gear or any similar company. All are brass.

The rack should be bent to shape after the motor, gears and rudder are in place. Measure the distance between the vertical rudder post and the gear, then draw a circle on paper with this as a radius. Bend the rack to shape, using the perimeter of the circle as a pattern. Exactness is not necessary—the whole system is far from a precision job but it is adequate. Lubrication of the gear system is not desirable—since it will catch dust—and is not necessary for low speeds and intermittent operation.

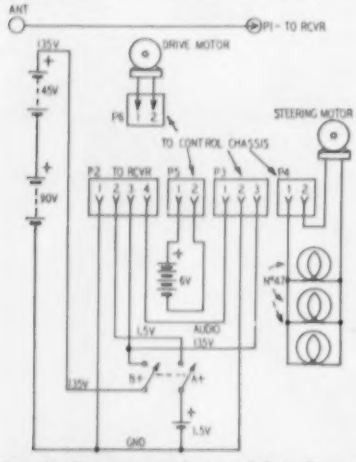



Fig. 6—Permanent boat wiring. Lamps prevent rudder motor from going too fast; when cold, their low resistance passes extra current for motor starting.

## Final adjustment

The entire system can be adjusted on the bench before it sees the water. Make a simple stand to hold the boat (see photo in Part I). A banana jack is fastened to a hatch cover on the forward deck and the wire led to the antenna plug. The antenna is a piece of bus wire a couple of feet long, soldered at one end to a banana plug.

Turn on the transmitter (keep it a few feet away) and adjust the oscillator and amplifier tuning for maximum output, switching on any tone for this purpose. Advance the receiver regeneration control about a quarter-turn and tune the oscillator slug (L3 in Fig. 1) for maximum audio as indicated by vibration of a resonant relay or a pair of phones clipped to ground and some wire or plug pin connected to the receiver audio output. Adjust regeneration for a clear tone. Tune the antenna coil for maximum output; this will not be a sharp maximum.

Now, if it has not been done before (and even if it has, do it as a touchup), adjust the values of the tone-tuning capacitors in the transmitter so that the relays operate. There may be spots in the room, especially if it is in a steel-beamed building, where there is poor reception. This is due to standing waves and will not happen out of doors.

When the receiver battery voltage is low, the steering and drive relays may not operate simultaneously due to lack of sufficient audio power output from V3-b (Fig. 1). While the receiver does not draw more than 20 ma from the B supply, this happens eventually. The batteries can be pepped up by connecting them to an external power supply for a few hours, with the supply voltage adjusted for a current to the batteries of around 30 to 50 ma. The same can be done for the transmitter, which is a principal reason for the test jack.

Before letting the boat ride the waves, one more thing is necessary—ballasting. The radio equipment will inevitably be out of balance, and probably will cause the boat to be down by the head. Fig. 7 shows a simple ballasting method—adding old screws and bolts in the rear compartment. Fill the bathtub with water and carefully place the boat in it. Then add old screws, bolts and anything else heavy that comes in small pieces to the rear compartment until the boat is balanced. Remove the antenna for this job. Then dump in generous quantities of Duco cement to hold the ballast in place. When dry, put the boat back in the tub and leave it for several hours to see that there are no leaks.

Then off to the nearest body of water and her maiden voyage! END

### Parts for receiver and control system

**Resistors:** 1—10,000, 1—82,000, 4—220,000, 1—2.2 megohms, ½ watt; 1—240 ohms (see text), 1 watt; 1—50,000 ohms, potentiometer, linear.

**Capacitors:** 2—5 μμf, 2—50 μμf, 1—100 μμf, mica; 1—.001 μf, 1—.002 μf, 2—.01 μf, 1—0.1 μf, 1—0.25 μf, 3—1 μf, 200 volts, paper; 1—40 μf, 200 volts, electrolytic.

**Relays:** 1—resonant, 416.3 cycles (Frahm 3304-8 or equivalent); 1—resonant, 442.6 cycles (Frahm 3304-7 or equivalent); 1—resonant, 470.5 cycles (Frahm 3304-6 or equivalent); 1—resonant, 500.2 cycles (Frahm 3304-5 or equivalent); 3—2,000 ohms (see text), sensitive, s.p.d.t. (G-E surplus); 1—10,000 ohms, sensitive, d.p.d.t. (Potter and Brumfield LM11 or equivalent).

**Miscellaneous:** 1—1T4, 2—3A5's, tubes; 1—coil L1, 3 turns of hookup wire over ground end of L2; 1—coil L2, 12 turns of No. 16 enameled wire on Millen 69046 form; 1—coil L3, same as L2; 1—transformer, interstage, 1:4 turns ratio, primary impedance 7,000 to 15,000 ohms, secondary center tap not used (Stancor A-64-C or equivalent); 1—transformer, output, 14,000 to 4 ohms (Stancor A-3496 or equivalent); 2—r.f. chokes, 6 meters; 1—banana jack and plug; 1—phone jack and plug; 1—4-pin male and female connector; 1—3-pin male and female connector; 3—2-pin male and female connector; 1—battery connector for 90-volt battery; 1—battery connector for 45-volt battery; 1—connector for 1.5-volt cell; 1—90-volt battery (RCA VS 090 or equivalent); 1—6-volt battery, wet, miniature (Willard or equivalent); 1—1.5-volt dry cell (Burgess 4F or equivalent); 1—45-volt battery (Eveready 455 or equivalent); 1—6-volt motor, d.c.; 1—4-6-volt motor, d.c.; 3—No. 47 lamps; 3—7-pin miniature sockets; 3—5-pin sockets (for 2,000-ohm relays); 1—aluminum box, 3 x 4 x 5 inches (Bud Minibox CU-3005 or equivalent); 1—gear set, 1 worm, 2 pinions, rack, 48 pitch, brass (Boston Gear); 1—coupling for drive motor; 1—d.p.s.t. switch; 4—crystal sockets, double, for resonant relays (Cinch 2K4 or equivalent).

# Contact Potential

By H. P. MANLY

SOMETIME, when you are working on a receiver, disconnect all but the heater leads from the socket of any tube. Set your vacuum-tube voltmeter for measuring negative d.c. volts, on the lowest range. As shown in Fig. 1, connect the positive lead of the v.t.v.m to the cathode lug on the tube socket and the negative lead to the grid lug. Turn on the power to heat the cathode of the tube. The voltage you read on the meter dial is contact potential.

Negative electrons are boiling out of the hot cathode into the surrounding vacuum to form a space charge. Billions of these electrons collect on the grid which is nearest the cathode and there they form a negative charge. These electrons can escape only slowly through many megohms of resistance in the v.t.v.m. and enough remain to hold the grid decidedly negative with respect to the cathode. In many minature tubes the difference of potential will read about 1.5 volts.

You will find contact potentials also on plates of triodes and on plates and screens of pentodes, but the values are very small. This is because not many space-charge electrons get past the grid. If, however, you check from the plate to cathode of a diode such as the 6AL5, contact potential will measure as high or higher than those on grids of triodes and pentodes. Electrons in the diode are intercepted by no other elements between cathode and plate.

Next connect a resistor of about ½ megohm between cathode and grid of a triode or pentode (Fig. 2) or between cathode and plate of a diode. Measure contact potential across this resistor. It will be only 20 to 30% of the former value for now electrons are returning to the cathode more rapidly through the resistor than they did through only the v.t.v.m. and fewer remain on the grid (smaller negative charge) at any given moment. If you substitute a grid-return resistor of only 10,000 to 20,000 ohms, the contact potential may not be measurable. Here we have one reason why so many tube data sheets warn against grid circuit resistance of more than ¼ to ½ megohm—or even 100,000 ohms. It is to reduce the biasing effect of contact potential.

Contact potential negatively biases a grid without the help of any external voltage. In many radio receivers the grid resistor on the audio voltage amplifier has a value of about 10 megohms. A familiar circuit is shown in Fig. 3. Contact potential across this high resistance supplies the entire negative bias needed by the amplifier.

When a twin-diode tube is used in a vacuum-tube voltmeter or other service instrument as a rectifier or detector, one section may be employed solely for balancing the contact potential of the other section. A method of doing this is illustrated in Fig. 4. At *a* is a simple shunt rectifier consisting of a single diode which delivers pulsating positive direct current when a.c. voltage is applied. With or without an applied a.c. voltage there is contact potential, and at very small a.c. inputs this contact potential may add materially to d.c. output voltage.

At *b* a second diode is added with its connections reversed. If contact potentials of the two diodes are equal at the d.c. output, they will balance each other. In practice, the contact potentials of two diodes or of two sections of a twin-diode are likely to be different, so we resort to the connections at *c* of Fig. 4.

With these connections, positive and negative contact potentials of the two diodes act at opposite ends of a balancing potentiometer, with rectifed d.c. output taken from the slider. Moving the slider will allow picking up enough negative contact potential from the second diode to balance the positive contact potential from the first, and d.c. output will be unaffected.

Contact potential may be balanced also with any available d.c. voltage of opposite polarity which may be adjusted to suitable value. But without some form of balancing, low-voltage measurements may be erroneous. There is no measurable contact potential between elements of a crystal diode, and no balancing is needed. This is an advantage of the crystal over the tube when used in detector probes for service instruments.

Contact potential in a tube becomes less with lower heater voltage and cathode temperature since electrons boil less rapidly out of the cooler cathode and form a weaker space charge. At half normal heater voltage, contact potential may be two-thirds or less its maximum value. Contact potential tends to be greater in tubes of high transconductance than in those of less amplification. The reason is that grid wires are more closely spaced and may be closer to the cathode in a high-gain tube, and the grid collects more negative electrons.

You may wonder why we talk about *contact* potential when the tube elements are not actually in contact. It is because this effect is similar to that observed when different metals are in close contact, even when surrounded by air. For instance, brass becomes negative to aluminum by almost 0.2 volt. Again, when different metals are immersed in a liquid electrolyte, the metals acquire a difference of potential, called contact potential. In vacuum tubes the grid takes electrons from the cathode through a vacuum when no external voltage is applied, but the effect still is called contact potential. END

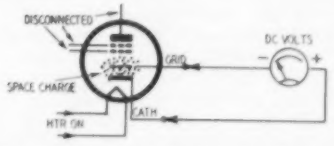



**Fig. 1—Negative electrons collect on grid to produce a contact potential.**

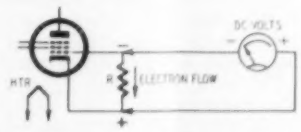



**Fig. 2—Measuring the contact potential across a grid-return resistor.**

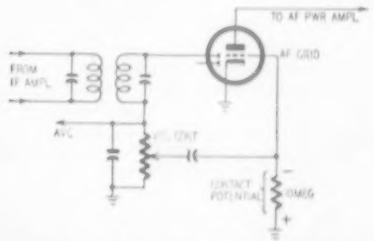



**Fig. 3—Conventional audio amplifier circuit biased by contact potential.**

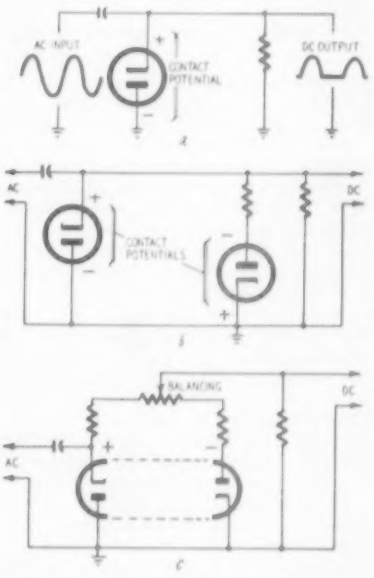
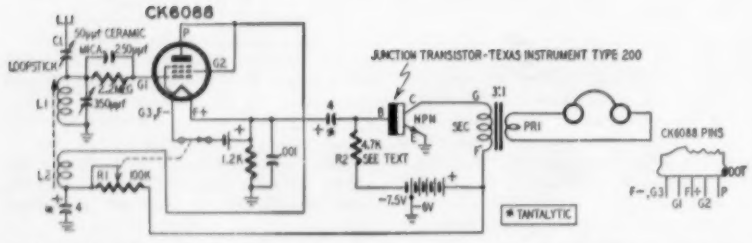



**Fig. 4—Balancing contact potential.**

# TUBE and TRANSISTOR RADIO

By IRVING GOTTLIEB




**Schematic diagram showing all components in the tube–transistor receiver.**

IN many respects the transistor is admirably suited for the construction of compact radio receivers. In addition to its space-saving feature, it requires considerably less battery power than does the tube. Unfortunately, it is not easy to use transistors efficiently with resonant circuits. The input impedance of the transistor is, in some arrangements, too low to connect to a conventional parallel resonant circuit; in other configurations it is too high to use the tuning properties of a series resonant circuit. The transistor counterpart of a vacuum-tube regenerative detector is likely to be less sensitive and generally less selective than the tube circuit. This represents quite a problem to the would-be constructor of a small headphone receiver.

A successful solution which overcomes this obstacle is a hybrid circuit consisting of a tube detector and one or two transistor audio amplifiers. The battery economy of such a set, though not as attractive as the straight transistor circuit, is much better than that of a design based entirely on tubes. The CK6088 is a good tube for this purpose in view of the rather frugal demand of the filament, only 20 ma at approximately 1.5 volts. Such a tube–transistor set consumes 20 ma from a size D flashlight cell and about 3.25 ma from a 7.5-volt C battery.

A two-tube version of this set required 40 ma from the A supply and, for the same performance as the tube–transistor radio, a 22.5-volt B battery was needed. With a tube and two transistors the percentage difference in battery drain between such a combination and a three-tube set is even greater. Furthermore, the tube–transistor combination works as well as straight tube sets. The additional power gain that might be expected from tubes is largely lost because of the low $g_m$ of subminiature tubes and from the difficulty in obtaining high sensitivity and high audio amplification simultaneously in the tube detector.

## Circuit description

The circuitry of the tube–transistor receiver is shown in the diagram. The tube operates as a cathode follower at audio frequencies, at the same time providing radio-frequency regeneration. The reason for this unusual arrangement is that the low input impedance of the grounded-emitter transistor stage must be fed by a signal source also of low impedance if we are to obtain efficient power transfer. In addition the current and power gain developed by a cathode follower is used in driving a transistor amplifier.

In the initial adjustment of this receiver it is important that L2 should have just enough turns so that oscillation starts with R1 practically in its zero-resistance position. Start with L2 having about six turns around the ground end of L1. The tube will not deliver enough power to drive the transistor if its plate voltage is reduced too far below the applied 6 volts despite the fact that—with enough feedback—the detector can oscillate with a plate potential of 2 volts or so. For this reason, the prescribed number of turns for L2 may be a bit skimpy. However, sensitivity and selectivity will be very much improved even if the regeneration is below the value needed to cause the detector to oscillate when R1 is fully advanced. Some experimenting should be done to determine optimum conditions of detector operation. This is easy since the coupling between L1 and L2 can be varied considerably by adjusting the position of the ferrite core. The effect upon the tuning range and Q of L1 will not be great, provided the greater portion of the slug remains within L1. To take advantage of this easy way to establish optimum feedback, it is important that L2 be wound next to one end, preferably the ground end of L1, and not directly over L1.

Most important, keep in mind that the wrong phasing of L2 will produce degeneration, with the very opposite of the benefits desired from regeneration. This can be readily determined by trying the connections to L2 first one way, then the other. The connections which result in oscillation or in the most peppy performance are right and should not be reversed for any subsequent change in the number of turns on L2 or in spacing between L2 and L1.

The antenna, like the feedback adjustment, can be expected to vary with receiving conditions. A 15-foot outdoor antenna should be adequate for good pickup of weak stations, provided a ground is also used. Of course, a longer antenna (within limits) is better. A 4-foot vertical whip without any ground is sufficient for strong and medium-strength stations. Fairly good reception could be obtained by connecting only the ground wire to the antenna terminal of the set. Whatever the antenna

used, C1 must be adjusted to find the best coupling conditions. The shorter the antenna, the higher must be the capacitance of C1. For operation with a whip antenna, C1 should be paralleled by an additional 100-$\mu\mu$f capacitor.

The transistor collector current should be about 1.5 ma. This current is primarily determined by R2. Since transistors differ considerably from unit to unit, it may be necessary to modify R2. The transistor used was a germanium junction n-p-n type. Equal results may be expected from a p-n-p junction transistor but the circuit will have to be altered so that opposite polarities of bias voltage are applied to the emitter and collector with respect to the n-p-n transistor. The point-contact transistor (usually p-n-p) is not recommended because it is not stable in the grounded-emitter amplifier circuit.

### Modifications for the CK722

To use the more popular CK722 p-n-p junction transistor, the following circuitry changes should be made:

1. Reverse the polarity of the B battery so that the −7.5-volt terminal connects to the output transformer.

2. Remove the ground connections from the transistor emitter and from the B battery tap. Reconnect the ground to the negative terminal of the B battery.

3. Remove the R1 connection to the output transformer and reconnect it to the positive pole of the B battery.

4. Connect the emitter to the −1.5-volt terminal of the B battery.

**Parts for tube-transistor radio**

**Resistors:** 1—1,200, 1—4,700 (see text), 1—2 megohms, ½ watt; 1—100,000 ohms, potentiometer.

**Capacitors:** 1—50 $\mu\mu$f, ceramic variable; 1—250 $\mu\mu$f, mica; 1—350 $\mu\mu$f, variable (larger section of conventional two-gang tuning capacitor can be used); 1—.001 µf, mica; 2—4 µf, G-E Tantalytic (if physical size is not important, a low-voltage paper capacitor of 1 µf or larger can be used).

**Miscellaneous:** 1—Ferri-Loopstick or equivalent; 1—L2, 6 or more turns wound adjacent to ground end of loopstick coil (see text); 1—3:1 audio transformer; 1—size D flashlight cell; 1—tapped 7.5-volt radio C battery (Burgess 5540 or equivalent); 1—CK6088 (Raytheon subminiature); 1—n-p-n junction type transistor (Texas Instrument type 200); 1—phone jack.

The purpose of these modifications is to bias the elements of the p-n-p transistor with the same voltages as the n-p-n unit shown in the schematic, but with opposite polarities. The counterpart to this situation does not exist with tubes; the applied d.c. plate voltage must be positive with respect to the cathode. It is possible that the experimenter might feel more at home with the n-p-n transi r because its base and collector are polarized exactly as the corresponding elements of the tube, the grid and plate, respectively.

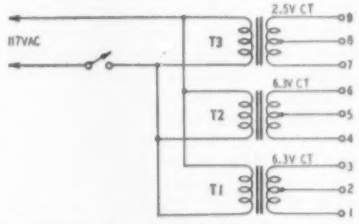
The audio transformer provides an approximate impedance match between the transistor collector circuit and the headphones. A fair degree of performance may be obtained by inserting high-impedance headphones directly in the collector circuit if it is desired to eliminate the transformer in the interest of miniaturization. END

# A.C. VOLTBOX

By RUFUS TURNER

ALL experimenters have occasional need for a source of variable low-voltage, high-current a.c. Common applications include tube heating, relay operation, experimental rectifier type bias supply, line-frequency signal voltage for bridge tests and impedance measurements, low-range a.c. voltmeter calibration, and control voltage in phase-operated electronic devices. Not all experimenters can afford Variacs.

A step type a.c. voltbox can be constructed, using three or more small surplus filament transformers, as shown in the diagram. These transformers are inexpensive and a number of voltages in closely spaced steps can be obtained. It is not necessary to stick to the secondary voltages shown in the diagram but I found that two center-tapped 6.3-volt units and one center tapped 2.5-volt unit provide a wide combination of output voltages. The various separate voltages are obtained




**Schematic diagram of the a.c. voltbox.**

by connecting the secondaries or halves of secondaries in series, either adding or opposing. As can be seen in the table, the three transformers specified provide any one of 22 voltages ranging from 0.65 to 15.1.

The voltbox may be assembled in a small metal utility box. The transformer secondary leads are connected to nine front-panel insulated binding posts, as indicated in the diagram. The various output voltages are obtained by connections to these terminals, as detailed in the table. Construction may be simplified and the size of the unit reduced greatly by using a single transformer with multiple secondary windings, instead of three separate transformers.

**TERMINAL CONNECTIONS**

| Output Voltage | Connect Terminals | Output Terminals |
|---|---|---|
| 0.65 | 3 to 9 | 2 and 7 |
| 1.25 | | 7 and 8 |
| 1.90 | 3 to 9 | 2 and 8 |
| 2.50 | | 7 and 9 |
| 3.15 | | 1 and 2 |
| 3.80 | 3 to 9 | 1 and 7 |
| 4.40 | 3 to 7 | 2 and 8 |
| 5.05 | 3 to 9 | 1 and 8 |
| 5.65 | 3 to 7 | 2 and 9 |
| 6.30 | | 1 and 3 |
| 6.95 | 3 to 4 and 5 to 9 | 1 and 7 |
| 7.55 | 3 to 4 and 5 to 7 | 2 and 8 |
| 8.20 | 3 to 4 and 5 to 9 | 1 and 8 |
| 8.80 | 3 to 7 | 1 and 9 |
| 9.45 | 3 to 4 | 1 and 5 |
| 10.10 | 3 to 4 and 6 to 9 | 1 and 7 |
| 10.70 | 3 to 4 and 5 to 7 | 1 and 8 |
| 11.35 | 3 to 4 and 6 to 9 | 1 and 8 |
| 11.95 | 3 to 4 and 5 to 7 | 1 and 9 |
| 12.60 | 3 to 4 | 1 and 6 |
| 13.85 | 3 to 4 and 6 to 7 | 1 and 8 |
| 15.10 | 3 to 4 and 6 to 7 | 1 and 9 |

This procedure must be followed to polarize the transformers correctly: Connect terminals 3 and 4 together. Check voltage between terminals 1 and 6—the voltage should be 12.6, since the secondaries should be series-aiding. If it turns out to be zero or some value lower than 6.3, the secondaries of T1 and T2 are bucking and the primary leads of T2 must be reversed. Connect terminals 6 to 7 and measure the voltage between 4 and 9—this voltage should be 8.8. If it is somewhat less than 6.3, the secondaries of T2 and T3 are bucking and the primary leads of T3 must be reversed.

If a single transformer with multiple secondaries is used, polarizing must be accomplished by manipulating the *secondary* leads, since there will be only one primary winding.

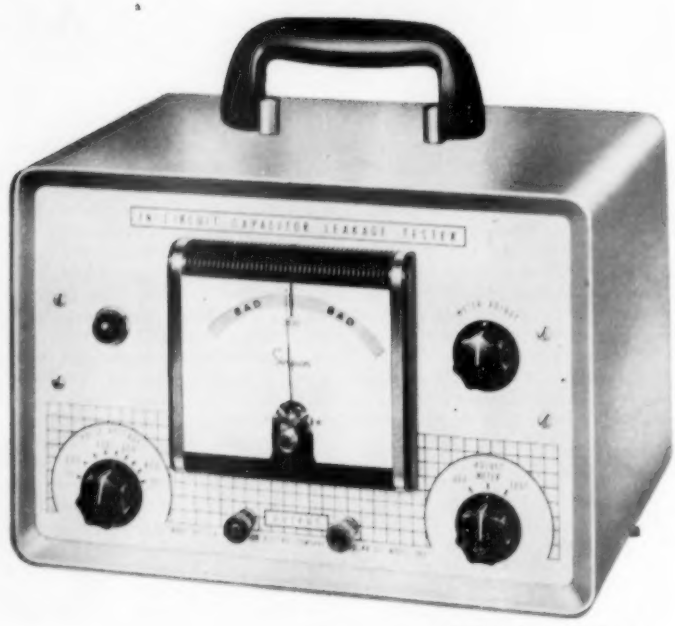
Although a voltbox of this type is not continuously variable, the output voltage steps are spaced closely enough to compensate for the lack of smooth variation. The use of "free-point" binding post terminals, rather than switching, reduces the complexity of the device. In most applications, one voltage will be used continuously for some time after its selection, so the use of jumpers between terminals should introduce no hardship.

Connect the voltbox to the 117-volt a.c. line through a fuse of around 5 amps. This prevents blowing the main fuses in the event of an overload or a short circuit. END

"You and your short cuts!!"

# New Test for Capacitor Leakage

*Dynamic characteristic of leakage resistance is basis for in-circuit capacitor checks*



Front view of the Simpson model 383.

By ROBERT G. MIDDLETON*

FOR years, the radio and TV service technician has dreamed of an instrument that could be applied directly to a fixed capacitor in a receiver circuit to determine whether or not the capacitor is leaky. The problem is illustrated in Fig. 1, which shows a capacitor (paper, mica or ceramic) shunted by circuit resistance R.

This capacitor may be used for interstage coupling or as a screen or a.g.c. bypass for example. When it develops sufficient leakage resistance ($R_{LK}$), circuit operation deteriorates or fails.

The problem is to find the presence of $R_{LK}$ when shunted by R. A new discovery, which is the basis of a pending patent application, discloses that leakage resistance is in general *a different type of resistance* from circuit resistance and can be distinguished by a definite test. Leakage resistance differs from ordinary circuit resistance in that in some forms it is unstable and nonlinear when tested dynamically with a pulse voltage.

These new concepts are not entirely simple, and the graphs in Figs. 2, 3 and 4 will serve to make them more understandable. The fixed capacitor whose leakage resistance is now causing trouble in the receiver was good when installed and the receiver operated satisfactorily. But after a period of service the initial high value of leakage resistance has gradually declined to the point where it causes trouble. The technician is concerned with this form of leakage resistance that usually drops during the life of the capacitor. This is an important point. There are other forms of leakage resistance such as that of a brand-new poorly made capacitor having a poor dielectric. Such a capacitor has a low value of leakage resistance that does not have the declining characteristic that makes possible the in-circuit type of leakage test.

*Chief field engineer, Simpson Electric Co.

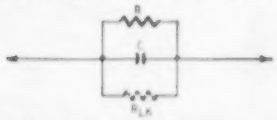



**Fig. 1—Leakage resistance $R_{LK}$ affects set operation and may be hard to detect.**

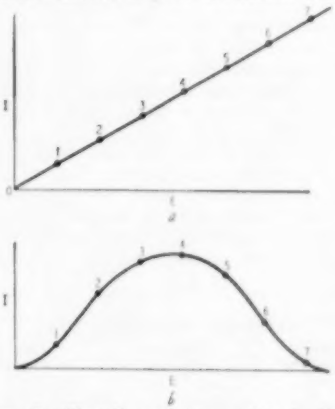


**Fig. 2—Circuit resistance (*a*) is linear but leakage resistance (*b*) is not.**

Fig. 2-a shows that circuit resistance is linear. The current through it is proportional to the applied voltage. But Fig. 2-b shows that leakage resistance may rise slightly at first and then fall off rapidly to a very low value as the applied voltage is increased. Fig. 3 illustrates another common form of leakage resistance. Curve A shows leakage currents when different test voltages were applied to a .002-$\mu$f 600-volt paper capacitor. This capacitor showed infinite leakage resistance when checked with an electric ohmmeter (v.t.v.m.) but leakage currents indicate resistance of 24 megohms at 100 volts and only 7.4 megohms at 200 volts. Curve B shows the result of similar measurements made on a .001-$\mu$f 600-volt mica capacitor that showed 2 megohms of leakage resistance on the ohmmeter. Incidentally, this characteristic is well known to experienced service technicians, and they do not rely on low-voltage ohmmeter tests.

Leakage resistance is often unstable, fluctuating or drifting when voltage is applied. Fig. 4 is the graph of measurements made on a .005-$\mu$f 600-volt paper capacitor. When the test voltages were first applied, the leakage resistance was low and then rose suddenly to a higher and more stable value. Initial currents rose to the high levels shown, then fell to lower and more stable values.

By using these characteristics of leakage resistance we can detect it by applying a low voltage—1 volt or so—across the capacitor and measuring the current that flows and then increasing the voltage and again measuring the current. E/I will be the same in each case if there is no leakage resistance but it will differ if leakage resistance is present. See Fig. 5. Unfortunately, the heavy current flowing at 600 volts will often burn out the circuit resistance so other methods must be used.

## The pulse test

Capacitors in pulse circuits fail sooner than those in sine-wave or d.c. serv-

ice, so a pulsed voltage should be ideal for such a test. Furthermore, a pulse may have a peak voltage as high as desired with a short duration. The small amount of energy in the pulse may be integrated for definite tests without endangering circuit resistances. By substituting a narrow pulse for the

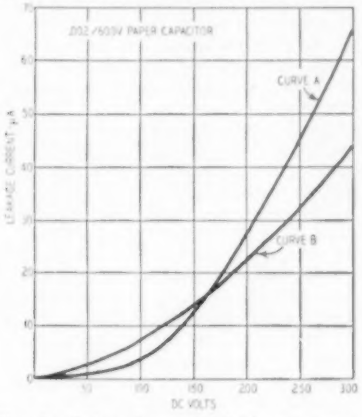



**Fig. 3—Other forms of leakage resistance.**

battery in Fig. 5 we can briefly charge capacitor C to 600 volts without causing sufficient current flow to overheat resistor R across the capacitor under test. If the pulse (dashed lines in Fig. 6) is generated by a very low impedance source, the capacitor will be raised instantaneously to the peak voltage of the pulse, irrespective of the value of R. Note that the average value of the pulse, as generated, is zero. This means, if the pulse is displayed on the screen of a scope with a sawtooth sweep, that the positive area of the pulse above the zero-volt line will be exactly equal to the negative area of the pulse below that line. The meter is not deflected. But, if leakage resistance $R_{LK}$ is present, circumstances are altered. The nonlinear characteristic of $R_{LK}$ causes partial rectification of the pulse voltage and its average value is no longer zero. A d.c. microammeter in series with the pulse circuit will be deflected. The pulse voltage (solid lines in Fig. 6) does not rise to its 600-volt peak because $R_{LK}$ decreases to a small value as the pulse voltage rises above a certain point. This nonlinear increase in current through $R_{LK}$ is sufficient to deflect the meter.

After pulsing, the value of $R_{LK}$ may or may not return to its initial value. When a d.c. voltage is connected in series with the microammeter (Fig. 7) the value of current may change only during pulsing (dynamic testing), but it may in addition show a fixed change as indicated by a continuing greater deflection of the meter pointer after the pulse voltage is removed from the capacitor under test.

Sometimes the value of $R_{LK}$ increases when the pulse voltage is applied and remains at a higher value when the pulse voltage is switched off, but in most cases the change is to a lower value. This agrees with the earlier observation that capacitors which are failing in service have declining values of leakage resistance. But this is not the complete picture.

In practice the application of a high-voltage pulse sometimes serves to "burn out" the leakage resistance and to make a good capacitor out of a bad one (Fig. 8). More often, however, the leakage resistance is changed to a much lower value or a dead short and the capacitor is left in worse condition than before. A good capacitor is completely unchanged by application of the test pulse.

Some capacitors whose leakage resistance has dropped to a low value—to several megohms, for example—may produce relatively small deflection of the meter until a certain critical value of pulse voltage is reached, such as 300, 400 or 600. Then the capacitor may break down suddenly, accompanied by a snapping sound from within and a violent kicking of the meter pointer. A capacitor that is not failing in service, however, maintains its original characteristic and does not break down nor show a change in leakage current when pulsed at rated working voltage.

There is not necessarily any close correlation between the amount of deflection obtained on the meter for various values of $R_{LK}$. Thus, a capacitor having a relatively low value of leakage resistance may produce a much larger deflection on the meter than a capacitor having a high value of leakage resistance or vice versa. As a rough rule of thumb it can be stated that there is a tendency on the average for high values of leakage resistance (100 or 1,000 megohms) to produce less pointer deflection than low values of 100 or 100,000 ohms. Hence, it it desirable to use a meter of reasonably high sensitivity.

A 25–0–25-$\mu$a meter is satisfactory for general service work. However, more capacitors with high-resistance leakage can be detected with a 0.5–0–0.5-$\mu$a meter. The latter type costs more and is more expensive to use because auxiliary circuitry is required to protect it against current surges. In general service work a 50-$\mu$a zero-center meter is suitable.

A zero-center meter is needed because leakage resistance sometimes goes up instead of down when the capacitor is pulsed. The center line of the scale is marked GOOD, with BAD sectors on either side.

In operation, battery voltage E (see Fig. 7) is adjusted so the flow of current through the circuit brings the pointer up from the OFF position (about ¼ inch from center) to the reference or GOOD line. This permits the operator to determine readily whether there is a permanent change in effective circuit resistance when the circuit is pulsed. Then the pulse generator is started and the meter observed for a second or two. If the pointer moves down or up scale, the capacitor has appreciable leakage resistance. The pulse voltage is then switched off, and the meter is read again to determine whether the effective circuit resistance has changed permanently. This dynamic test is more definite than the static test.

In practice the simple functional diagram in Fig. 7 is not sufficient. Passage of the pulse through the meter produces only a momentary kick of the needle, so a series of pulses must be integrated for normal observation. The test current consists of both a.c. and d.c. so two electrolytic capacitors are connected back to back across the meter to integrate the pulses of the d.c. and produce a smooth normal meter de-

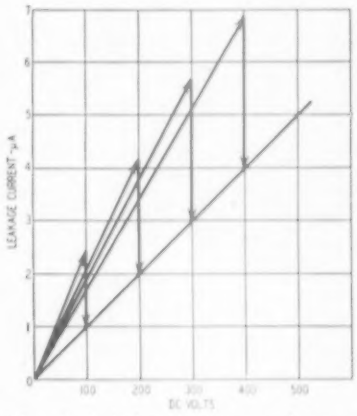



**Fig. 4—Drifting leakage resistance.**

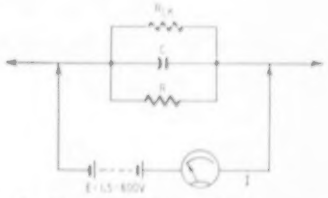



**Fig. 5—Varying voltage shows presence and magnitude of leakage resistance.**

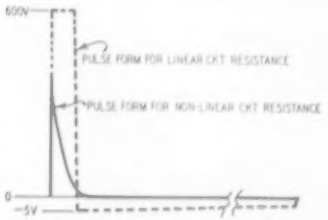



**Fig. 6—Leakage resistance affects the pulse shape and peak output voltage.**

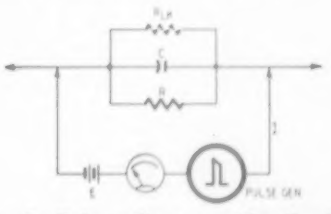



**Fig. 7—Pulse voltage provides the dynamic test for leakage in capacitors.**

flection. The capacitor values are determined by the internal resistance of the meter. The 2,000-$\mu$f values are suitable for a standard 25–0–25-$\mu$a meter.

After the pulse is switched off, the meter bypasses and integrators must also be switched out of the circuit. If the meter has been deflected to the end of the scale, considerable time will be required for the pointer to return to the reference position. Accordingly, the switching system of the instrument must open the meter circuit and also short-circuit and discharge the large electrolytic capacitors in preparation for the next test.

### A practical instrument

The new Simpson model 383 In-Circuit Capacitor Leakage Tester uses this principle for checking leakage in capacitors. Its circuit is shown in Fig. 9.

It will be apparent that the varying conditions of test are such that a useful instrument must provide a very-low-impedance pulse. A cathode circuit, for example, has a very low effective resistance and cannot be raised to peak pulse voltage unless the internal impedance of the pulse generator is quite low. Hence, a 2050 thyratron pulse generator is utilized. The repetition rate of the pulser is fast enough to provide satisfactory integration at 600 volts.

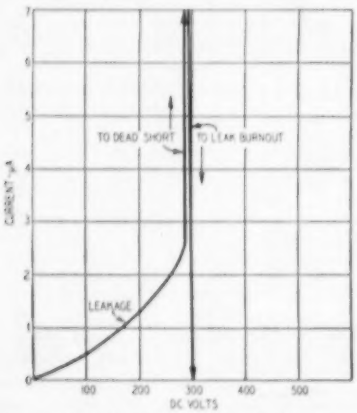



**Fig. 8—Pulse voltage may break down leaky capacitors or cure the trouble.**

The rise time of the test pulse is also a very important consideration. Although the internal impedance of the pulse generator may be low, the rise time must be fast since a capacitive storage source is used in the generator. It also is desirable because leakage resistance is more unstable in the presence of fast rise. The Simpson model 383 provides a rise time of 1 $\mu$sec.

The reader will see that, since the tester operates upon the basis of unstable resistance characteristics, that the instrument might serve likewise to locate noisy resistors in receiver circuits. It can. When the test leads are applied across a noisy resistor and the pulse voltage is applied, the pointer responds by moving off into the BAD sector. Thus a BAD indication may be the result of either a bad resistor or a bad capacitor in the circuit. But in most practical situations the capacitor is faulty.

Since radio and television circuits have many branches, the question might arise as to whether the operator can know exactly which capacitor is really being tested when a BAD indication is observed. The answer to this is that even a small value of resistance between the point of pulse application and the capacitor under test reduces the pulse voltage to such a small value that a test is not obtained. This is a consequence of the fast rise of the test pulse. Hence, few situations are encountered in practice wherein the operator is not certain which capacitor in the circuit chain is the bad one.

The energy contained in the test pulse, while small, is not entirely negligible in all cases and certain minimum precautions must be taken in its use. In the first place it gives the operator an uncomfortable shock if contacted. HANDS OFF is the rule while the pulse voltage is on. Also, the pulse has sufficient energy to damage video detector crystals and to burn out 1.5-volt tube filaments. Hence, you must not apply pulse voltage across crystals and you must remove the tubes from battery portable sets before testing the filament bypass capacitors.

There are some limitations in the practical application of the instrument. For example, when the capacitor under test is shunted by a coil, the effective circuit resistance becomes so low that the microammeter cannot satisfactorily monitor changes. The 383 cannot be used satisfactorily in this application. However, the instrument is useful in checking leakage resistance in other circuits where the value of the leakage resistance is several hundred times greater than the value of the shunting circuit resistance.

The receiver must, of course, be turned off when testing capacitors, as d.c. voltage from the receiver can back up into the microammeter and burn it out. It is also advisable to avoid damage to the thyratron by giving it a few seconds to warm up before the pulse generator is switched on. Likewise, the instrument should be used at line voltages of approximately 117 to obtain normal life expectancy from the thyratron. Do not operate the instrument continuously across a dead short circuit. This damages the cathode coating and the thyratron.

The OFF position of the switch opens the primary circuit of the power transformer and the battery circuit to the meter. In the second position (ADJUST METER), the battery circuit is completed so that the meter can be set with the 500-ohm potentiometer; plate power is applied to the thyratron, but the grid circuit is biased off and the tube does not fire. The meter bypass capacitors are shorted.

In the third (TEST) position of the switch, the bias on the thyratron is reduced to a value previously set by adjustment of the 5,000-ohm potentiometer and pulses are generated across the 600-ohm load. The integrating capacitors are connected across the meter. According to the setting of the thyratron bias control, indicated on the scale plate, the operator can adjust the peak voltage of the pulse from approximately 15 to 900.

If one side of the capacitor under test should be connected to the chassis of the receiver, full pulse voltage is applied by connecting the LOW terminal to the receiver chassis. In most cases, neither side of the capacitor under test is connected to the receiver chassis so the test leads are applied across the capacitor without regard to which side is LOW or HIGH.

The operator who uses the model 383 for the first time will be surprised at the number of leaky capacitors present in older receivers, which nevertheless are not causing trouble because they are operating in noncritical circuits or because their leakage resistance has not yet fallen to a value which impairs circuit operation noticeably. It is not the purpose of this article to assert whether such leaky capacitors should be replaced. END

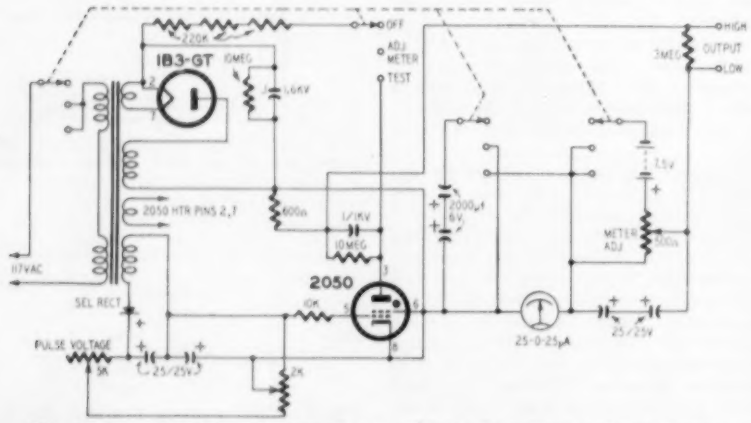


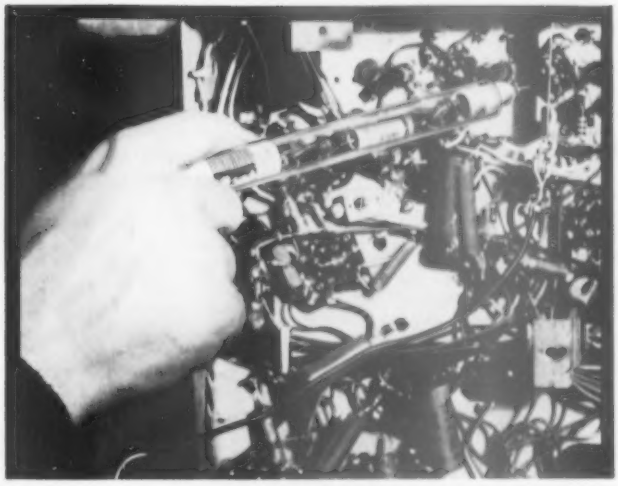

**Fig. 9—Circuit of the Simpson 383 In-Circuit Capacitor Leakage Tester.**

*High-gain unit permits measuring signal directly from television tuner*

Closeup shows components in probe.

# Transistor Demodulator Probe

By HOMER L. DAVIDSON



Troubleshooting with transistor probe.

THE transistor demodulator probe (see photos) was designed and constructed so greater amplification could be obtained when shooting video trouble in television receivers. Most oscilloscopes do not have enough vertical amplification to display the video signal properly as it appears at the tuner. Generally the signal is amplified enough in the first and second video i.f. stages but this does not always indicate the source of trouble. So from this small want a transistor was chosen for an amplifying stage and placed in a probe type tester.

There are not too many components in this small unit. The input section (see diagram) consists of a 1N34 crystal detector stage with associated resistor and capacitor. Perhaps it would have been best for the demodulator or crystal unit to have been constructed in a metal instead of plastic container but results were gratifying and no 60-cycle or stray signals were picked up by the probe. From the detector the signal is coupled to the CK722 transistor amplifier. The bias return resistor is 220,000 ohms, obtained by placing a 500,000-ohm variable resistance in the circuit and varying it for best results. The 10,000-ohm output resistor was obtained in the same fashion. When doing this, place a 0–10-ma meter in the output circuit and do not permit the CK722 transistor to draw more than 5 ma.

It is best to construct the transistor demodulator probe in a breadboard style first before final assembly. By doing this the unit can be hooked to a working television receiver and oscilloscope. With the probe in operation it is very easy to vary both the bias and load resistor for best results. It was found that a lot of noise was amplified when the resistors were varied for greatest amplification. So a happy medium was set where two variable resistors permitted high amplification and low grass or noise as seen on an oscilloscope.

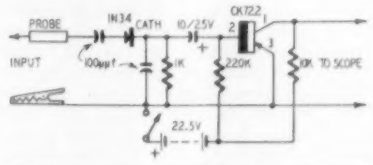
After best results were obtained all the leads and components were mounted closer together. The components were laid in a line and soldered so that they didn't occupy more than 10 inches. They were mounted so that at any one point along the assembly they could easily be pushed into the 1-inch plastic tubing.

The tip of the demodulator probe was the cap of a nose-drop bottle. A small hole was drilled through it so that a 1-inch 6-32 bolt and nut could enter. The small bolt was ground to a sharp point at one end.

Solder the 100-$\mu\mu$f capacitor to the bolt before the parts are placed in the container. After the components are inserted, place the cap in the plastic end and glue it into place. The small 6-32 nut screwed on the outside of the cap forms a sturdy tip probe.

A small battery is at the rear of the demodulator probe. On the positive side of the battery a s.p.s.t. slide switch is soldered directly to it and a small slot is cut into the tubing so the switch could be fitted. The shielded mike cable is then soldered into place and two small lugs are soldered to the other ends.

Comparison tests were made with a commercial type demodulator probe and the small transistor demodulator. The amplification obtained was about 10 times greater than that of the commercial probe. This was plenty of amplification to measure the signal directly from the television tuner. Passing through each stage, the oscilloscope gain should be kept in its lowest position. END




**Parts for demodulator probe**

1—1,000-ohm resistor, ½ watt; 1—10,000-ohm resistor, ½ watt; 1—220,000-ohm resistor, ½ watt; 2—100-μμf capacitors, postage type; 1—10-μf capacitor, 25 volts, electrolytic (small as possible); 1—1N34 detector; 1—CK722 transistor; 1—s.p.s.t. slide switch; 1—22.5-volt battery, less than 1-inch diameter; 1—2 feet of microphone cable; 1—alligator clip; 1—1-inch diameter plastic container, 10 inches long; 1—bottle cap for probe tip (see text); 1—6-32 bolt, 1 inch long, and nut.

# TRANSISTOR PERFORMANCE

*Analyzing characteristics; the tetrode transistor and high-frequency operation*

By EDWARD D. PADGETT

TEST methods and specifications are necessary for proper evaluation of transistors because they are temperature-sensitive devices (see Practical Transistor Tests, July, 1955) whose characteristics and parameters vary over wide ranges. Consequently, the operating point of a transistor will vary unless it is "stabilized."

Vacuum tubes operate with constant plate and grid voltages, while transistors operate with constant collector voltage and constant base current. And, like a tube, a transistor operates along a load line. The slope of the collector load line is $1/R_L$. The operating point of a transistor can be established either with fixed or self bias. For fixed bias (fixed base-current bias) operation, resistor $R_B$ is connected between the supply voltage and base electrode (Fig. 1). This resistor should be large enough so it will supply a *constant* current to the base.

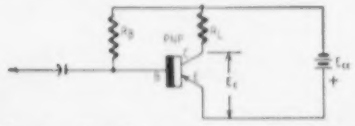



**Fig. 1—Circuit operates on fixed bias.**

When the operating point is determined by self bias, resistor $R_B$ is connected between collector and base electrodes (Fig. 2). The base biasing current is determined by Ohm's law.

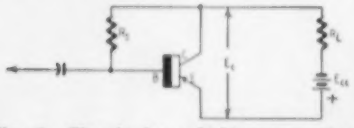


**Fig. 2—Circuit for self-bias operation.**

That is, base current $I_b$ is determined by collector operating voltage $E_c$ and $R_B$. If $E_c$ is 10 volts and $R_B$ is 400,000 ohms, the base current is $I_b = E_c/R_B = 10/400{,}000 = 25$ microamperes.

The collector load line (d.c. load line) is determined by the values of collector supply voltage $E_{cc}$ and $R_L$ (Fig. 3). The bias line is included since the base current is known (from the Ohm's law example) for various values of $E_c$ and $R_B$. The d.c. operating point is given by

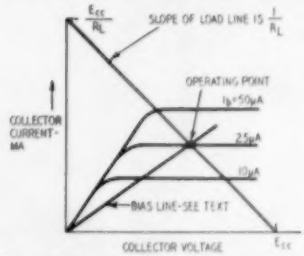



**Fig. 3—Typical collector load line.**

the intersection of the biasing and collector load lines.

Since transistor characteristics vary with temperature, a shift in the $I_c$–$E_c$ curves occurs; that is, the spacing between curves changes with temperature. We know that transistor parameters such as current gain and output impedance vary with temperature (also, transistor parameters vary because of small changes in physical conditions occurring during the manufacturing process). This means that the transistor operating point shifts when the spacing between $I_c$–$E_c$ curves changes.

All the above deviations contribute to variations in collector current and voltage from unit to unit of a given transistor type. This can lead to a serious situation unless design practices are good. For example, suppose that a defective collector load resistor decreases in value. If this happens, the collector current can increase beyond the rated value. The excessive dissipation would ruin a transistor (even though the collector voltage is well within safe limits). Similar damage could occur if the leakage currents ($I_{co}$ or $I_{cbo}$) increased beyond safe limits because a customer left his transistor radio in the hot sun at the beach (and this will happen, sure as shooting!!).

Consequently, adequate methods for *stabilizing* the operating point must be used if transistors are to be regarded as reliable electronic devices. Fortunately, several methods of stabilization are available, and are simple to apply.

Stabilization is obtainable in several ways: with current feedback, combinations of current feedback and fixed bias or current and voltage feedback. Combination current and voltage feedback

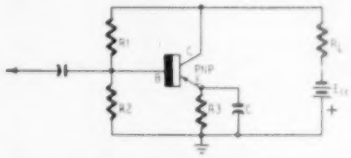



**Fig. 4—Stabilization with a combination of current and voltage feedback.**

is shown in Fig. 4. Current feedback is obtained from emitter resistor R3 and resistor R2 connected between base and ground. Resistor R2 provides reverse base bias; R1, between collector and base electrodes, supplies voltage feedback. Self-biasing resistor R1 (like $R_B$ in Fig. 2) supplies forward base bias to establish the operating point.

R. F. Shea[1] has established a mathe-

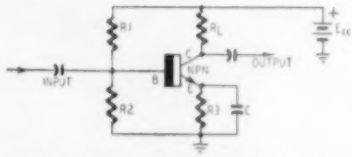



**Fig. 5—Circuit for determining stabilization of transistor amplifiers.**

matical criterion for stabilization of transistor amplifiers. Fig. 5 shows an R-C-coupled amplifier. It will be stabilized if

$$S_f = \frac{\Delta I_c}{\Delta I_{co}} = \frac{1 + \frac{R3}{R1} + \frac{R3}{R2}}{\frac{1}{1+\beta} + \frac{R3}{R1} + \frac{R3}{R2}}$$

where $\beta$ is the current gain of a grounded-emitter stage; $S_f$ is an expression of the ratio of changes in collector current $\Delta I_c$ and leakage current $\Delta I_{co}$. The numerical value of $S_f$ should be small (in general, values from about 1 to 7 give satisfactory stabilization).

[1] R. F. Shea, *Principles of Transistor Circuits*, p. 103, Wiley & Sons, 1953.

*Courtesy Germanium Products Corp.*

**Internal construction of the RDX-300-A (3N23-C) germanium tetrode transistor.**

Additional stability is obtained by *derating* the transistor (collector current and voltage reduced below rated values) and reducing the I²R losses in the stabilizing resistors.

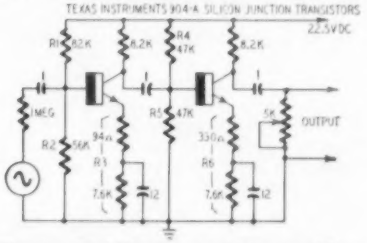



**Fig. 6—Stabilized transistor amplifier.**

To look at stabilization from a practical viewpoint, consider the following circuits: Fig. 6 shows a *stabilized* amplifier using hermetically sealed silicon junction transistors. In the first stage resistors R3 and R2 provide current feedback, while the *parallel resistance* of R1 and R2 controls the amount of stabilization. The *ratio* of R1 and R2 determines the operating bias.

A similar situation exists for the second stage: R6 and R5 supply current feedback, the parallel value of R4 and R5 controls the amount of stabilization, the ratio of R4 and R5 determines the bias. Also, the $S_f$ factor is small, and the supply voltage has been derated 25%.

The performance of this amplifier is better than many vacuum-tube amplifiers in several respects. The frequency response of a stabilized silicon junction amplifier, for two different ambient temperature conditions, is shown in Fig. 7. Fig. 8 shows an unstabilized amplifier for comparison with the stabilized unit. It is an R-C-coupled amplifier operating with fixed bias, with some degeneration present because of the resistors in the emitter circuits. The performance of this amplifier is unsatisfactory and unpredictable since it is unstabilized.

It is interesting to note that hermetically sealed type 904-A silicon junction transistors (Texas Instruments) show an increase in gain at higher temperatures (even when a high percentage of humidity is present) as shown in Fig. 7.

The low-frequency response of an R-C-coupled amplifier depends on the values of coupling capacitor, coupling resistors and the load resistor (Fig. 9).

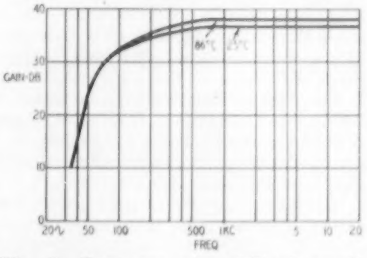



**Fig. 7—Response of stabilized amplifier using silicon junction transistors.**

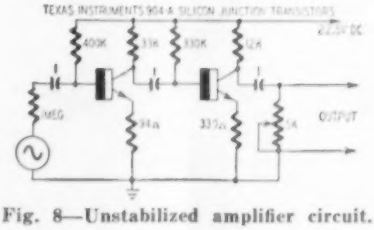



**Fig. 8—Unstabilized amplifier circuit.**

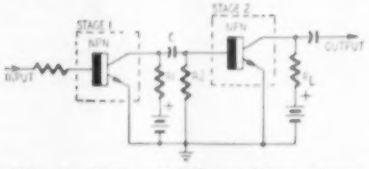



**Fig. 9—R-C-coupled amplifier stage.**

The coupling resistors reduce current amplification at lower frequencies because the input (base) resistance of most junction transistors (stage two) is small. Also, the impedance of the coupling capacitor is much greater than the input resistance of this stage at lower frequencies. For a bird's-eye view of this, assume coupling resistor R1 equals load resistor $R_L$. The frequency at which the response is 3 db down from the mid-frequency value is given by $f = \frac{1(R_i + R_L)}{(2\pi C)(R_i + R_L)}$. If C is 1 $\mu$f and R1 = $R_L$ = 10,000 ohms, the response is down 3 db at approximately 33 cycles.

Low-frequency transistor circuits are reliable and practical. In designing low-frequency amplifiers, it is convenient to have available some general "rules of thumb" to use a check. The *conductance* (and current gain) of the first stage should be large; this requires the use of a *grounded-emitter* stage. Sometimes a *grounded collector* (emitter follower, analogous to a cathode follower) is used as the first stage, especially if the generator (source) impedance is large. The grounded emitter is usually used for intermediate stages because the current amplification should be as large as possible.

The final stages require the use of power transistors or stages designed for *maximum power gain*. Single-ended or push-pull grounded-emitter power stages are used here. Sometimes the *grounded-base* configuration is used if the load impedance is large. Low-powered, hermetically sealed, germanium transistors suitable for this are the 2N34, 2N43A and 2N38. Suitable silicon transistors are the hermetically sealed 900 series of Texas Instruments. A satisfactory hermetically sealed germanium power transistor is the Minneapolis-Honeywell 2N57. A satisfactory hermetically sealed silicon power unit is the Texas Instrument type X-15.

The high-frequency response of transistor circuits is complex—it depends on solid-state parameters, collector-junction capacitance (area), phase shift and other variables. Consequently, high-frequency circuits are difficult to design and give less reliable performance. The high-frequency response of a transistor is described on most data sheets by the phrases "alpha cutoff frequency" or "beta cutoff frequency." This language describes when the high-frequency response is 3 db down from the mid-frequency value. For conventional low-powered junction transistors this point is somewhere between 1 and 9 mc.

### The tetrode transistor

One of the most promising devices for obtaining improved high-frequency operation is the tetrode transistor. The RDX-300-A (3N23-C) germanium tetrode, made commercially by Germanium Products Corp., Jersey City, N. J., is a hermetically sealed, n-p-n, grown-junction transistor with four electrodes.

A tetrode has an emitter electrode, a collector electrode and two base electrodes. The emitter and collector are n type material. Bases 1 and 2 (Fig. 10) are connected to opposite sides of a thin p type layer of germanium. The internal design of this tetrode is shown in the photograph.

There are several reasons for the improved high-frequency response of the n-p-n tetrode. This type design decreases the area of the collector junction, the use of thin layers of p type material increases the high-frequency range, reduction of the base resistance improves the high-frequency response.

In general, the operation of the tetrode transistor is as follows. Base 2 usually is used as the biasing electrode. Base 1 can be used in two ways. It can be the input electrode for grounded-emitter operation (Fig. 10). Or, if emitter input is used, base 1 is grounded (Fig. 11). When a satisfactory bias is applied to base 2, it confines the current flow to the neighborhood of base 1. This action reduces the intrinsic base resistance by an appreciable amount, increasing the upper-frequency response of the tetrode. Fundamentally, a tetrode is a "twin-based triode."

Selected RDX-300-A tetrodes have been used as sine-wave oscillators at frequencies near 100 mc. Also, they have been used as tuned amplifiers at frequencies near 50 mc. No doubt tetrodes will be used in future television sets as i.f. amplifiers.

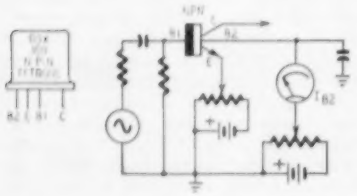



Fig. 10—Tetrode using base 1 input.

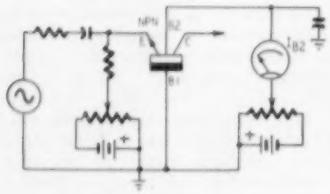



Fig. 11—Tetrode using emitter input.

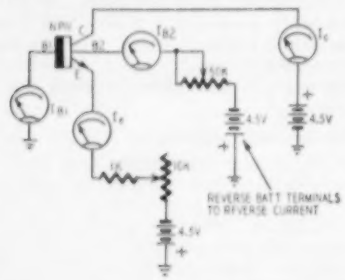



Fig. 12—Circuit used for measuring tetrode transistor d.c. characteristics.

The d.c. leakage currents $I_{cs}$ and $I_{cs_2}$ (emitter open and leakage measured from collector to base 1 and then from collector to base 2) of a tetrode must be less than 10 $\mu$a *each*, at room temperature, with 4.5 volts on the collector. In $I_{cs_2}$ leakage current (current between collector and emitter with bases open-circuited) should be less than 150 $\mu$a with 4.5 volts on the collector. These leakage currents are uncomfortably high in presently available tetrodes.

A circuit for the measurement of the d.c. characteristics of tetrodes is shown in Fig. 12. Although this circuit can be used to obtain the usual collector current *vs.* voltage characteristics, it can also be used to obtain other valuable data such as collector current *vs.* base 2 bias current (for a constant emitter current—1 ma—and collector voltage, 4.5). Such characteristics are similar in shape to series resonance curves (when circuit resistance is large) or somewhat similar in shape to the curve in Fig. 14.

The small-signal current gain $\beta$ of a tetrode may be obtained with the circuit of Fig. 13. In this case the tetrode is operated with $E_c$ at 4.5 volts, $I_e$ is set at $-2$ ma and an input frequency of 1 kc is used. Beta is read directly from the v.t.v.m. and is derived as follows:

$$\beta = \frac{di_c}{di_b} = \frac{\frac{E2}{10^3}}{\frac{E1}{10^6}} = \frac{(10^6)\ (E2)}{(10^3)\ (E1)} =$$

$$(10^3)\ (E2) = 10{,}000\ E2$$

since E1 was set at unity. For example, if the v.t.v.m. reads .004 volt, beta is 40.

Fig. 14 is interesting because it shows the variation in beta as the base 2 bias current is varied. The best r.f. performance is obtained when base 2 bias current is negative.

An experimental tuned high-frequency tetrode amplifier is shown in Fig. 15. The input signal (approximately 1 to 10 $\mu$a over the 2- to 50-mc range, depending on circuit and transistor parameters) is applied to base 1.

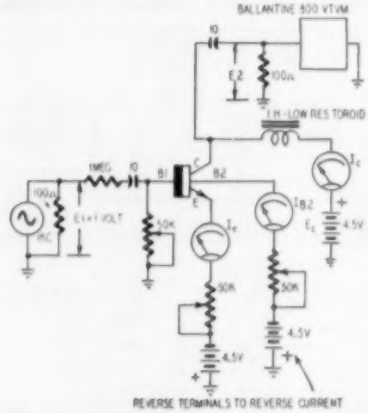



Fig. 13—Circuit diagram for measuring small-signal current gain tetrodes.

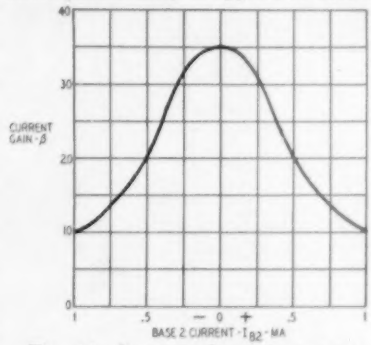



Fig. 14—Beta vs. base 2 current.

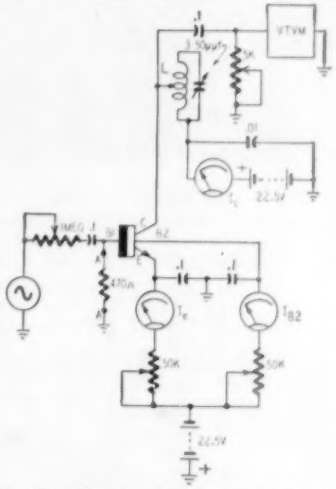



Fig. 15—Circuit of experimental tuned high-frequency tetrode amplifier.

Performance will be improved if the resistor at A–A in base 1 can be replaced with a coil of about 10 turns of No. 20 wire wound on a ferrite torroidal or bar core (obtainable from General Ceramic and Steatite Corp.).

The potentiometers in the base 2 and emitter leads establish a suitable bias (emitter current adjusted from 1 to 2 ma). Base 2 and emitter are bypassed to ground. The collector lead is attached to a tap near the center of output coil L. Experiment a little to find the best point. This coil consists of from about 8 to 10 turns (a few more at lower frequencies) of No. 20 wire wound on another miniature ferrite core (core diameter less than ½ inch). The tuning capacitor in the output circuit is adjusted for maximum output signal taken from the collector through a 0.1-$\mu$f capacitor. Collector current $I_c$ should not exceed 5 ma.

The configuration of Fig. 15 can be used as the basic circuit for interesting high-frequency experiments which will lead to the formulation of good design practices for u.h.f. transistor amplifier and oscillator circuits. Power gains of from 15 to 17 db at 5 mc and 8 to 10 db at 25 mc have been obtained from tetrode transistor amplifiers. END

# CONVERGENCE..

## *not impossible but difficult*

By HAROLD DAVIS

*Part I—Rainbows in black-and-white pictures; author suspects convergence trouble*

*MONDAY, 8:30 am*—One of my out-of-town dealers called. He had just received the first 21-inch color set to be shipped into this area.

"Come over, and let's play with it," he invited.

"*Play!*" The word was to take on new significance.

*11:05 am*—Harry and I pulled up in front of the store after a 40-mile drive. On the way over I had rehashed all I had read and heard in a two-day color school. I was pretty sure I could get it going.

When we arrived on the scene, the dealer already had the set unpacked. At a casual glance it looked like a regular 21-inch black-and-white set, except that the round tube with the masked top and bottom seemed to date it back a few years.

"Have you tried it?" I asked.

"We had it on a few minutes. It gets pictures, but everyone has a rainbow around his shoulders."

I reached down and snapped the on–off switch on the volume control. The set came on normally and, as the dealer had said, got pictures but with rainbows around the images.

I dropped the lid on the control box. It contained only two new controls, one marked HUE and the other COLOR. Turning these made little difference.

I opened the service manual I had brought along and read the instructions for black-and-white reception. The only variation from a regular set was that COLOR should be off.

I turned COLOR off, but the figures still had rainbows.

Going through the service manual carefully, I could find no mention of anything that had to do with color in black-and-white pictures. I decided that since the set was getting pictures, the tuner, i.f.'s, video and sound were O.K. That left the trouble somewhere in the color section. I reasoned that perhaps I could kill the color section by pulling out a tube or two and localizing the trouble.

*11:35 am*—Harry brought in the tool box and we started taking screws out of a metal back. When we got it loose, there was a noise like a spring flying out of an alarm clock. Harry was halfway to the door before I could tell him it was only some kind of safety switch held down by the back and which flew up when released. Nonchalantly, I worked the lever up and down with my hand.

Harry brought the "cheater" and I plugged it in. In a few seconds I heard a "Pfftt." The tube didn't light.

Back to the instruction manual and I found that the lever wasn't a switch, but a shorting bar that grounded the high voltage. The same job I had been doing with a screwdriver for years.

Harry reluctantly agreed to hold the lever down while I tried it a second time. Still no light on the picture tube. I was sure I had blown a high-voltage rectifier, which I was just as sure I couldn't obtain anywhere nearby.

I started looking for a way to get into the high-voltage compartment and was surprised to find no screws—just one small latch and the lid was released. However, there was another alarm-clock spring noise. This turned out to be a second shorting bar, put there, I suppose, further to discourage the careless from committing suicide.

Before I could start changing tubes, I discovered a blown fuse. It is in the high-voltage line, and blows if the shorting bar or bars are not held open when turned on. This is on page 17 of the instruction manual, I found out later.

I replaced the 0.45-amp fuse with a 0.5-amp unit and closed the lid on the lethal chamber. I then propped the outside shorting bar open with a piece of 2 x 4 about 3 feet long.

*12:15 pm*—The set came on. I turned it off and examined the tube location chart to see which tube to pull. It had more 6AN8's than my distributor carries in stock, so I decided on one of these.

I pulled one and turned the set back on. Still pictures with rainbows.

I pulled another and another without any effect on picture or rainbows. Harry started pacing the floor and I knew he was getting hungry.

"Go get yourself a bite to eat," I suggested, "while I read this instruction manual. There is bound to be something in here that tells how to get rid of rainbows."

*1:00 pm*—Harry returned, with a "what now?" expression on his face.

"I have decided that the trouble is either purity or convergence adjustments." I tried to say the two new words smoothly.

"Well," Harry shrugged his shoulders, "it could be either or both and I wouldn't know — I don't even know what you're talking about."

I decided we couldn't do anything about convergence without a dot generator, but we could check purity. I loosened four bolts that held the top of the cabinet and lifted this piece neatly off—to the amazement of the employes.

A ring around the bell of the picture tube held six round magnets described as MAGNETIC FIELD EQUALIZING ASSEMBLY. I set all these the maximum distance away from the tube as instructed. I set the contrast fully off and the brightness fully on. I started looking for the screen controls. Back in another place in the manual I read how

to take the control panel out and pull up a wooden wedge beneath it.

The control panel came out, but the wedge was wedged. I dared not use a screwdriver on this $1,000 piece of merchandise and, after all the strong-fingered guys in the place had failed to unwedge, I discovered a new trick of bumping the removable piece with the palm of my thumb. A few bumps on each side and it came up and out.

I found the control for RED SCREEN wrapped around AGC and turned it full on. The GREEN was wrapped around the BLUE, and I turned them completely off.

Going to the back of the set, I located the PURITY adjustment, a thing that looks like a positioning ring on a black-and-white set. I found it also just as aggravating to adjust. I turned the set on and had a pink screen with some blue and greenish shadows around the edge. By turning the purity ring I could vary these shadows more or less. I also adjusted the two tabs as with a centering ring. Playing with these a while to see their effect, I set them for the purest pink I could get. I then slid the yoke back and forth as instructed and left this at best setting. The individual magnets around the bell were manipulated out, in and turned to eliminate the fringes of blue-green color.

*1:45 pm*—I backed off and scrutinized the screen. I was fully satisfied that the purity was pure.

I brought up the GREEN SCREEN control and the screen took on a yellowish look. Bringing up the blue turned it into a dirty white. I balanced the three screens to get the whitest possible screen. A little color crept in around the edges which I balanced out with the field magnets.

As per instructions I turned up the contrast and tuned in a picture. I couldn't help but notice it still had rainbows.

I adjusted BLUE VIDEO GAIN and GREEN VIDEO GAIN. I still had rainbows.

As per instructions, I turned the brightness down low and adjusted BLUE BACKGROUND and GREEN BACKGROUND until the background seemed neutral. I still had rainbows.

Now, I'm not a "diddler," but I must be distantly related to one. I decided to risk one little turn on the convergence magnets I found installed on a ring wrapped around the picture-tube neck behind the yoke. The only effect I could see was that it possibly changed the color of the rainbows.

*3:30 pm*—Pinky Lee came on and would have been delighted with my new version of his checkered coat.

Harry started gathering up the tools and discovered we hadn't put the 6AN8's back. We installed them, but still had rainbows.

I looked at the convergence chassis hung on the side near the top of the cabinet and Harry read my mind.

"Why don't you turn one of those and see what happens?"

Without this suggestion I might not have, but I did it boldly and bravely.

I turned RED HORIZ AMPL. Nothing happened.

I turned RED VERT AMPL. Nothing happened.

I turned RED VERT TILT. Nothing happened.

I pulled out the RED connecting plug. I pulled out the GREEN. I pulled out the BLUE. Nothing happened.

I pulled the entire master plug to the convergence chassis. Nothing happened. We still had rainbows, and now there was one around Pinky's nose.

*4:15 pm*—I started thinking about my good black-and-white customers. To heck with color!

*10:30 pm*—I staggered homeward after having caught only half of my regular calls.

*Tuesday*—I spent the day catching up on regular work, but took time out to call on one of the local TV stations and borrow a dot generator and a color bar producer.

*Wednesday, 11:00 am*—Harry and I unloaded the color equipment and my tools and I began my first color convergence setup.

I hooked up the dot generator as best I could without instructions, which I hadn't picked up with the instruments. The instructions in the service manual said something about connections to the video—with a note that oscillators that produced r.f. should be connected to the antenna. This I did and tuned the machine to channel 6. I turned the channel selector to the same number and adjusted the fine tuning. By adjusting the contrast and tuning the generator I finally produced some dots but they were walking both ways.

"So," I said to myself, "no color sync."

I hooked up the color bar generator and turned everything on it. I managed to get some bars but they all looked alike. Breaking out my color book, I found a pattern that looked similar. The caption said it was a color bar pattern with the color section of the set inoperative.

I decided to call the engineer at the TV station, who had had some experience with 15-inch color sets.

*12:30*—I finally got him on the phone and told him of my predicament.

"What channel are you on?" he asked.

I yelled to Harry to see what channel the set was on.

"Channel 6."

"Channel 6," I repeated.

"Well," the engineer answered sympathetically, "The bar generator is crystal-controlled on channel 3."

"Well, that will probably take care of that, but what about the dot generator having no sync?" I asked.

"You know you have to supply sync to the dot generator." He phrased the sentence, it seemed, to give me a chance to cover my stupidity.

"No," I answered frankly, "I didn't."

"Yes," he continued, "take a piece of wire and run it from H SYNC on the generator to the yoke. Just wrap it around the yoke leads. Do the same for the vertical if you need it."

I thanked him and hung up.

The color bar machine was still hooked up, so I changed the channel selector to 3 and after manipulating the fine tuning carefully was able to produce a set of bars exactly like those described in the color book as "normal."

I then hooked up the dot generator as instructed and, sure enough, the dots were stable as a rock.

The dot generator had controls marked V BARS, H BARS, DOTS and CROSSHATCH. I tried them all out to see the effect. On V BARS there was another control that increased and decreased the number of vertical bars on the screen. The same for H BARS. When the control was set for DOTS or CROSSHATCH, the size of the dots and crosshatch could be regulated by increasing and decreasing the number of vertical and horizontal bars. I remember reading somewhere

that the small dots were better for convergence setups.

I readjusted the dots and observed the pattern. A few dots were white, but most had some color showing around the edges. The dots on the edges of the tubes were much out, showing little rectangles of red, blue and green. I couldn't help but notice that instead of getting *dots*, I got *squares*.

*1:00 pm*—I drank a Coke while reviewing the instructions. A note at the beginning said to check the high voltage and adjust it to 25,000 before beginning convergence.

I didn't have a high-voltage probe, so that let that out.

It also said to remove the high-voltage fuse and connect a 500-ma meter in its place to adjust the horizontal drive.

Having never been a switchboard electrician, I didn't have that either.

I knew the horizontal drive needed adjusting because the screen had that tell-tale white vertical line associated with many black-and-white sets when the horizontal drive is excessive.

I had to turn to the chassis layout to find the horizontal drive adjustment. It was just ahead of the high-voltage compartment, and I didn't cherish the thought of playing around so near 25,000 volts. However, I found that the control could be turned with a long plastic screwdriver like that used to adjust oscillator slugs. I backed off on it a bit and the line disappeared.

The set was still in good focus, so I reasoned the high voltage hadn't changed since it was originally set up.

*1:30 pm*—Convergence was now about to start.

I turned the red, green and blue HORIZ and VERT AMPL controls fully counterclockwise. These comprised half the controls on the convergence box. The others were marked TILT and PHASE. I set the VERT TILT to mid-range as instructed.

At this point the dots should have been displaced, but they were not like the diagram.

As per instructions, I attempted to converge the center dot using the knurled knobs on the convergence magnets. This wasn't too difficult. I now had a few white dots in the center becoming farther displaced as they neared the edges.

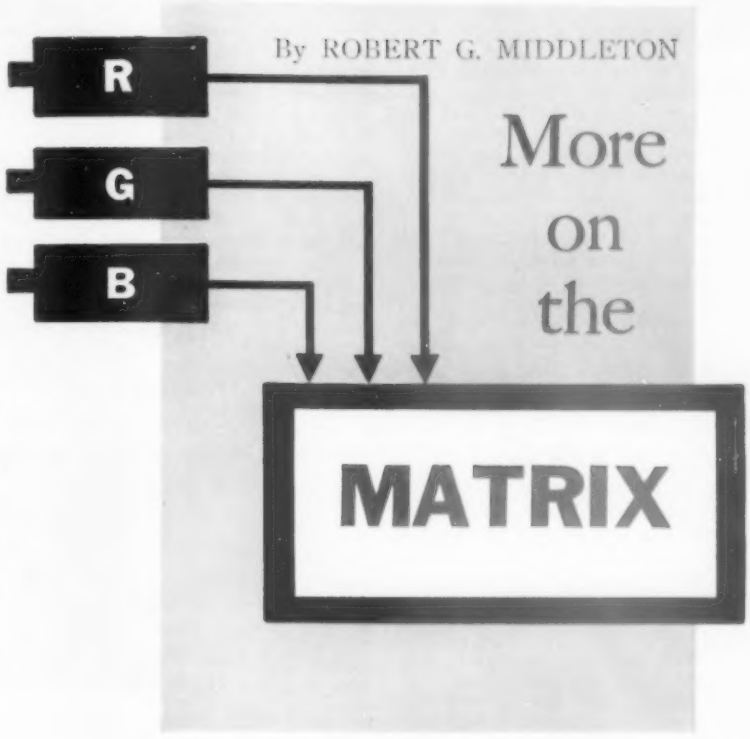
Turning the dot generator to STANDBY, I went through the purity, screen, video gain and background adjustments a second time.

*3:30 pm*—I was anxious to get to the dynamic convergence.

I rechecked the white dots in the center of the screen and following instructions I turned RED VERT AMPL full clockwise. As I did, I looked for movement of the red dot, but there was little. Other controls likewise had little effect. I pulled out the plug to the convergence box. It had little effect. The box just wasn't operating.

*4:30 pm*—My poor customers!

TO BE CONTINUED




By ROBERT G. MIDDLETON

# More on the MATRIX

*Matrix operation with balanced and unbalanced color signal; the color intensity control*

IN "How a Matrix Works" (August, 1955) we saw how a simple matrix works—one which largely uses the color TV picture tube itself as the matrix. The discussion thus far has been color signals. However, balanced color signals are *not* transmitted. They are obtained at the receiver by adjusting the color detectors so that the B − Y detector develops more output voltage than the R − Y detector. This adjustment is made with the *color balance* control, a service adjustment.

Before we consider the adjustment of the color balance control in detail, let us very briefly review the operation of a matrix. Fig. 1 shows a simple matrix arrangement illustrating the important points with which we are concerned:

1. The Y signal is applied to all three cathodes. When the cathodes only are energized, a black-and-white picture appears.
2. The output from the R − Y detector is applied to the red grid. When the red grid is energized, a red hue appears.
3. The output from the B − Y detector is applied to the blue grid. When the blue grid is energized, a blue hue appears.
4. Green (not transmitted as such) is obtained at the receiver by compounding R − Y and B − Y in the green matrix. The output from the green matrix is applied to the green grid. When the green grid is energized, a green hue appears.

Why is it that we see a black-and-white picture when the cathodes of the color picture tube are energized by the Y signal? It is because white (or grays) consists of red + green + blue

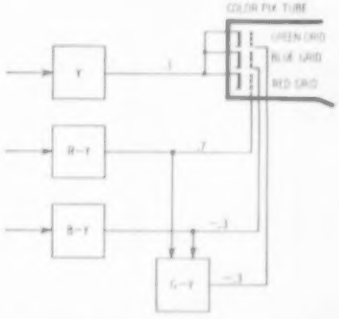



Fig. 1—A simple matrix arrangement.

and the screen and brightness controls for the three guns are adjusted so that, when the voltage on the cathodes of the picture tube goes up or down, the proportions of red, green and blue are such as to produce various shades of gray, or white when fully driven.

And why is it that we see a red hue on the screen when the cathodes are driven by the Y signal and the R − Y detector drives the red grid of the picture tube? It is because the red gun delivers more beam current when the grid and cathode are *both* driven, and more beam current means a resulting red tint on the screen of the color picture tube.

Further, what is the condition for the display of a *saturated* red hue on the screen? When a saturated red hue is processed by the receiver circuits, the signal appears on the screen of a wide-band scope as shown in the "red" bar of Fig. 2. The important thing to note here is that the red signal has a Y (luminance) component and a 3.58-mc (chrominance) component. The chrominance component is superimposed on the Y component—in other words, the average value of the chrominance component is zero (being an a.c. wave), so that the chrominance waveform is centered on the luminance voltage.

When this saturated color-bar signal proceeds through the receiver circuits, the two components divide, with the Y signal ending up on the cathodes of the color picture tube and the chrominance signal at the inputs of the R − Y and B − Y detectors. A little arithmetic here is very enlightening:

saturated red =
30% Y + 70% (R − Y) − 30% (B − Y) − 30% (G − Y)

Graphically, a saturated red signal appears as shown in Fig. 3. The color TV transmitter sends out information

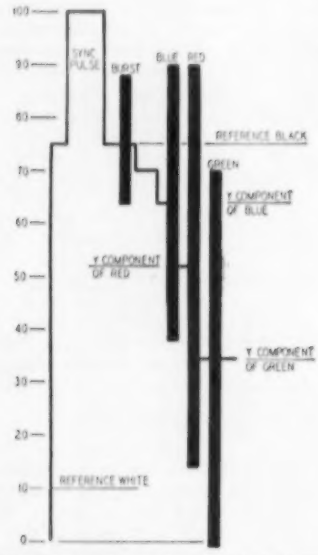



**Fig. 2—Waveform showing the voltages of 100% saturated red, blue and green.**

on a red field as follows: The R − Y signal is 70% of maximum, the B − Y signal is −30% and the Y signal is 30%. If we prefer, we can say that the −(B − Y) signal is 30% of maximum. *In other words, the minus sign indicates a phase reversal.* At the receiver, a phase reversal to the input of the B − Y detector results in negative instead of positive polarity output.

These waveforms are all demodulated patterns as seen at the outputs of the R − Y, B − Y and picture (Y) detectors, on a scope screen, and represent relative voltages.

One of the signals, G − Y, is missing from Fig. 3. This is explained in Fig. 4, where the G − Y matrix mixes R − Y with B − Y to produce G − Y. For saturated red R − Y = 70%, B − Y = −30%. The matrix adds:

−0.51(R − Y) =
−0.51 × 0.70 = −0.357
−0.19(B − Y) =
−0.19 × 0.30 = +.057

to produce: G − Y = −0.30

We end up as shown in Fig. 5 with grid and cathode of the red gun adding up to 100%, but with grid and cathode of the blue gun, and grid and cathode of the green gun subtracting to 0. So the red gun is running wide open and the blue and green guns are cut off—result, a saturated red hue. (See Fig. 6 for illustration of desaturated red display.)

## Unbalanced color signal

This discussion has been based on the color detectors delivering equal voltages when equal input signal voltages were applied. Unfortunately it is not quite this simple. There is a problem of

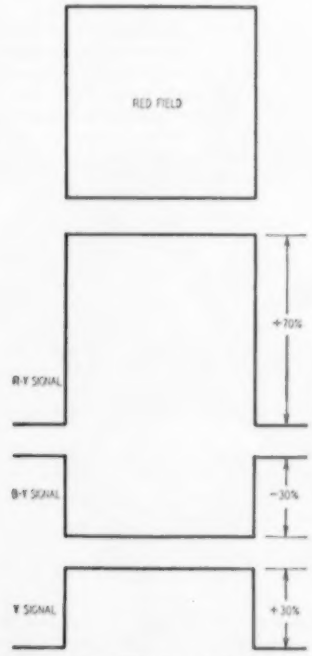



**Fig. 3—Color TV signal for red field.**

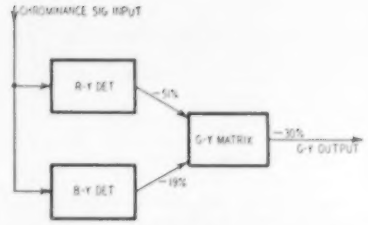



**Fig. 4—G − Y matrix input and output.**

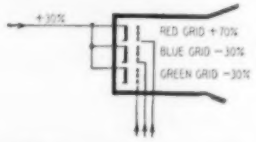



**Fig. 5—Voltages on grids and cathodes of color tube for saturated red signal.**

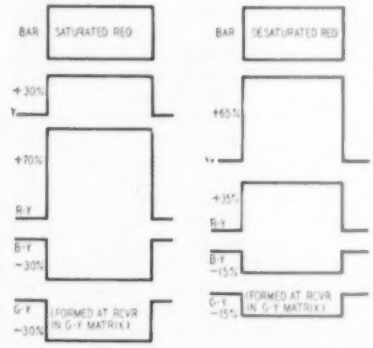



**Fig. 6—When saturated red bar is transmitted, B − Y and G − Y cancel against Y. When transmitting a desaturated red bar, partial cancellation occurs.**

overmodulation at the transmitter and hence we use what is termed *readjusted chrominance values.*

This means that both R − Y and B − Y are cut down somewhat. In fact, B − Y is reduced more than R − Y. In terms of relative voltages, R − Y is reduced to 87.7%, and B − Y to 49.3% of its original value. Thus, the transmitter does not provide color balance since R − Y is predominant. But this can be easily corrected at the receiver by adjusting the relative outputs of the color detectors so that the B − Y detector puts out more than the R − Y detector. A *color balance potentiometer* is provided for this purpose—it is an important service adjustment.

If you divide 87.7% by 49.3%, you will find that the unbalance amounts to 1.78 to 1, so that the output from the B − Y detector must be adjusted to be 1.78 times greater than the output from the R − Y detector. How is this done? Fig. 7 shows the R − Y output from a color bar generator. In similar fashion, the B − Y output can be switched on instead, and at equal voltage. For color balance, look at the square wave on the scope screen which

results from application of the R − Y signal, for example, and note its height. Then, check the output from the B − Y detector with a B − Y signal input and adjust the output for a square wave with a height 1.78 times the former. Then the color detectors will restore the required color balance. (See Fig. 8.)

This is a process which is analogous to pre-emphasis and de-emphasis in FM transmission.

The color detectors will not operate properly unless the *color phase control* has been properly set. How do we do this? There are several ways but, since we are working with a scope at the color detectors, here is the best way. Apply an R − Y signal to the input of the receiver and connect the scope at the output of the B − Y. Turn the color phase control until the voltage of the square wave on the scope screen drops to zero. Then, cross-check the operation by applying a B − Y signal to the input of the receiver and connect the scope at the output of the R − Y detector. Again, a zero square-wave voltage should result. If not, there is circuit trouble present, such as a faulty 90° phase-shifter adjustment or leaky capacitors.

Unless the 3.58-mc color subcarrier

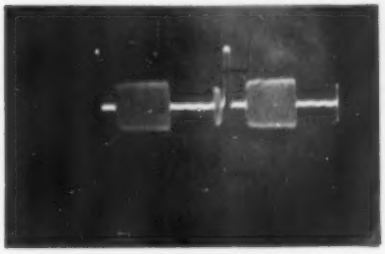


**Fig. 7—Appearance of R – Y on a wide-band scope, from color bar generator.**

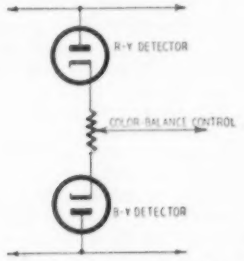



**Fig. 8—Color balance control, a simple gain control that permits the technician to adjust output from the detectors.**

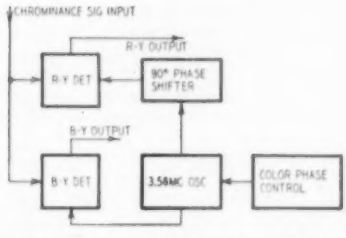



**Fig. 9—Diagram shows relationship of 3.58-mc oscillator to other circuitry.**

(Fig. 9) is inserted into the chrominance signal in proper phase, the detectors will not demodulate on the R − Y and B − Y axes. The R − Y output will contain B − Y contamination and the B − Y output will contain R − Y contamination. To demodulate along the correct axes, the color phase control must be adjusted properly with exactly 90° of phase shift between the local subcarrier oscillator and the R − Y detector.

This procedure assumes that you have a standard NTSC bar generator. If you are using a keyed rainbow generator, you usually cannot obtain individual R − Y and B − Y signals, so that the output from the detector contains varying outputs of other signals also (Fig. 10). In such case, you must count bars until you come to the R − Y bar and adjust the color phasing

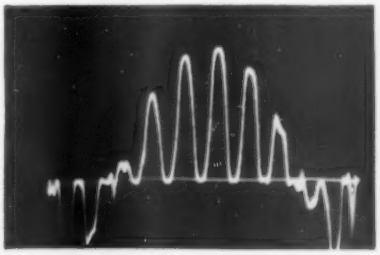


**Fig. 10—Keyed rainbow signal at output of color detector, or the G – Y matrix.**

control to produce zero output from the B − Y detector. Likewise, to cross-check you must count bars until you come to the B − Y bar and connect the scope at the output of the R − Y detector to see whether the B − Y bar voltage is practically zero (as it should be).

This brings us to the G − Y matrix. How shall we tell whether the G − Y matrix is operating correctly? Remember this important fact: The matrix responds to applied signals like the color detectors. When a keyed rainbow signal is applied to the input of the color receiver, the G − Y bar will appear at maximum if the G − Y matrix is operating correctly. Or, suppose that we are using a standard NTSC bar generator which provides a G − Y ∠90° signal. If we switch on this G − Y∠90° signal, the G − Y matrix responds with practically zero output. In other words, the G − Y matrix nulls on a G − Y∠90° signal, just as an R − Y detector nulls on a B − Y signal.

Having checked the G − Y matrix for either maximum output on a G − Y keyed rainbow signal or for zero output on a G − Y∠90° signal, the voltage value of the output can be checked, for example, on a green bar signal. When a green bar signal is applied to the input of the receiver, the G − Y output voltage should be 41%; when a red bar signal is applied it should be − 30% and for a blue bar signal − 11%. Remember if positive voltages go *up* on the scope screen, negative voltages go *down*. Adjust the vertical gain control of the scope so that the value of the signal can be counted in terms of squares.

Here are the relative output voltages from the R − Y detector and the G − Y matrix for some common colors:

| | | |
|---|---|---|
| red: | R − Y, | +70% |
| | G − Y, | −30% |
| green: | R − Y, | −59% |
| | G − Y, | +41% |
| blue: | R − Y, | −11% |
| | G − Y, | −11% |
| yellow: | R − Y, | +11% |
| | G − Y, | +11% |

## Obtaining 100% saturated colors

Although readjustment of chrominance values at the transmitter or generator results in a signal which does not have 100% saturated colors, it is possible to obtain true 100% saturated colors at the receiver by adjusting the color intensity control.

Chrominance values at the transmitter are adjusted by reducing R − Y to 0.877, and B − Y to 0.493 of its original value. *Y is not modified.* At the receiver, the luminance and chrominance signals are separately processed. The output from the Y amplifier is applied to the cathodes of the color picture tube. In the chrominance section of the receiver, correct color balance is first obtained by adjusting the B − Y detector for an output 1.78 times that of the R − Y detector. This adjustment results in R − Y and B − Y signals having 0.877 of their original values. The G − Y matrix, which operates on these R − Y and B − Y signals, likewise generates a G − Y signal having 0.877 of its original value.

When the color intensity control is adjusted to raise these signal levels by a factor of 1.14, chrominance signals R − Y, B − Y and G − Y are restored to their original values for application to the red, blue and green grids of the color picture tube. Since Y is also applied to the cathodes of the picture tube at its original value, true 100% saturated colors are reproduced on the picture-tube screen.

Thus, the outputs from the red, blue and green guns of the color picture tube faithfully follow the outputs from the red, blue and green cameras at the transmitter. There is one limitation, however, in the reproduction of *some* highly saturated colors. In spite of the fact that readjusted chrominance values are used, certain 100% saturated colors such as green will produce overmodulation at the transmitter. In a case of this sort, a prominent dot structure appears in the area of overmodulation and the hue and saturation values are not correct. Sync buzz may also appear in the sound. However, fully saturated greens are rarely encountered in nature, and this is the basis for the compromise in the assignment of NTSC readjusted chrominance values. END

# Television . . . it's a cinch

*Eighteenth conversation, first half: The trichromatic principle; transmission problems; simultaneous or sequential; saving the fine detail; how to carry the color inside the 6-mc band*

By E. AISBERG

From the original "La Télévision? . . . Mais c'est très simple!" Translated from the French by Fred Shunaman. All North American rights reserved. No extract may be printed without the permission of RADIO-ELECTRONICS and the author.

KEN—Well, why the disgusted look? Anything happen?

WILL—I've just been thinking that here I've spent all this time learning about television, and now in a year or two we'll have very little but color TV. So all the time I've spent on ordinary television is wasted. I'll have to start all over again.

KEN—Don't let it bother you! Most of the circuits in a color televiser are the old familiar ones we've been studying in black-and-white. Besides, black-and-white will be with us for some time yet. And the color circuits ar'n't going to be too hard—they say!

WILL—Oh, yeah? And can you tell me in a few well chosen words just how they transmit and receive color?

KEN—Well, several systems have been tried. All, of course, based on the trichromatic principle . . .

WILL—. . . in which all the hues are reproduced from three fundamental colors: red, yellowish green and greenish blue. By mixing them in the proper proportions, you can get all the shades and tints you like.

KEN—Wonderful! I didn't know you'd been studying the subject.

WILL—I learned that working in a print shop, where they printed pictures with red, blue and yellow inks. If you look at the pictures through a magnifying glass, you see the dots in those *primary* colors but at a short distance the eye mixes them up to make a solid picture. And, because I already knew a little about it, I was interested to find that the primary colors in TV are red, green and blue. That's because you're working with light and *add* the colors together. But when you print colors one on top of the other, it's equivalent to subtraction, so you have to use different colors to get the same result.

KEN—Boy, you keep right on surpising me! I never thought of you as an artist or color expert.

WILL—Do you take me for an ignoramus altogether? But let's get back to TV. I suppose, to transmit an image in color, we must work the same as in printing. First, we have to *separate* our scene into the three primaries, then transmit them separately and superimpose them at the receiving end to build up our picture.

KEN—That's just about it. So we have to get three images—red, blue and green—from our multicolor scene. How do we do it?

WILL—Easy. By using color filters. For example, if you photograph the scene through a red filter, you get a red image. The brightness of any surface element in it depends entirely on the amount of red light emitted by the corresponding area in the scene. So the red parts are brightest. And the blue and green parts, which emit no red light whatever, are black after they've gone through a good red filter.

KEN—That's right. Now we have three images: red, green and blue. What are we going to do with them?

WILL—Transmit them like any other television signals, of course. Then, at the receiver, we'll bring in each image in black-and-white on a separate picture tube. But in front of the "red" tube I'll put a red color filter (a piece of red

glass probably) and green and blue filters before the other tubes. Then all we have to do is superimpose the three images—it should be easy to do it by projection—to get the original image in true color. I can't see why the idea won't work!

KEN—Neither can I, Will. In fact, one of our big companies experimented with just that system about 10 years ago with some success. In spite of difficulty in registering the three images (as a printer you'd understand that!) they got very satisfactory pictures.

### Simultaneous or sequential

WILL—From the sound of your voice, there's a "but" in this somewhere!

KEN—And can't you see where? Three cameras, three transmitters, three channels, three receivers and three picture tubes?

WILL—I suppose it would cost a lot. And those three channels! No, with the spectrum as crowded as it is, you'd never get away with that! But what *is* the solution?

KEN—Remember the first things we learned in television? How, to get all points in a scene to the eye simultaneously . . .

WILL—. . . we transmitted them successively! I get it now! The solution is to send the red, blue and green images successively along a single channel. If they follow each other rapidly enough, the eye will blend them into a single picture!

KEN—That's the general idea. But don't think you can transmit the whole green image, then the red, then the blue. Unless you have a very large number of images a second you'll run into *flicker*.

WILL—Why?

KEN—Well, suppose part of your image is pure blue. Then that part would be transmitted only once during the time three images were going across space, for the red and green images wouldn't add a single quantum of brightness to the receiving screen. The eye would get the sensation of a light flicker over that part of the image because that part of the screen would be dark so long between the times the blue area would light up.

WILL—Can't we interlace the same as in black-and-white? First transmit the odd lines, then the even ones . . .

KEN—You're on the right track—you can use the same principle in color.

WILL—Fine! Now just how would we transmit a color picture if we vary the colors for every field?

### The color disc

KEN—O.K. Here's a system actually used today. It uses a revolving disc which passes red, green and blue filters successively ahead of the lens of the camera, and a similar disc ahead of the picture tube. The discs are kept in step by the sync signals.

WILL—I see that each disc has *six* filters: red, blue, green; then red, blue, green again. Three filters ought to be enough.

KEN—They are. But if we use six, we can cut the speed in two, which is an excellent idea. You develop a lot of centrifrugal force in those discs and, if you quadruple it by doubling the disc speed, you take a chance on the discs flying apart.

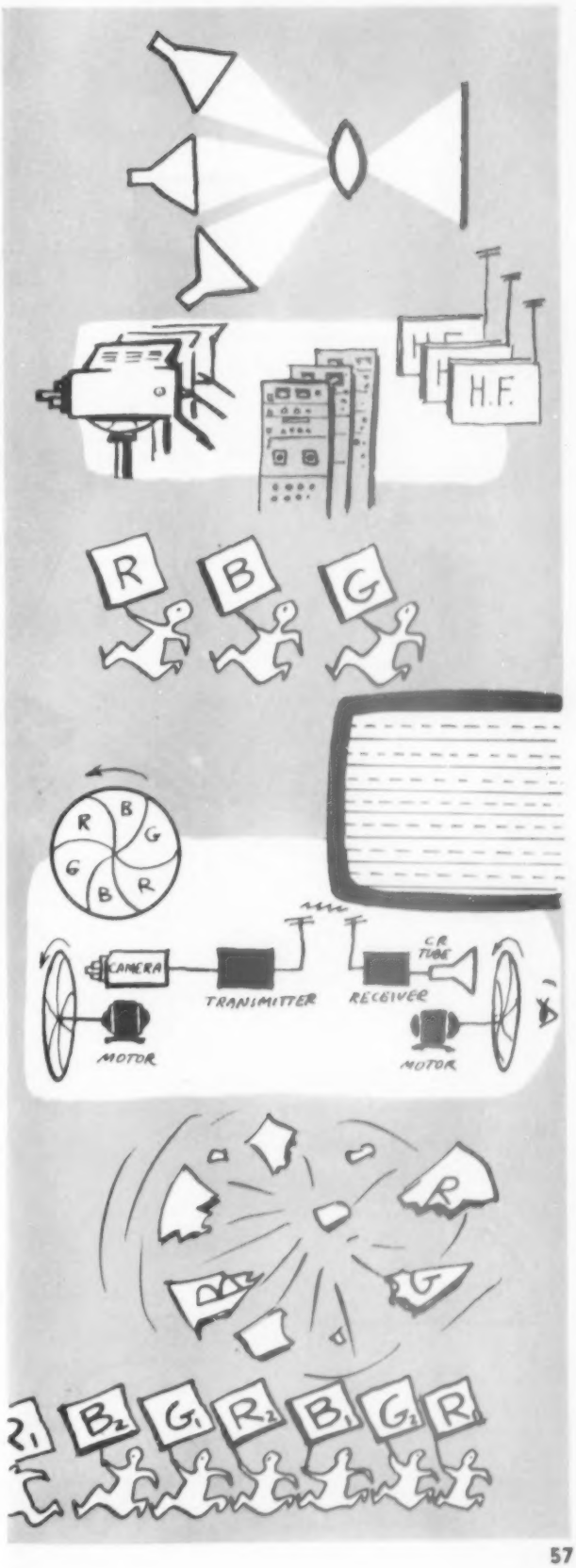
WILL—And so, while one color filter is passing ahead of the screen, you're not analyzing a complete color image, but only one color field—either the odd or even lines?

KEN—Exactly. Can you analyze the procedure?

WILL—Let's see. Suppose we start with the red odd lines. Then we have six fields:
1. Red, odd lines / 2. Blue, even lines / 3. Green, odd lines / 4. Red, even lines / 5. Blue, odd lines / 6. Green, even lines and then it starts all over again.

KEN—And in one turn of the wheel, each image is analyzed in each of the three primary colors, both for odd and even lines, and the fields are interlaced.

WILL—But that's six fields for black-and-white's two. Looks like we still might get flicker. But did you say something about more images a second?



KEN—Well, I have to confess something to you, Will. This system is not the one used by broadcast stations. It was abandoned for broadcasting some years ago. I told you the truth when I said it was used today, but it's used only for closed-circuit television. Different manufacturers can use different standards. Some have gone to very high line and field frequencies for higher definition. But the general rule has been to follow the old standard of 29,160 lines and 144 fields per second that was used when we almost had color television back in 1951.

WILL—But why not stick to the black-and-white standards of 15,750 lines and 60 fields a second?

KEN—You forget that you have to transmit three times as many points or surface elements. Even with the higher line and frame frequencies, you can't squeeze them all in. So—with the old sequential-color standard—the number of lines per frame was cut from 525 to 405. The eye is so satisfied with the sensation of life and depth that you get with color that the poorer definition doesn't bother it. The eye doesn't notice it, in fact.

## Saving the fine detail

WILL—So a lot of faults are covered up with a good coloring job. Who was it said television is like a woman?

KEN—But there are ways of limiting the modulation bandwidth without losing too much detail. The most important one is to transmit the fine details in black-and-white and to save color for the relatively larger areas, which of course would not need as high a frequency for their transmission. The result is very satisfactory.

WILL—Of course. I knew that when I was a small child.

KEN—Huh?

WILL—Definitely. My parents used to give me coloring books and I smeared up big areas with water-colors. That never obscured the picture detail, which was printed in black-and-white.

KEN—I can see that color television must look pretty simple to you!

WILL—Maybe. But let's get back on the job again. How's about giving a little on how television really is broadcast in color?

KEN—Well, you've been coming pretty close to it. If we keep our fine details in black-and-white, we find that we can send all our color on a band less than 1500 kc wide. That's quite a bit different from three television channels.

WILL—But you've still got to have an extra channel of some kind to transmit the color?

KEN—That problem has been solved too. The color signals modulate an oscillator at approximately 3.58 mc, in the video band. And this modulated *subcarrier* is part of the video signal that modulates the transmitter frequency. At the receiver, special circuits pick out the 3.58-mc signals, demodulate them, and . . .

WILL—Hold on! You are talking about one color signal, and we have to deal with three colors. Are there any other color subcarriers?

KEN—It's not quite as simple as that. *Two* color signals —I and Q—are sent on the color subcarrier—one at 90° phase difference from the other. These two signals are phase-modulated according to the colors being transmitted. They are detected at the receiver by a phase detector or demodulator, whose output is divided among the color tubes of the receiver so that the original colors are reproduced.

WILL—It's no use! You've been way over my head for the last 10 minutes. And now you're even talking about color *tubes* in the receiver. I thought there was only one.

KEN—You're right, Will—color is too tough a subject for a single conversation. If you're really interested, maybe we can get together sometime soon and go into it seriously.

WILL—O.K. But what about that tube?

KEN—You're right about it, too. Modern receivers use only one, though the old simultaneous system used three. The one that's almost universally used today reminds one a little of the old three-tube system: it has three guns, one for each color. But there is also a single-gun tube, and some sets using that are now under construction. TO BE CONTINUED

# *Converting* 630 RECEIVERS *to* INTERCARRIER OPERATION

*With an intercarrier circuit, the old standby gives a fine account of itself in the u.h.f. spectrum*

By HOWARD BIERMAN*

EARLY field reports in v.h.f.–u.h.f. areas, as submitted to manufacturers of 630 type receivers, noted excellent signal-to-noise ratio, superior picture quality and above average sync stability. However, one particular problem was considered objectionable — oscillator drift during u.h.f. operation necessitated frequent resetting of the fine tuning control to maintain clear sound reception. It was therefore necessary to redesign the sound and video i.f. sections of the original 630 chassis for intercarrier circuitry, which is substantially immune to oscillator drift problems. The conversion described in this article has been made in several thousand sets during the past year and has proven highly successful in u.h.f. areas under various signal-strength conditions.

Proper design and careful alignment have resulted in clear, crisp audio output free from the annoying and discordant buzz often heard in less expensive intercarrier sets. Several hours' labor and less than $10 worth of components are the only necessary expenses to convert a 630 set to the newer improved intercarrier circuitry.

Let's compare the operation of split-sound and intercarrier receivers. The transmitted TV sound carrier is 4.5 mc higher than the video carrier; this frequency difference is closely maintained at the station in accordance with FCC regulations. In split-sound design (such as the original RCA 630 i.f. section shown in Fig. 1) the video and sound i.f. signals developed at the mixer are separated at the tuner output or in one of the first two video i.f. stages, and fed to separate i.f. stages for further amplification. Individual sound and pictures detectors then feed their demodulated output to the audio and video amplifier stages, respectively.

In intercarrier systems, the video and sound i.f. signals are passed through a

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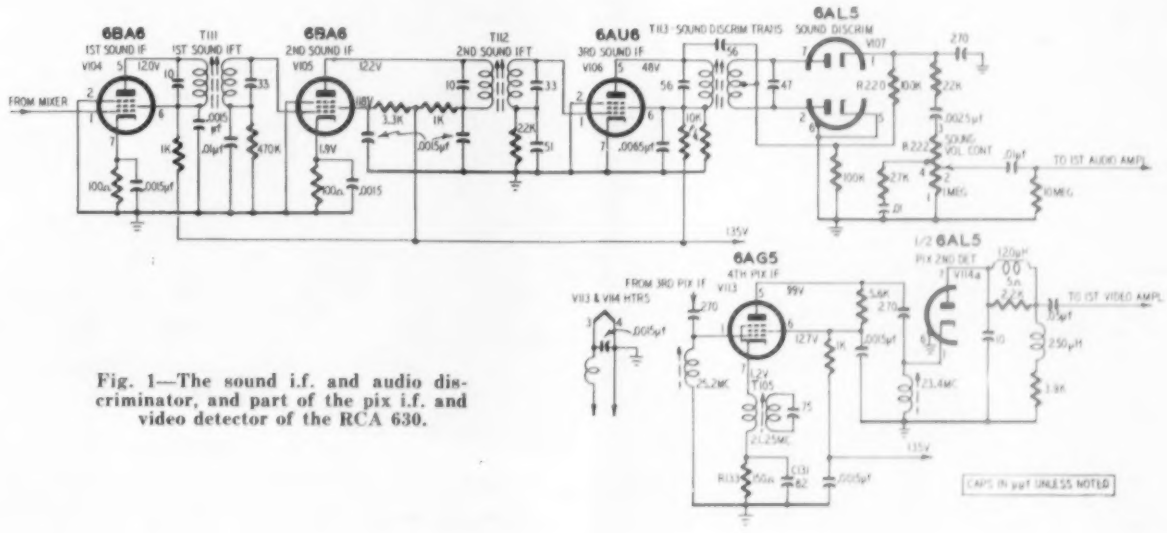
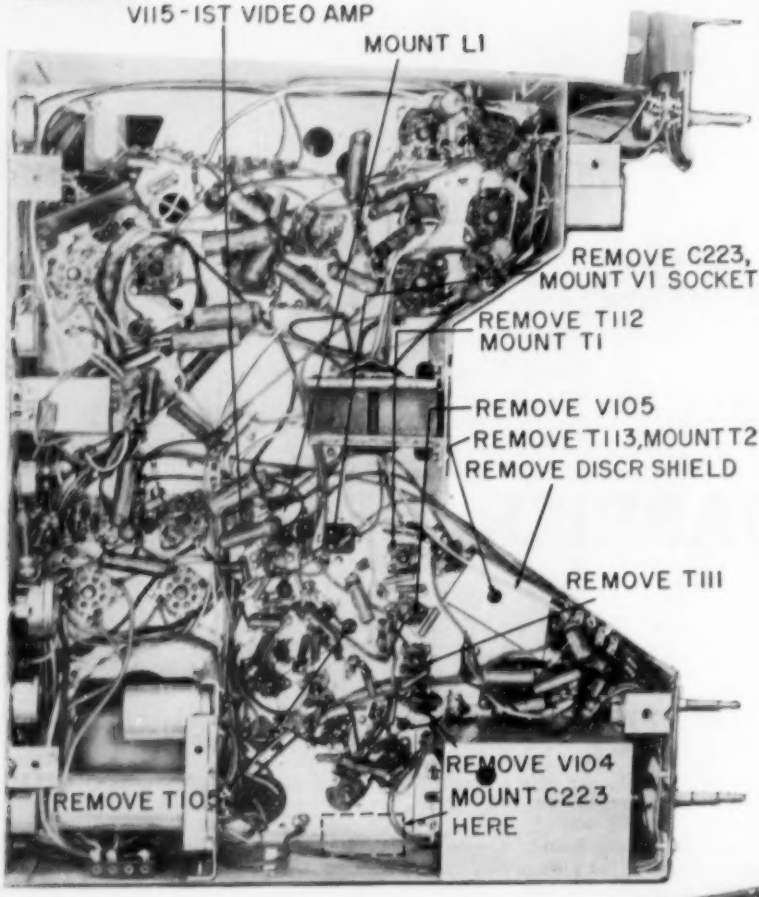


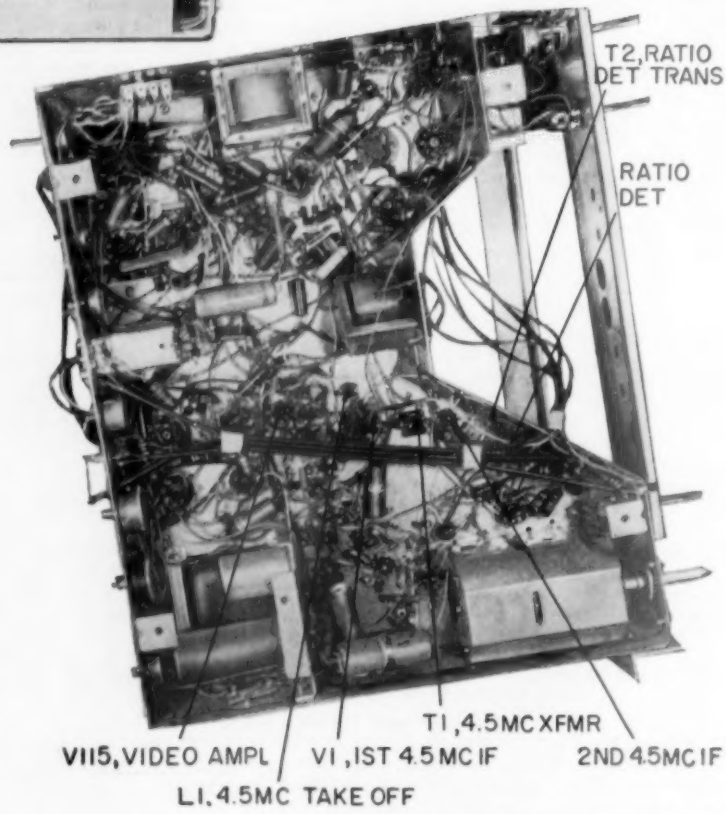

**Fig. 1—The sound i.f. and audio discriminator, and part of the pix i.f. and video detector of the RCA 630.**




Underchassis view of a 630TS split-sound receiver—before modification.

common wideband i.f. section and applied to a single detector stage. A heterodyne action takes place during the combined detection process, producing a 4.5-mc carrier containing the same frequency-modulated variations as the transmitted sound carrier. This 4.5-mc signal is then amplified and applied to an FM detector—usually a ratio detector type—which produces audio signals for the sound section of the receiver.

In v.h.f., as in u.h.f. operation, the local oscillator stage of the tuner is subjected to thermal changes, B plus variations and humidity effects which produce frequency drift. Since heterodyne action between the incoming sound and picture r.f. carriers and the local oscillator signal determines the i.f. carriers, a shift in oscillator frequency will produce a similar variation in the i.f. signals. In split-sound design this causes weak, distorted or complete loss of sound since the sound i.f. carrier is displaced from the center of its relatively narrow bandpass region. In intercarrier receivers, however, the audio signals are not affected since they are developed from the 4.5-mc beat note, maintained by the frequency difference between video and sound carriers at the transmitter. Regardless of local oscillator drift and shift in i.f. carrier values, the 4.5-mc beat note is unchanged.




A 630 type chassis after modification for intercarrier operation.

While this article is specifically directed toward 630 type receivers, the principles and practices apply to most models and may be used as a guide for similar conversion jobs. The initial step requires a complete removal of the entire sound section, shown in Fig. 1. (All codes used in Fig. 1 are those used in original RCA diagrams. Codes and values in some 630 type receivers may differ slightly from the original at certain points.

Unsolder the various components of the three sound i.f. amplifiers and discriminator stage, indicated as V104, V105, V106 and V107. Avoid loosening or pulling out any socket pins or it will become necessary to repair the socket or mount a new one. Remove the two sound i.f. transformers (T111 and T112), the discriminator shield cover, the discriminator transformer (T113) and tube sockets V105 and V106. Remove electrolytic capacitor C223 (10 $\mu$f, 40 $\mu$f, 450 volts; 10 $\mu$f, 350 volts) and mount it at the side of the chassis (see photo), extending the wires attached to it by well spliced connections. Finally, remove sound trap T105 located in the cathode circuit of the fourth picture i.f. stage. (The photos are not "before" and "after" shots of the same chassis. One is a 630 type chassis in its original form, the other is a different but similar chassis after conversion. This accounts for the can type C223 in one photo and the tubular type in the other.)

In addition to the various resistors and capacitors shown in the schematic of the intercarrier circuit (Fig. 2) several 4.5-mc transformers are required. Several manufacturer's types are indicated in the parts list. These components are physically interchangeable with the original 630 parts, avoiding unnecessary drilling or filing.

In assembling the new parts, first drill a 5/16-inch hole near the first video amplifier tube V115 (see photos). Be careful to avoid disturbing or damaging any wiring or parts in this area. Mount trap L1 in the 5/16-inch hole. Mount a seven-pin miniature wafer socket in the space previously occupied by electrolytic capacitor C223. The capacitor has been moved to the side of the chassis and the tube socket substituted in this region to keep lead lengths of the 4.5-mc circuits as short as possible. This tube location is the new first sound i.f. stage, V1. Mount the 4.5-mc sound i.f. transformer T1 in the space previously occupied by the second sound i.f. transformer T112. Then mount ratio detector transformer T2 in the space originally used for discriminator transformer T113. The receiver is now ready for wiring.

Since the cathode trap of the fourth picture i.f. stage has been removed (to prevent excessive attenuation of the sound i.f. carrier before it reaches the detector stage), it is necessary to wire cathode components R133 and C131 (Fig. 1) directly to the cathode of V113. Change C131 from 82 to 1,500 $\mu\mu$f. Then carefully wire all components contained in the intercarrier section, using the schematic shown in Fig. 2. Keep all lead lengths as short as possible and avoid placing the grid and plate leads adjacent to prevent oscillation. Use high-quality ceramic bypass capacitors and make all ground connections to the closest possible chassis points. Avoid haphazard component layout and careless wiring which may result in instability or faulty operation. Dress the heater leads away from grid and plate leads, as well as from trap L1 to avoid hum modulation.

After completing the wiring, check the finished job carefully against Fig. 2 and place the various tubes in their sockets. To minimize the possibility of power supply overload or component burnout, invest a few minutes in a resistance check at the plate and screen (pins 5 and 6) of the 6AU6 4.5-mc amplifier tubes. If these points measure about 5,000 ohms or so to ground, power may be applied for alignment. Should the ohmmeter reading fall well below this value, carefully recheck the wiring and components before proceeding further.

## Alignment

The last remaining task in the conversion is accurate alignment of the new 4.5-mc section, as well as the oscillator section of the tuner. Apply power to the receiver and test equipment to be used (v.t.v.m. and signal generator) and allow several minutes' warmup time. If available, an r.f. signal generator equipped with a 4.5-mc crystal would be the most desirable source of signal input. However, an accurately calibrated r.f. generator or even a station signal is sufficient for a proper alignment job.

Assuming an r.f. generator or crystal calibrator is used, feed a 4.5-mc unmodulated signal to the cathode of the 6AL5 video detector stage V114-a (Fig. 1). Set the receiver station selector to an unused channel to prevent interference beat notes and then connect a v.t.v.m. across ratio detector load resistor R1. The v.t.v.m. selector switch should be placed to its "plus d.c." range; if a v.t.v.m. is not available, a 20,000-ohms-per-volt multimeter will be adequate.

Detune the secondary of ratio detector transformer T2 by rotating its bottom slug several turns. Then adjust the top slugs of T2, T1 and L1 for maximum indication on the v.t.v.m. Following these adjustments, connect the v.t.v.m. across C1 and ground. Slowly adjust the bottom slug of ratio detector transformer T2 for exact zero reading on the v.t.v.m. As the slug is turned, the v.t.v.m. reading will be positive, pass through zero and then become negative—the point at which it passes through zero is the correct setting.

If an accurate 4.5-mc source is not available, tune the receiver to a strong local station (transmitting a test pattern and tone signal preferably). Set the receiver fine-tuning control until the picture is clearest or just before the point at which sound bars begin to appear on the picture. Follow the previous alignment instructions, using the station signals as the input source.

For receivers that have individually adjustable oscillator slugs for each channel, set the fine-tuning control to its mid-position. Adjust the oscillator slugs of each received channel to the point where sound bars (horizontal lines whose number and intensity vary as the sound modulation changes) just begin to appear.

If the conversion job has been neatly and carefully followed in assembly, wiring and alignment, it should now be possible to enjoy u.h.f. as well as v.h.f. reception without the annoying necessity of constantly retouching the fine-tuning control. Sound and picture quality will be as sharp and clear as before the conversion since no compromise or sacrifice in receiver operation has been made. END

**Parts for 630 conversion**

**Resistors:** 1—47, 1—100, 1—1,000, 1—33,000, 2—6,800 (5%), 1—39,000, 1—47,000, 1—56,000, ohms, ½ watt; 1—39,000 ohms, 1 watt.

**Capacitors:** 1—2.2 $\mu\mu$f, 1—47 $\mu\mu$f, 1—390 $\mu\mu$f, 2—470 $\mu\mu$f, 1—.0015 (C131, Fig. 1), ceramic; 4—0.1 $\mu$f, ceramic, 500 volts, 1—4 $\mu$f, 50 volts, electrolytic.

**Miscellaneous:** 1—6AU6; 1—7-pin miniature wafer socket; 1—4.5-mc takeoff coil (Techmaster L308A, Miller 1469, Meissner 17-3402 or equivalent); 1—4.5-mc interstage transformer (Techmaster T212, Miller 1466, Meissner 17-1021 or equivalent); 1—4.5-mc ratio detector transformer (Techmaster T214A, Miller 1468, Meissner 17-1033 or equivalent).

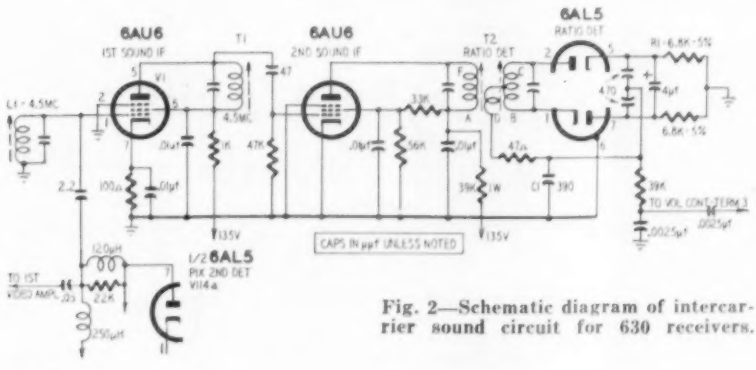



**Fig. 2—Schematic diagram of intercarrier sound circuit for 630 receivers.**

## Retrace blanking (continued)

A circuit somewhat similar to those discussed last month is used in Sparton chassis 23U214 (Fig. 1). Here the retrace elimination pulse is taken from the secondary of the vertical output transformer. This negative pulse of approximately 90 volts peak to peak is applied through a wave-shaping network consisting of integrator R1-C1 and coupling capacitor C2 to the grid of a 21ZP4-B. A 330,000-ohm resistor isolates this circuit from the brightness control, and the video signal is fed to the picture tube cathode. The voltage applied to the grid is a sharply spiked 55 volts peak to peak.

A somewhat more complicated circuit is used in the Admiral 17XP3 chassis (Fig. 2). This circuit contains an autotransformer in the plate circuit of the 6S4-A vertical output tube. A 60-volt peak-to-peak negative pulse is taken from the low end of the vertical deflection coils and fed to the grid of the 17AVP4 through a printed-circuit wave-shaping network. The output of this network consists of a sharp negative pulse approximately 30 volts peak to peak.

Capacitor C1 and resistor R2 form a differentiating circuit that filters out the low-frequency component that often causes picture shading. High-frequency horizontal ringing components are removed by the integrating network R1-C2. Without this network vertical bars may appear. A 120,000-ohm resistor is used between the brightness control and cathode. The video signal is fed to the cathode.

Another variation is shown in the Raytheon 16AY211 chassis (Fig. 3). In this circuit a positive pulse, taken from the high side of the deflection coils, is shaped and fed to the cathode of the picture tube. The video signal from the 12AT7 is fed to the control grid of the picture tube. The brightness control in this circuit is isolated through a 100,000-ohm resistor.

From the previous circuits it can be seen that a retrace elimination circuit can vary from a simple coupling capacitor to a relatively complex network. In addition, individual component values vary considerably. Thus, due to the circuit variations between TV receivers, each retrace elimination circuit should be custom-made for optimum performance. The circuits shown here form a center value about which variations should be made to obtain a good sharp spike voltage of sufficient amplitude. In experimenting with these circuits, an oscilloscope is almost indispensable for observing pulse shapes.

When working without a scope and not sure of pulse polarity, reverse your connections if retrace lines are not eliminated. As a final check, advance the brightness control and decrease the contrast. At extreme settings the retrace lines may be faintly visible. However, for any setting less than full brilliancy, retrace lines will be eliminated.

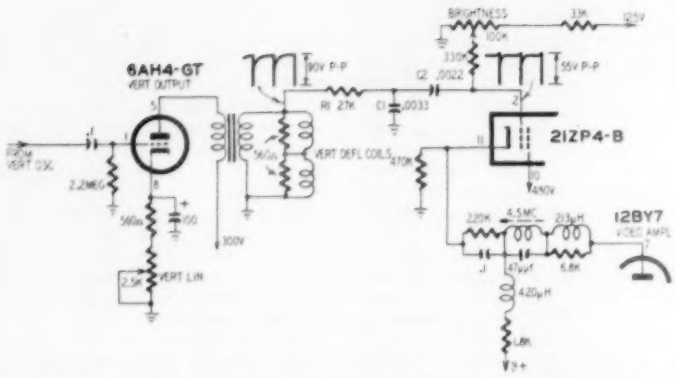



Fig. 1—The retrace blanking circuit used in the Sparton 23U214 TV receiver.

### Audio hum

*A Magnavox receiver now on the bench came in with a complaint of hum. The set uses a separate audio amplifier that shows no sign of hum when used without the TV receiver. I have used crystal input and magnetic input (through a preamp) on the amplifier without the slightest trace of hum. However when I connect the amplifier to the TV chassis, there is considerable hum.*

*The owner says that this set is new and that he has had the trouble since*

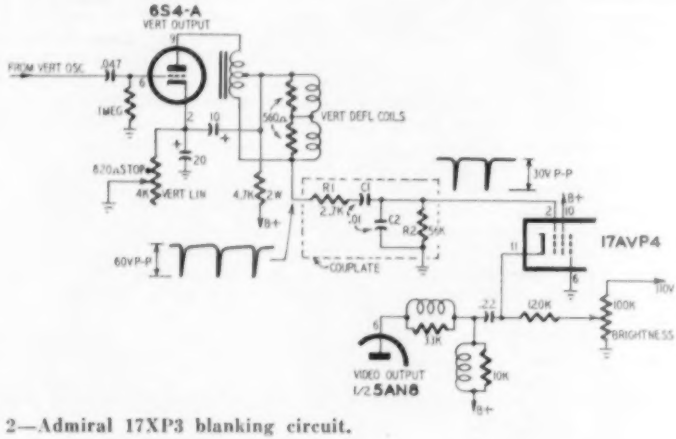



Fig. 2—Admiral 17XP3 blanking circuit.

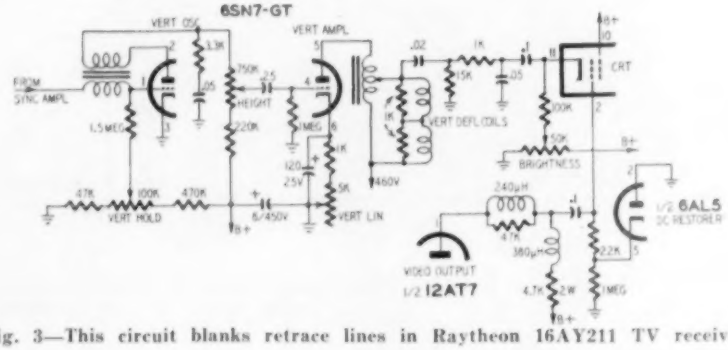



Fig. 3—This circuit blanks retrace lines in Raytheon 16AY211 TV receiver.

*he bought it. Furthermore, he was told that the hum is characteristic and cannot be eliminated. I don't think this is so and I would like some suggestions on how to clean up the trouble. I cannot read the entire model number, but it says 300 series and model CT followed by some other illegible identification.—T. W., Cleveland, Ohio*

The Magnavox 300 series and models starting with the code CT cover a very wide range of chassis circuitry. However we can discuss the problem in general. The receivers using a separate audio amplifier have a TV–phono switch in the TV chassis that could be causing the trouble. Carefully dress all the shielded audio leads from this switch away from the filter choke and close to the chassis. You might also try reversing the amplifier a.c. plug, however this will generally have little effect if the leads to the TV–phono switch are properly dressed.

If you have not already done so, replace the 6T8 ratio detector and first audio. If you have a scope, look for hum ripple in the plate circuit of the 6T8. This is a low-level signal point and, if there is any appreciable hum, add a decoupling network between the plate load resistor and B plus. Use a resistor of about 50,000 ohms and a bypass capacitor of about 0.1 to 0.5 μf.

Most of these chassis have a 120,000-ohm resistor connected from one side of the a.c. line to chassis ground. Place this resistor as close to the a.c. receptacle as possible and connect it to the side of the a.c. line which does not contain the on–off switch.

## High-voltage fuse

*A Stromberg-Carlson model 400 came in with the high-voltage fuse blown. I checked the horizontal output, damper and high-voltage circuits but found all voltages and resistance measurements to be normal. With a new fuse in the circuit, everything worked fine. When the set was turned off and on again, however, the fuse blew. The same thing occurs when the set is switched from the radio to TV. I have tried checking for defective components but everything measures as per manufacturer's specifications.—R. M., Ogden, Utah.*

Although this trouble is not particularly characteristic of this chassis, the symptoms you describe very much indicate oscillator failure. With this circuit not operating, the necessary drive voltage to the grid of the horizontal output amplifier is not developed. Plate and screen currents cause the fuse to blow.

The oscillator uses a type 6SN7 and may contain the relatively recently introduced 6SN7-GTA which apparently does not oscillate as readily as the older 6SN7-GT. This trouble, not confined to any one tube manufacturer, has shown up in many cases where switching has caused the oscillator to fail and the fuse to blow. Thus, observe the grid drive on the horizontal output tube. Use a 6SN7-GT in the horizontal oscillator circuit. If there is still no oscillation, you will have to check out all components in the oscillator circuit.

## Critical horizontal hold

*A particularly rough set on hand has already caused me three callbacks. The receiver is a Sentinel model 438, and each check revealed a different defective component in the horizontal oscillator causing the raster to disappear.*

*Even when repaired the horizontal hold control setting is very critical and the customer reports that before the raster disappears the horizontal hold is almost impossible to maintain. I am sure that the trouble is in the phase detector or horizontal oscillator circuits.—W. M., Houston, Tex.*

There is a very strong likelihood that the trouble of critical horizontal hold is being caused by a leaky .047-μf capacitor (C81, Fig. 4) used in the horizontal reference feedback circuit. When defective, this unit will often cause other components, generally resistors, to change value. The resistors affected are those connected in series with the feedback capacitor to ground and those in the cathode and plate circuit of the horizontal oscillator. This feedback capacitor, when defective, will often cause associated capacitors to fail.

Thus, it could be that you are continually finding defective components and replacing them without getting at the basic source of the trouble. Your very first remedy is to replace this feedback capacitor with a new .047-μf 1,000-volt unit. Following this, check every component in the horizontal oscillator and feedback circuit. Replace any that are off value by more than 10%.

## Weak horizontal sync

*The complaint on a G-E 21C347 receiver was very weak sync. Upon thorough checking it was found that the horizontal sync was very poor but the vertical sync was normal. In all other respects the picture and sound were normal. I have checked all tubes in the sync and horizontal deflection circuits but this did not help. I do not have a schematic of this circuit and am not familiar with its operation or waveshapes, so it is difficult to troubleshoot it as I would more conventional circuits. May I have a list of the more likely causes of this trouble and some typical voltages that would indicate proper operation of the circuit?—J. S., San Diego, Calif.*

Your first test should be a check of the sync amplitude at the input of the horizontal phase detector (Fig. 5). This signal comes from the cathode of the sync phase splitter and should be about 50 volts peak to peak. Check the bias and plate voltages on the control (horizontal reactance) tube.

A common cause of the trouble described is defective components in the sine-wave oscillator. Carefully check coil L251, capacitors C260, C264 and resistors R265, R266. Other capacitors to be checked are C255 and C258. Another very important group of components to be tested are those in the network that determines the waveform of the feedback signal. These include capacitors C272, C273, C276 and resistors R279, R278.

In addition, be sure all tubes involved have been checked by direct substitution. Often slight differences in the characteristics of "good" tubes can make the difference between normal and poor operation. END

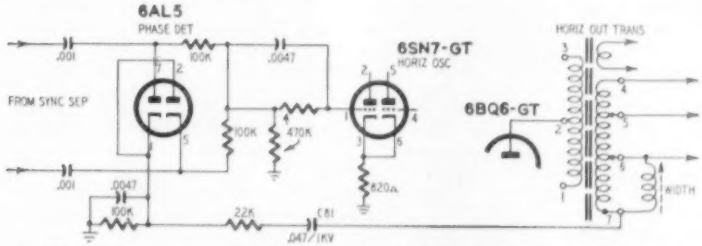



**Fig. 4—Phase detector and reference circuit in Sentinel model 438 TV sets.**

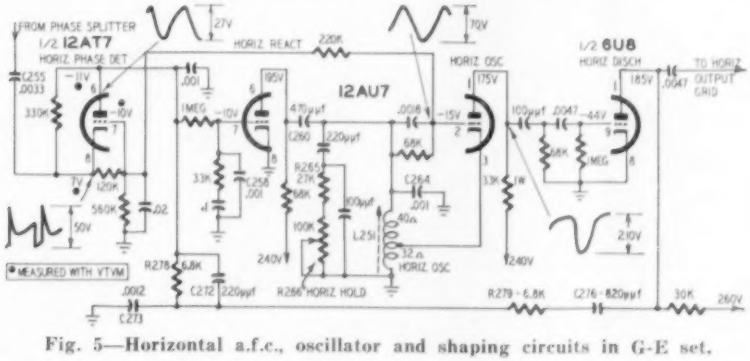



**Fig. 5—Horizontal a.f.c., oscillator and shaping circuits in G-E set.**

COVER FEATURE

**The equipment room at the Narragansett Marine Laboratory. All the apparatus in this photograph is used solely for recording the sounds made by fish.**

By ERIC LESLIE

# NOISY FISHES

THE noisemaking abilities of some fish have long been known—witness such names as "grunter" and "croaker." Systematic study of their acoustic output has been undertaken only recently, and most of the work has been done since 1949.

Interest in fish sounds began during World War II when sonarmen, submariners and others began to report strange sounds, which at first they attributed to enemy action. The fishy sounds were considered important enough to warrant an extensive program of study, and now the characteristic sounds of the noisier fishes have been recorded for posterity—or study.

Possibly the world's greatest authority on the subject of fish-made sounds is Mrs. Marie Poland Fish, biological oceanographer of the University of Rhode Island's Narragansett Marine Laboratory. Her studies have taken place in most of the oceans of the world and have included other ocean-dwelling noisemakers as well as fish. Mrs. Fish finds that noisemaking is common among many types of marine life: voluntarily as a means of communication, particularly to implement breeding; as an expression of fright; as a measure of defense or offense; as a response to environmental changes or as a means of orientation, and involuntarily in connection with swimming, feeding, collision or other activity.

These conclusions were reached through study of 62 species of temperate coastal and 105 tropical and subtropical fishes, 20 crustaceans and 2 species of marine mammals. In many cases the marine life was monitored "on location." For more intensive studies the fish were held captive in tanks, particularly at the laboratory near Kingston, R. I., and in Bermuda and Bimini in the British West Indies.

One such tank is the subject of our cover, which shows one of the star performers near the microphone or hydrophone, and Mrs. Fish operating the tape recorder which preserves the sounds emitted by the subjects in the tank. Not only have simple recordings been made, but frequency spectra have been run with harmonic wave analyzers and octave filters. Some of the equipment used for recording and analysis is shown in the photograph on this page. Incidentally, marine life is studied directly with a hydrophone on a long cable run out the window in the background and down to an arm of the Atlantic 200 feet or so away. Shallow water types are best monitored thus directly—deep-water fishes are more accurately handled by dredging them up and studying them in the tank. Some of the sound recordings—both tank and in natural habitat—have been accompanied with moving picture film, thus positively and permanently identifying the soundmakers.

The project is one of basic research, but has numerous practical angles. The Navy is particularly interested, due to the difficulties in World War II as a result of not expecting or being able to interpret the remarkable variety of underwater sounds. As a result, the Office of Naval Research is partly sponsoring the work of the laboratory.

The practical applications, says Mrs. Fish, include use of the reference file of recordings to indoctrinate sonarmen and familiarize them with expected animal interference; to collect biological data which show what sonic animals can be expected, in what numbers and in what seasons (useful in predicting sound conditions in strategic areas) and collection of physical data which spot sound levels and frequency ranges (useful in design and operation of acoustic and electronic equipment).

The equipment includes a Magnecord PT63 for permanent tape records, though disc recorders and a converted Gray Audograph Electronic Soundwriter have been used. The microphones are quartz-crystal hydrophones developed for the project. High- and low-pass filters, Navy octave filters and a Hewlett Packard 300A wave analyzer complete the laboratory equipment, though there is also a portable lightweight, self-contained outfit designed for field use. Much of the equipment has been designed or modified from Navy gear by William H. Mowbray, electronics engineer engaged with Mrs. Fish in the project.

Persons in peaceful pursuits—as well as the Navy—may benefit by study of underwater sound. Any new information of this type may be interesting and useful to commercial or sport fishermen, as well as a tool for oceanography and marine life research. END

By CHARLES L. HANSEN

# TRANSPLANTING AMPLIFIERS

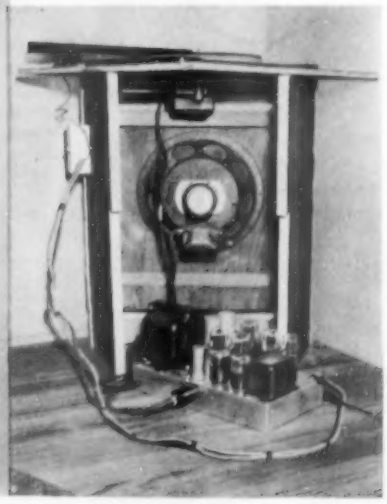
*The audio portion of old radios provides good phono equipment*

HIDDEN in back rooms and basements of radio and television repair shops are forgotten relics of the console radio age collecting dust and taking up valuable space. A great number of these radios have a hidden value; they have the makings of a good-sounding phonograph amplifier. And they can be purchased for only a dollar or two. Many of them, built in the 'Thirties and 'Forties, have excellent amplifier and speaker systems which can be put to use as a phonograph amplifier for practically no cash outlay.

The finished product will be equal in performance to at least a $50 commercially built phonograph amplifier. This opens a path for constructing a good amplifier for practically the price of time—time for the removal of the amplifier and the power-supply sections from the original chassis and for transplanting the parts to a new aluminum chassis and plywood cabinet.

A socket punch, hand drill, scribe for marking the new chassis and soldering iron are all the tools needed. For the cabinet work, as with the chassis, only simple tools are used. A handsaw, a keyhole saw, some sandpaper and a wood rasp will finish the woodwork. The additions of a phonograph turntable and pickup, coupled with the cabinet, amplifier and speaker, complete the project. A dozen trips to the local radio store for more parts or exchanges are not necessary because all parts are available. Everything turned out so well on my first project that I built several phonograph amplifiers in a short time and used them as gifts.

**Above — The completed phonograph installation.**



**Right — Rear view of the completed cabinet together with the amplifier from an old radio.**

The amplifier (see photo) selected for the first job was a Crosley, vintage about 1935. It used push-pull 2A5 tubes and a 12-inch dynamic speaker.

In purchasing an old console radio it might not hurt to ask the radio service technician if it would be possible for you to plug in the set to find out if the audio section is working. In any case give the set a hasty once-over, observe the condition of the speaker and the chassis and notice if any parts or tubes are missing.

You will be able to tell just how good a bargain you got after cleaning up the chassis on your work bench. Chances are that the radio and amplifier will work right from the start. The diagram for your purchase can be found in Rider's or can be traced from the wiring. If the chassis is very old, the electrolytic filter capacitors in the power supply will have to be replaced. For ease of rewiring, use new tube sockets. The chassis selected should be able to hold all the amplifier and power supply parts comfortably.

In sizing up the job of transplanting, look at the diagram and see if the manufacturer wanted this set to do double duty as a phono–radio combination or if it was just for radio use. If it was used only for radio, then the builder may have to insert another stage of amplification ahead of the tube driving the final amplifiers. This can be done simply by choosing a tube similar to the driver. Then add compensation for the type of crystal pickup to be used. Standard equalization diagrams have been published in RADIO-ELECTRONICS in past articles for different types of pickups or the circuits generally supplied with the crystal pickup can be used.

One driver may be enough to work the push-pull tubes if a high-output jukebox type pickup is used (3–4-volt output). If a conventional home type pickup is used, the extra stage of amplification will be necessary. In the Crosley a 56 type tube is used to drive the push-pull 2A5's and another stage of voltage amplification was added as shown in Fig. 1.

A few improvements over the original design can be made after the amplifier has been transplanted. For ex-

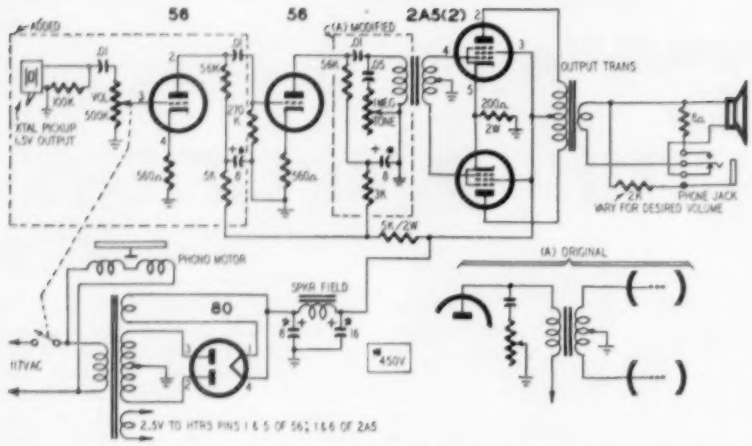



**Fig. 1.—Diagram of the Crosley amplifier showing the various modifications.**

ample, when transformer coupling is used, and it was used in most amplifier designs of the 'Thirties, a wiring change as shown in the illustration can be made. This minor modification will improve the high-frequency response and is worth while.

The volume and tone controls, on–off switch and phone jack are contained in a small utility box bolted to the side of the cabinet.

The long low-level leads to the control box are enclosed in shielded braid. All wires to controls and the a.c. switch are then taped together, forming one cable. Extending the controls in this manner permits greater flexibility of amplifier location within the cabinet. In my case the amplifier is not mounted permanently or as part of the cabinet. It is resting on the floor within the enclosure. Microphonics and feedback have not been experienced even with the volume turned up as loud as possible. If the amplifier is mounted on the speaker cabinet, acoustical feedback may occur.

Several radio console amplifiers were transplanted and used for phonograph amplifiers. Simple modifications were made in some of the circuits. In one case a tweeter speaker was added because the original 12-inch speaker did not perform as well as it should at high frequencies. Many different modifications and changes could have been made but the original purpose of this project would have been defeated.

The cabinet work is simple. Notice that the cabinet (see photo) is designed to fit into a corner of a room. There are no parallel surfaces within the enclosure and we therefore do not have to pad the inside. A minimum of wood finishing is needed as the wood area exposed is small. Both of these items save the builder time and money without any sacrifice in looks or performance. The phonograph turntable and pickup are mounted on top of the cabinet. The remaining exposed wood surfaces are stained mahogany and finished with clear shellac. Other decorative schemes can be used. One novel idea is to use one of the various wood veneers that are applied like wallpaper. Individuals adept in wood finishing can think of a number of ways to better finish the cabinet.

Fig. 2 shows how the front and top may be cut from a single 2 x 4-foot sheet of ¾-inch or heavier plywood and the sides from a piece of ¾-inch pine 4 feet long and 10 inches wide. The 12-inch circular cut may be made before or after the 24 x 21-inch front panel is cut in two. Fig. 3 shows the assembly of the sides and front pieces and Fig. 4 is a top view.

A 24-inch long strip of brass is screwed to the front panel pieces to hold them together and to support the grille cloth over the speaker opening. I used felt-lined brass weatherstrip with the felt removed. The sides, top and front are assembled and the speaker board mounted with flat-head screws.

The builder can expect a good-sounding amplifier which does credit to present day standards of good listening. It will not be high fidelity: it uses transformers designed 20 years ago. But for the purpose for which it is built, this amplifier has several advantages over high-fidelity systems. The response in the high-frequency range cannot be expected to exceed 6 kc from pickup to speaker. Perhaps 5 kc would be a better average. Play a shellac record on a hi-fi set and play the same record on this amplifier. Your shellac record sounds best on an outfit that starts to taper off around 5 kc. This has the same effect as adding a scratch filter to the hi-fi system. And for a children's phonograph nothing else could be desired even if all new parts were purchased and the amplifier specifically designed this way. The base response is adequate and an improvement in the low frequencies is obtained by the front and side horn loading design of this cabinet.

Sound through a phonograph amplifier of this kind will be a thousand times better than that obtained from those bargain-store purchases that sell for $20 to $50. END

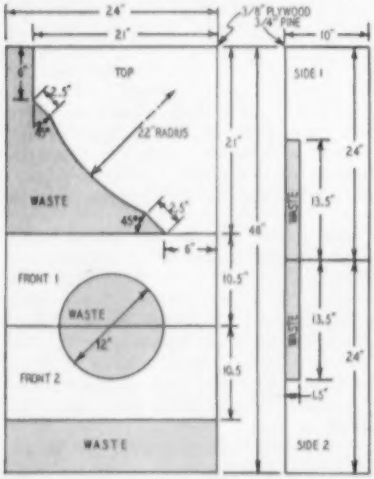



**Fig. 2—Layout of the speaker enclosure.**

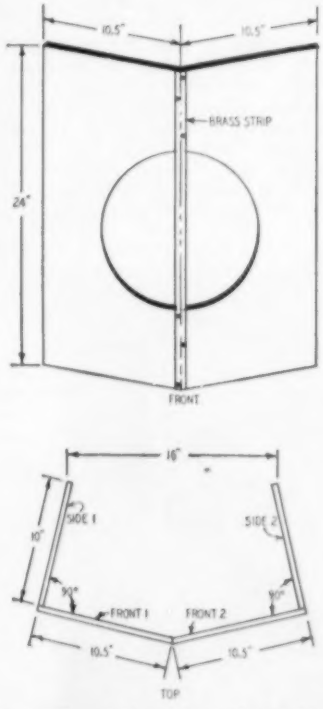



**Fig. 3—Front view of speaker cabinet. Insulator is normally used on door bottoms. Remove felt strip and attach.**

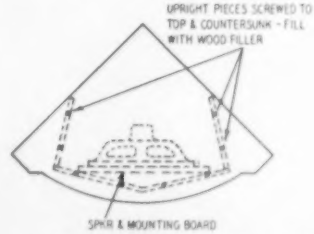



**Fig. 4—Top view of the speaker cabinet. If old speaker is mounted on board, remove it and attach to front of cabinet.**

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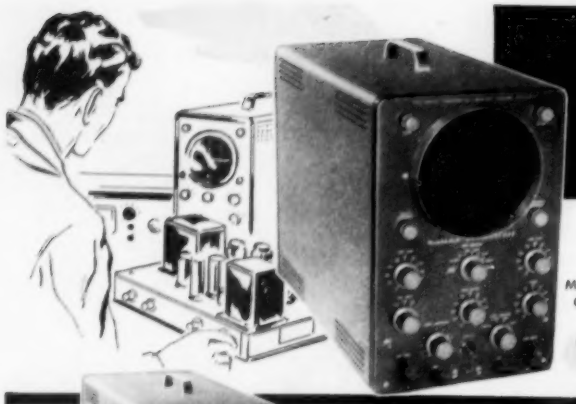

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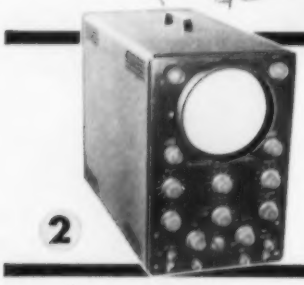

**1** *Heathkit* ETCHED CIRCUIT
COLOR-TV

## 5" OSCILLOSCOPE KIT

This deluxe quality oscilloscope has proven itself through thousands of operating hours in service shops and laboratories. Features the best in components—and the best in circuit design.

Features amplifier response to 5 Mc for color TV work, and employs the radically new sweep circuit to provide stable operation up to 500,000 cps. In addition, etched metal, pre-wired circuit boards cut assembly time almost in half, and permit a level of circuit stability never before achieved in an oscilloscope of this type.

Vertical amplifiers flat within +2 db −5 db from 2 cps to 5 Mc, down only 1½ db at 3.58 Mc. Vertical sensitivity is 0.025 volts, (rms) per inch at 1 Kc. 11 tube circuit employs a 5UP1 CRT.

Plastic molded capacitors used for coupling and bypass—preformed and cabled wiring harness provided.

Features built-in peak-to-peak calibrating source—retrace blanking amplifier—push-pull amplifiers and step-attenuated input.

MODEL O-10
**$69.50***
Shpg. Wt. 21 Lbs.

**2** *Heathkit* ETCHED CIRCUIT

## 5" OSCILLOSCOPE KIT

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Features full size 5" CRT (5BP1), built-in peak-to-peak voltage calibration—3 step input attenuator—phasing control—push-pull deflection amplifiers—and etched metal prewired circuit boards.

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**5** *Heathkit* ETCHED CIRCUIT

## 3" OSCILLOSCOPE KIT

This compact little oscilloscope measures only 9½" H. x 6½" W. x 11¾" D., and weighs only 11 lbs! Easily employed for home service calls, for work in the field or is just the ticket for use in the ham shack or home workshop. Incorporates many of the features of the Model OM-1, but yet is smaller in physical size for portability.

Employing etched circuit boards, the Model OL-1 features vertical response within ± 3 db from 2 cps to 200 Kc. Vertical sensitivity is 0.25 V. RMS/inch peak-to-peak, and sweep generator operates from 20 cps to 100,000 cps. Provision for r.f. connection to deflection plates for modulation monitoring, and incorporates many features not expected at this price level. 8-tube circuit features a type 3GP1 Cathode Ray Tube.

MODEL OL-1
**$29.50***
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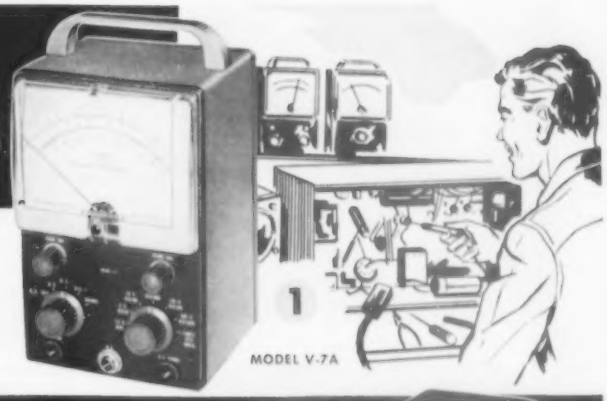
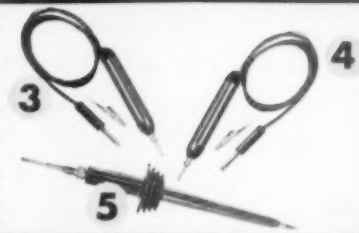
*fill your test requirements*

# WITH HEATHKITS




DESIGNED FOR YOU: *Heath Company test equipment is designed for the maximum in convenience. Besides being functional, Heathkits represent the very latest in modern physical appearance, and incorporate all the latest circuit design features for comprehensive test coverage.*



## 1 *Heathkit* ETCHED CIRCUIT VACUUM TUBE VOLTMETER KIT

Besides measuring AC (rms), DC and resistance, the modern-design V-7A incorporates peak-to-peak measurement for FM and television servicing.

AC (rms) and DC voltage ranges are 1.5, 5, 15, 50, 150, 500, and 1500. Peak-to-peak AC voltage ranges are 4, 14, 40, 140, 400, 1400, and 4000. Ohmmeter ranges are X1, X10, X100, X1000, X10K, X100K, and X1 megohm. Also a db scale is provided. A polarity reversing switch provided for DC measurements, and zero center operation within range of front panel controls. Employs a 200 μa meter for indication. Input impedance is 11 megohms.

Etched metal, pre-wired circuit board for fast, easy assembly and reliable operation is 50% thicker for more rugged physical construction. 1% precision resistors for utmost accuracy.

MODEL V-7A
**$24.50***
Shpg. Wt. 7 Lbs.

## 2 *Heathkit* 20,000 OHMS/VOLT MULTIMETER KIT

The MM-1 is a portable instrument for outside servicing, for field testing, or for quick portability in the service shop. Combines attractive physical appearance with functional design. 20,000 ohms/v. DC, and 5000 ohms/v. AC. AC and DC voltage ranges are 0-1.5, 5, 50, 150, 500, 1500 and 5000 volts. Direct current ranges are 0-150 μa., 15 ma., 150 ma., 500 ma., and 15 amperes. Resistance ranges are X1, X100, X10,000 providing center scale readings of 15, 1500 and 150,000 ohms. DB ranges cover −10 db to +65 db.

Features a 4½" 50 μa. meter. Provides polarity reversal on DC measurements. 1% precision resistors used in multiplier circuits. Not affected by RF fields.

MODEL MM-1
**$29.50***
Shpg. Wt. 6 Lbs.

## 3 *Heathkit* ETCHED CIRCUIT RF PROBE KIT

The Heathkit RF Probe used in conjunction with any 11 megohm VTVM will permit RF measurements up to 250 Mc with ± 10% accuracy. Uses etched circuits for increased circuit stability and ease of assembly.

NO. 309-C
**$3.50***
Shpg. Wt. 1 Lb.

## 4 *Heathkit* ETCHED CIRCUIT PEAK-TO-PEAK PROBE KIT

Now read peak-to-peak voltages on the DC scale of any 11 megohm VTVM with this new probe, employing etched circuit for stability and low loss. Readings made directly from VTVM scales, from 5 Kc to 5 Mc. Not required for Heathkit Model V-7A VTVM.

NO. 338-C
**$5.50***
Shpg. Wt. 2 Lbs.

## 5 *Heathkit* 30,000 VOLT D.C. HIGH VOLTAGE PROBE KIT

For TV service work or similar application for measurement of high DC voltage. Precision multiplier resistor mounted inside plastic probe. Multiplication factor of 100 on the ranges of Heathkit 11 megohm VTVM.

NO. 336
**$4.50***
Shpg. Wt. 2 Lbs.

## 6 *Heathkit* HANDITESTER KIT

The Model M-1 measures AC or DC voltage at 0-10, 30, 300, 1000, and 5000 volts. Measures direct current at 0-10 ma. and 0-100 ma. Provides ohmmeter ranges of 0-2000 (30 ohm center scale) and 0-300,000 ohms (3000 ohms center scale). Features a 400 μa. meter for sensitivity of 1000 ohms/volt. Because of its size, the M-1 is a very handy portable instrument that will fit in your coat pocket, tool box, glove compartment, or desk drawer. Makes a fine standby unit in the service shop when the main instruments are in use, or is ideal for the hobbyist or beginner. An unusual dollar value.

MODEL M-1
**$14.50***
Shpg. Wt. 3 Lbs.

**HEATH COMPANY** *A Subsidiary of Daystrom, Inc.* **BENTON HARBOR 20, MICHIGAN**

# Heathkit TV ALIGNMENT GENERATOR KIT

The Model TS-4 features a controllable inductor for all-electronic sweep, improved oscillator and automatic gain circuitry, high RF output, center sweep operation, and improved linearity. It sets a new high standard for sweep generator operation, and is absolutely essential for the up-to-date service shop doing FM, black-and-white TV, and color TV work.

Voltage regulation and effective AGC action insure flat output over a wide frequency range. Electronic sweep insures complete absence of mechanical vibration. Sweep deviation controllable from 0 up to 40 Mc, depending upon base frequency. Effective two-way blanking.

Fundamental output from 3.6 Mc to 220 Mc in 4 bands. Crystal marker provides markers at 4.5 Mc and multiples thereof. Crystal included with kit. Variable marker covers from 19 Mc to 60 Mc on fundamentals, and up to 180 Mc on harmonics. Provision for external marker.

MODEL TS-4
**$49.50**
Shpg. Wt. 16 Lbs.

## 1 Heathkit LINEARITY PATTERN GENERATOR KIT

The new-design Model LP-1 produces vertical or horizontal bar patterns, a cross-hatch pattern, or white dots on the screen of the TV set under test. No internal connections required. Special clip is attached to the TV antenna terminals. Instant selection of the pattern desired for adjustment of vertical and horizontal linearity, picture size, aspect ratio, and focus. Dot pattern presentation is a *must* for color convergence adjustments on color TV sets.

Extended operating range covers all television channels from 2 to 13. Produces 6 to 12 vertical bars or 4 to 7 horizontal bars.

MODEL LP-1
**$22.50**
Shpg. Wt. 7 Lbs.

## 2 Heathkit LABORATORY GENERATOR KIT

The Heathkit Model LG-1 Laboratory Generator is a high-accuracy signal source for applications where metered performance is essential. It covers from 100 Kc to 30 Mc on fundamentals in 5 bands. Modulation is at 400 cycles, and modulation is variable from 0-50%. RF output from 100,000 μv. to 1 μv. 200 μa. meter reads the RF output in microvolts, or percentage of modulation. Fixed step and variable output attenuation provided.

Features voltage regulation, and double copper plated shielding for stability. Provision for external modulation. Coaxial output cable (50 ohms).

MODEL LG-1
**$39.50**
Shpg. Wt. 16 Lbs.

## 3 Heathkit CATHODE RAY TUBE CHECKER KIT

This new-design instrument holds the key to rapid and complete picture tube testing, either in the set, on the work-bench, or in the carton. Tests for shorts, leakage, and emission. Features Shadowgraph test (a spot of light on the screen) to indicate whether the tube is capable of functioning.

The Model CC-1 tests all electromagnetic deflection picture tubes normally encountered in television servicing. Supplies all operating voltages to the tube under test, and indicates the condition of the tube on a large "GOOD-BAD" scale. Features spring loaded test switches for operator protection.

The CC-1 is housed in an attractive portable case and is light in weight -- ideal for outside service calls.

MODEL CC-1
**$22.50**
Shpg. Wt. 10 Lbs.

## 4 Heathkit DIRECT READING CAPACITY METER KIT

Not only is this instrument popular in the service shop, but it has found extensive application in industrial situations. Ideal for quality control work, production line checking, or for matching pairs.

Features direct reading linear scales from 100 mmf to .1 mfd full scale. Necessary only to connect a capacitor of unknown value to the insulated binding posts, select the correct range, and read the meter. The CM-1 is not susceptible to hand capacity, and has a residual capacity of less than 1 mmf.

MODEL CM-1
**$29.50**
Shpg. Wt. 7 Lbs.

**HEATH COMPANY**
A SUBSIDIARY OF DAYSTROM INC.

**BENTON HARBOR 20, MICHIGAN**

# Heathkit SIGNAL GENERATOR KIT

MODEL SG-8
Shpg. Wt. 8 Lbs.
**$19.50**

This is one of the biggest signal generator bargains available today. The tried and proven Model SG-8 offers all of the outstanding features required for a basic service instrument. High quality components and outstanding performance.

The SG-8 covers 160 Kc to 110 Mc on fundamentals in 5 bands, and calibrated harmonics extend its usefulness up to 220 Mc. The output signal is modulated at 400 cps, and the RF output is in excess of 100,000 uv. Output controlled by both a continuously variable and a fixed step attenuator. Also, audio output may be obtained for amplifier testing. Don't let the low price deceive you. This is a professional type service instrument to fulfill the signal source requirements in the service lab.

1

## 1 Heathkit . . . IMPEDANCE BRIDGE KIT

The IB-2 features built-in adjustable phase shift oscillator and amplifier, and has panel provisions for external generator. Measures resistance, capacitance, inductance, dissipation factors of condensers, and storage factor of inductance.

D, Q, and DQ functions combined in one control. ½% resistors and ½% silver-mica capacitors especially selected for this instrument. A 100-0-100 microammeter provides null indications. Two-section CRL dial provides 10 separate "units" with an accuracy of .5%. Fractions of units read on variable control.

MODEL IB-2
**$59.50**
Shpg. Wt. 12 Lbs.

2

## 2 Heathkit "Q" METER KIT

The Heathkit Model QM-1 will measure the Q of inductances and the RF resistance and distributed capacity of coils. Employs a 4½" 50 microampere meter for direct indication. Will test at frequencies of 150 Kc to 18 Mc in 4 ranges. Measures capacity from 40 mmf to 450 mmf within ± 3 mmf. Indispensible for coil winding and determining unknown condenser values. A worthwhile addition to your laboratory at an outstandingly low price. Useful for checking wave traps, chokes, peaking coils, etc. Laboratory facilities are now available to the service shop and home lab.

MODEL QM-1
**$44.50**
Shpg. Wt. 14 Lbs.

3

## 3 Heathkit 6–12 VOLT BATTERY ELIMINATOR KIT

This modern battery eliminator will supply 6 or 12 volt output for ordinary automobile radios as well as 12 volts for the new models in the latest model cars. Output voltage is variable from 0-8 volts DC, or 0-16 volts DC. Will deliver up to 15 amperes at 6 volts, or up to 7 amperes at 12 volts. Two 10,000 microfarad filter capacitors insure smooth DC output. Two panel meters monitor output voltage and current. Will double as a battery charger. Definitely required for automobile radio service work.

MODEL BE-4
**$31.50**
Shpg. Wt. 17 Lbs.

4 5 6

## 4 Heathkit DECADE RESISTANCE KIT

Twenty 1% precision resistors provide resistance from 1 to 99,999 ohms in 1 ohm steps. Indispensible around service shop laboratory, ham shack, or home workshop. Well worth the extremely low Heathkit price.

MODEL DR-1
**$19.50**
Shpg. Wt. 4 Lbs.

## 5 Heathkit VIBRATOR TESTER KIT

Tests vibrators for proper starting and indicates the quality of the output on a large "GOOD-BAD" scale. Checks both interrupter and self-rectifier types in 5 different sockets. Operates from any battery eliminator delivering variable voltage from 4 to 6 volts DC at 4 amps. Ideal companion to the Model BE-4.

MODEL VT-1
**$14.50**
Shpg. Wt. 6 Lbs.

## 6 Heathkit DECADE CONDENSER KIT

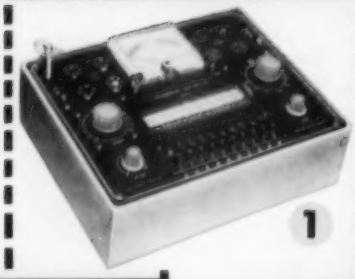
Provides capacity values from 100 mmf to 0.111 mfd in steps of 100 mmf. ± 1% precision silver-mica condensers used. High quality ceramic switches for reduced leakage. Polished birch cabinet. Extremely valuable in all electronic activity.

MODEL DC-1
**$16.50**
Shpg. Wt. 3 Lbs.

**HEATH COMPANY**
A SUBSIDIARY OF DAYSTROM, INC.

**BENTON HARBOR 20, MICHIGAN**

# *Heathkit* TUBE CHECKER KIT




**1** The Heathkit Model TC-2 is an emission type tube tester that represents a tremendous saving over the price of a comparable unit from any other source. At only $29.50, you can have a tube tester of your own, even if you are an experimenter, or only do part time service work. Extremely popular with radio servicemen, it uses a 4½" meter with 3-color meter face for simple "GOOD-BAD" indications that the customer can understand. Will test all tubes commonly encountered in radio and TV service work.

Ten 3-position lever switches for "open" or "short" tests on each tube element. Neon bulb indicates filament continuity or short between tube elements. Line adjust control provided. The roll chart is illuminated.

Sockets provided for 4, 5, 6, and 7-pin, octal, and loctal tubes, 7 and 9 pin miniature tubes, and the 5 pin Hytron tubes. Blank space provided for future socket addition. Tests tubes for opens, and shorts, and for quality on the basis of total emission. 14 different filament voltage values provided.

MODEL TC-2
**$29.50**
Shpg. Wt. 12 Lbs.

**2** *Heathkit* **PORTABLE TUBE CHECKER KIT**

The Model TC-2P is identical to the Model TC-2 except that it is housed in a rugged carrying case. This strikingly attractive and practical two-tone case is finished in proxylin impregnated fabric. The cover is detachable, and the hardware is brass plated. This case imparts a real professional appearance to the instrument. Ideal for home service calls, or any portable application.

MODEL TC-2P
**$34.50**
Shpg. Wt. 15 Lbs.

**3** *Heathkit* **TV PICTURE TUBE TEST ADAPTER**

The Heathkit TV picture tube test adapter is designed for use with the Model TC-2 Tube Checker. Test picture tubes for emission, shorts, and thereby determine tube quality. Consists of 12-pin TV tube socket, 4 ft. cable, octal connector, and necessary technical data. (Not a kit.)

MODEL 355
**$4.50**
Shpg. Wt. 1 Lb.

**4** *Heathkit* . . .

**CONDENSER CHECKER KIT**

Use this Condenser Checker to quickly and accurately measure those unknown condenser and resistor values. All readings taken directly from the calibrated panel scales without any involved calculation. Capacity measurements in four ranges from .00001 to 1000 mfds. Checks paper, mica, ceramic and electrolytic condensers. A power factor control is available for accurate indication of electrolytic condenser efficiency. Leakage test switch—selection of five polarizing voltages, 25 volts to 450 volts DC to indicate condenser operating quality under actual load conditions. Spring-return test switch automatically discharges condenser under test and eliminates shock hazard to the operator.

Resistance measurements can be made in the range from 100 ohms to 5 megohms. Here again, all values are read directly on the calibrated scales. Increased sensitivity coupled with an electron beam null indicator increases overall instrument usefulness.

For safety of operation, the circuit is entirely transformer operated. An outstanding low kit price for this surprisingly accurate instrument.

MODEL C-3
**$19.50**
Shpg. Wt. 7 Lbs.

**5** *Heathkit* VISUAL-AURAL

**SIGNAL TRACER KIT**

This signal tracer is extremely valuable in servicing AM, FM, and TV receivers, especially when it comes to isolating trouble to a particular stage of the circuit under test.

This visual-aural tracer features a high gain RF input channel to permit signal tracing from the receiver antenna input clear through all RF, IF, detector, and audio stages to the speaker. Separate low-gain channel provided for audio circuit exploration. Both visual and aural indication by means of a speaker or headphone, and electron beam "eye" tube as a level indicator. Also incorporates a noise locater circuit for DC noise checks, and a built-in calibrated wattmeter (30-500 watts). Panel terminals provided for "patching" output transformer or speaker into external circuit for test purposes. Designed especially for the radio and TV serviceman. Cabinet size: 9½" wide x 6½" high x 5" deep. A real test equipment bargain.

MODEL T-3
**$23.50**
Shpg. Wt. 9 Lbs.

**HEATH COMPANY**
A SUBSIDIARY OF DAYSTROM INC

**BENTON HARBOR 20, MICHIGAN**

MODEL HD-1

Shpg. Wt. 13 Lbs. **$49.50**

Used with a sine wave generator, the Model HD-1 will check the harmonic distortion output of audio amplifiers under a variety of conditions. Reads distortion directly on the meter as a percentage of the input signal. Operates between 20 and 20,000 cps. High impedance VTVM circuit for initial reference settings and final distortion readings. Ranges are 0-1, 3, 10, and 30 volts full scale. 1% precision resistors. Distortion scales are 0-1, 3, 10, 30 and 100% full scale. Requires only .3 volt input for distortion test.

## *Heathkit* HARMONIC DISTORTION METER KIT

### ❶ *Heathkit* AUDIO ANALYZER KIT

This instrument consists of an audio wattmeter, an AC VTVM, and a complete IM analyzer, all in one compact unit.

Use the VTVM to measure noise, frequency response, output gain, power supply ripple, etc. Use the wattmeter for measurement of power output. Internal loads provided for 4, 8, 16, or 600 ohms. VTVM also calibrated for DBM units. High or low impedance IM measurements made with built-in 6KC and 60 cps generators. VTVM ranges are .01, to 300 volts in 10 steps. Wattmeter ranges are .15 mw. to 150 w. in 7 steps. IM scales are 1% to 100% in 5 steps.

MODEL AA-1 **$59.50** Shpg. Wt. 13 Lbs.

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### ❷ *Heathkit* AUDIO GENERATOR KIT

This new Heathkit Model features step-tuning from 10 cps to 100 Kc with three rotary switches that provide two significant figures and multiplier. Less than .1% distortion. Frequency accurate to within ± 5%.

Output monitored on a large 4½" meter that reads voltage or db. Both variable and step-type attenuation provided. Meter reads zero-to-maximum at each attenuator position. Output ranges (and therefore meter ranges) are 0-.003, .01, .03, .1, .3, 1, 3, 10 volts. Step-tuning provides rapid positive selection of the desired frequency, and allows accurate return to any given frequency.

MODEL AG-9 **$34.50** Shpg. Wt. 8 Lbs.

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### ❸ *Heathkit* AUDIO OSCILLATOR KIT

(SINE WAVE — SQUARE WAVE)

The Model AO-1 features sine wave or square wave coverage from 20-20,000 cps in 3 ranges. It is an instrument specifically designed to completely fulfill the needs of the serviceman and high fidelity enthusiast. Offers high level output across the entire frequency range, low distortion and low impedance output. Features a thermistor in the second amplifier stage to maintain essentially flat output through the entire frequency range. Produces an excellent sine wave for audio testing, or will produce good, clean, square waves with a rise time of only 2 microseconds.

MODEL AO-1 **$24.50** Shpg. Wt. 10 Lbs.

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### ❹ *Heathkit* RESISTANCE SUBSTITUTION BOX KIT...

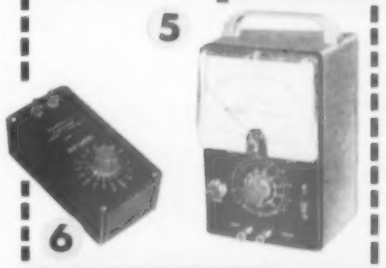
Provides switch selection of 36 RTMA 1 watt standard 1% resistors ranging from 15 ohms to 10 megohms. Numerous applications in radio and TV work, and essential in the developmental laboratory.

MODEL RS-1 **$5.50** Shpg. Wt. 2 Lbs.

### ❺ *Heathkit* AC VACUUM TUBE VOLTMETER KIT...

The Heathkit AC VTVM features high impedance, wide frequency range, very high sensitivity, and extremely wide voltage range. Will accurately measure a voltage as small as 1 mv. at high impedance. Excellent for sensitive AC measurements required by laboratories, audio enthusiasts and experimenters. Frequency response is substantially flat from 10 cps to 50 Kc. Ranges are .01, .03, .1, .3, 1, 3, 10, 30, 100, and 300 v. RMS. Total db range −52 to + 52 db. Input impedance 1 megohm at 1 Kc.

MODEL AV-2 **$29.50** Shpg. Wt. 5 Lbs.



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### ❻ *Heathkit* CONDENSER SUBSTITUTION BOX KIT...

Very popular companion to Heathkit RS-1. Individual selection of 18 RTMA standard condenser values from .0001 mfd to .22 mfd. Includes 18" flexible leads with alligator clips.

MODEL CS-1 **$5.50** Shpg. Wt. 2 Lbs.

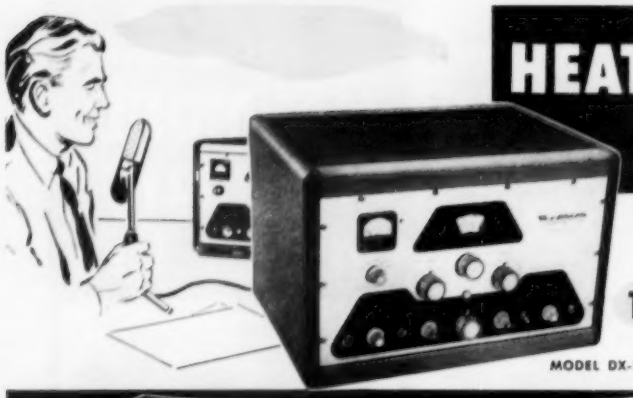
**HEATH COMPANY**

A SUBSIDIARY OF DAYSTROM INC.

**BENTON HARBOR 20, MICHIGAN**

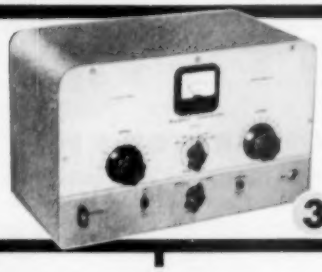
# HEATHKIT HAM GEAR

*for high quality at moderate cost*



MODEL DX-100

DOLLAR VALUE: *You get more for your Heathkit dollar because your labor is used to build the kit instead of paying for someone else's. Also, the middleman's margin of profit is eliminated when you deal directly with the manufacturer.*



## 1 *Heathkit* DX-100 PHONE & CW TRANSMITTER KIT

The reception given this amateur transmitter has been tremendous. Reports from radio amateurs using the DX-100 are enthusiastic in praising its performance and the high quality of the components used in its assembly. Actual "on the air" results reflect the careful design that went into its development.

The DX-100 features a built-in VFO, modulator, and power supplies, and is completely bandswitching for phone or CW operation on 160, 80, 40, 20, 15, 11, and 10 meters. All parts necessary for construction are supplied in the kit, including tubes, cabinet, and detailed step-by-step instructions. Easy to build, and a genuine pleasure to operate.

Employs push-pull 1625's modulating parallel 6146's for RF output in excess of 100 watts on phone and 120 watts on CW. May be excited from the built-in VFO or from crystals (crystals not included with kit). Features five-point TVI suppression: (1) pi network interstage coupling to reduce harmonic transfer to the final stage; (2) pi network output coupling; (3) extensive shielding; (4) all incoming and outgoing circuits filtered; (5) inter-locking cabinet seams to eliminate radiation except through the coaxial output connector. Pi network output coupling will match 50 to 600 ohm non-reactive load. Illuminated VFO dial and meter face. Remote control socket provided.

The chassis is made of extra-strong #16 gauge copper-plated steel. It employs potted transformers, ceramic switch and variable capacitor insulation, solid silver loading switch terminals, and high-grade well-rated components throughout. Features a pre-formed wiring harness, and all coils are pre-wound.

High-gain speech amplifier for dynamic or crystal microphones, and restricted speech range for increased intelligence. Plenty of audio power reserve. Measures 20⅞" W. x 13¾" H. x 16" D. Schematic diagram and complete technical specifications on request.

MODEL DX-100
**$189.50**
Shpg. Wt. 120 Lbs.

Shipped Motor Freight Unless Otherwise Specified
$50.00 Deposit Required on C.O.D. Orders

## 2 *Heathkit* VFO KIT

The Model VF-1 covers 160-80-40-20-15-11 and 10 meters with three basic oscillator frequencies. Better than 10-volt average RF output on fundamentals. Features illuminated and pre-calibrated dial scale. Cable and plug provided to fit crystal socket of any modern transmitter.

Enjoy the convenience and flexibility of VFO operation at no more than the price of crystals. May be powered from plug on the Heathkit Model AT-1 transmitter, or supplied with power from most transmitters. Measures: 7" H. x 6½" W. x 7" D.

MODEL VF-1
**$19.50**
Shpg. Wt. 7 Lbs.

## 3 *Heathkit* CW AMATEUR TRANSMITTER KIT

The Model AT-1 is an ideal novice transmitter, and may be used to excite a higher power rig later on.

This CW transmitter is complete with its own power supply, and covers 80, 40, 20, 15, 11, and 10 meters. Features single-knob bandswitching, and panel meter indicates grid or plate current for the final amplifier. Designed for crystal operation or external VFO. Crystal not included in kit. Incorporates such features as key click filter, line filter, copper-plated chassis, pre-wound coils, 52 ohm coaxial output, and high quality components throughout. Instruction book simplifies assembly. Employs a 6AG7 oscillator, 6L6 final amplifier. Operates up to 35 watts plate power input.

MODEL AT-1
**$29.50**
Shpg. Wt. 15 Lbs.

## 4 *Heathkit* . . . ANTENNA COUPLER KIT

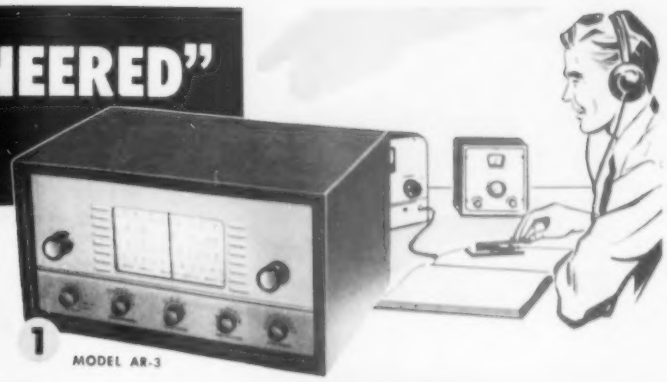
The Model AC-1 will properly match your low power transmitter to an end-fed long wire antenna. Also attenuates signals above 36 Mc, reducing TVI. 52 ohm coax. input→ power up to 75 watts—10 through 80 meters—tapped inductor and variable condenser—neon RF indicator—copper plated chassis and high quality components. Ideal for use with Heathkit AT-1 Transmitter.

MODEL AC-1
**$14.50**
Shpg. Wt. 4 Lbs.

**HEATH COMPANY** *A Subsidiary of Daystrom, Inc.* **BENTON HARBOR 20, MICHIGAN**

# "AMATEUR-ENGINEERED"

*Equipment For The Ham*



MODERN DESIGN: *You can be sure of getting all the latest and most desirable design features when you buy Heathkits. Advanced-design is a minimum standard for new Heathkit models.*

1 MODEL AR-3

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## 1 *Heathkit* COMMUNICATIONS-TYPE ALL BAND RECEIVER KIT

The new Model AR-3 features improved IF and RF performance, along with better image rejection on all bands. Completely new chassis layout for easier assembly, even for the beginner

Covers 550 Kc to 30 Mc in four bands. Provides sharp tuning and good sensitivity over the entire range. Features a transformer-type power supply–electrical bandspread–separate RF and AF gain controls–antenna trimmer–noise limiter–AGC–BFO–headphone jacks–5½" PM speaker and illuminated tuning dial.

CABINET: Fabric covered cabinet with aluminum panel as shown. Part No. 91-10, shipping weight 5 lbs. $4.50.

MODEL AR-3
**$27.95***
Shpg. Wt. 12 Lbs.
(Less Cabinet)

## 2 *Heathkit* "Q" MULTIPLIER KIT

Here is the Heathkit Q Multiplier you hams have been asking for. A tremendous help on the phone and CW bands when the QRM is heavy. Provides an effective Q of approximately 4,000 for extremely sharp "peak" or "null." Use it to "peak" the desired signal or to "null" an undesired signal, or heterodyne. Tunes to any signal within the IF band-pass of your receiver. Also provides "broad peak" for conditions where extreme selectivity is not required.

Operates with any receiver having an IF frequency between 450 and 460 Kc. Will not function with AC-DC type receivers. Requires 6.3 volts AC at 300 ma. and 150 to 250 VDC at 2 ma. Derives operating power from your receiver. Uses a 12AX7 tube, and special High-Q shielded coils. Simple to connect with the cable and plugs supplied. Measures only 4-11/16"H.x7⅜"W.x4⅛"D. A really valuable addition to the receiving equipment in your ham shack.

MODEL QF-1
**$9.95***
Shpg. Wt. 3 Lbs.

## 3 *Heathkit* VARIABLE VOLTAGE REGULATED POWER SUPPY KIT

Provides well filtered DC output, variable from zero to 500 volts at no load and *regulated* for stability. Will supply up to 10 ma. at 450 VDC, and up to 130 ma. at 200 VDC. Voltage or current monitored on front panel meter. Also provides 6.3 VAC at 4A. for filament. Filament voltage isolated from B+, and both isolated from ground. Invaluable around the ham shack for supplying operating potentials to experimental circuits. Use in all types of research and development laboratories as a temporary power supply, and to determine design requirements for ultimate power supply.

MODEL PS-3
**$35.50***
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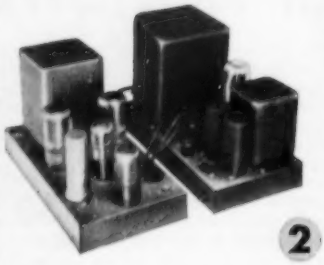

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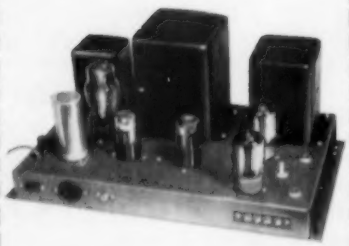

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MODEL WA-P2
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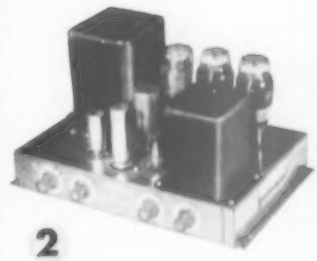

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MODEL A-7D
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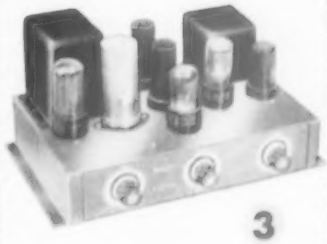

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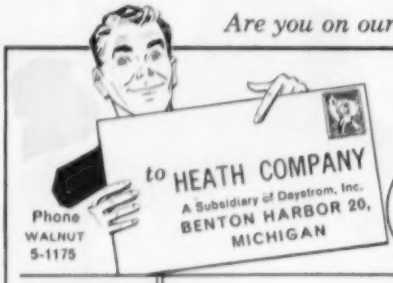


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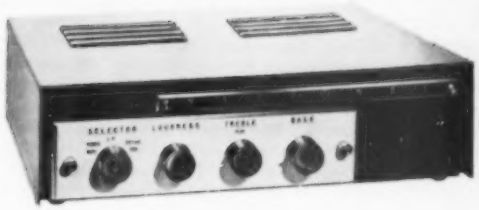

The National Horizon 10-watt amplifier.

By ROBERT F. SCOTT
TECHNICAL EDITOR

# Circuit Features in HI-FI Power AMPLIFIERS

*Circuit analysis of the single-ended push-pull amplifier in National's Horizon series*

IN the preceding installment (August) we saw how the McIntosh unity-coupled output circuit solves the problem of switching transients and notch distortion caused by high leakage reactance in output transformers in class-AB and -B service. A different solution is offered by Drs. Donald B. Sinclair and Arnold P. G. Peterson. Theirs is the *single-ended push-pull* circuit used in the National Company's Horizon 10 and Horizon 20 amplifiers.

In the conventional push-pull circuit (Fig. 1) the tubes develop a.c. signal voltages that are series-aiding across the load while the plates are paralleled across the d.c. supply. The new single-ended push-pull circuit is the dual or converse of the conventional in that the tubes are in series for d.c. and supply the load in parallel. Thus the optimum load impedance—as in the McIntosh circuit—is only one-quarter of the plate-to-plate load in the usual push-pull connection.

Fig. 2 shows a basic form of the new circuit. The tubes are in series across a d.c. supply with the load connected between a tap on the B supply and the plate–cathode junction. Although the load is in its cathode circuit, we cannot consider V1 as a cathode follower because the signal voltage is applied between the grid and cathode rather than between grid and ground as in a cathode follower. The load also appears in the plate circuit of V2 which, like V1, has its grid driving signal applied between grid and cathode.

The voltages at the ends of the secondary of a transformer are 180° out of phase, so that connections to secondary No. 2 are transposed to show that the grids of V1 and V2 are driven in the same manner as in Fig. 1.

The basic single-ended push-pull amplifier with signal voltages supplied by a phase inverter is shown in Fig. 3. We have retained the dual power supply of Fig. 2. Grid excitation for V1 is developed across R1, the phase inverter plate load resistor and the grid return for V1. By careful selection of operating conditions we can use this direct-coupled circuit with V1 being biased by the drop across R1. Tube V2 is driven by an equal but 180°-out-of-phase signal voltage across R2 in the phase inverter cathode return. Battery BA1 supplies operating bias for V2 because grounding R2 directly would make V2's grid positive with respect to its cathode.

Two of the three d.c. supplies can be eliminated by using the variation in Fig. 4. Battery BA1 is eliminated by using the drop across R3 as cathode bias for V2. Batteries BA2 and BA3 are replaced by a single supply (BA4) delivering a voltage equal to that of BA2 and BA3 in series. The load is connected between the plate–cathode junction and the junction of two large capacitors (C1 and C2) in series across BA4.

Fig. 5 illustrates another variation of the basic circuit. This is used when one side of the load must be grounded.

Although the optimum load impedance of these circuits is only one-quarter that used in conventional push-pull operation, it is still too high for direct coupling to voice coils in the conventional impedance range. A single 6A7-G used for VI and V2 has an optimum load impedance of around 280 ohms and it may be used to drive two 500-ohm speakers (Stephens or equivalent) in parallel through a direct connection. However, we must still use an output transformer for matching speakers with voice coil impedances in the range of 4 to 16 ohms.

Fig. 6 is the equivalent circuit of Fig. 4 with pentode output tubes transformer-coupled to the load. The output transformer has a split primary. Screen-to-cathode bypass capacitors C1 and C2 and filter capacitor C3 effectively connect the halves of the primary in parallel for audio signal voltages.

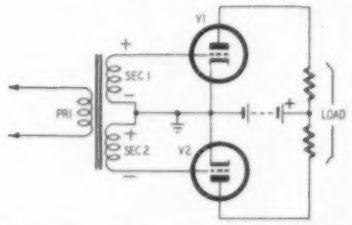


Fig. 1—Conventional push-pull circuit.

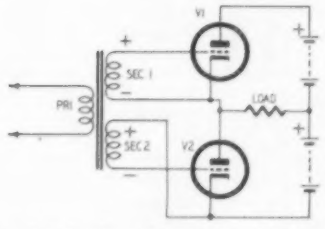


Fig. 2—Single-ended push-pull circuit.

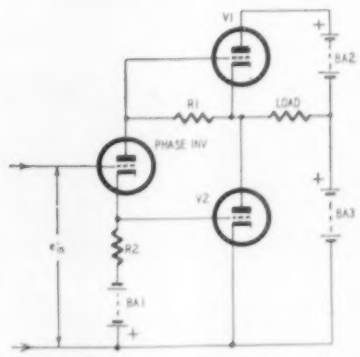


Fig. 3—Phase inverter feeds amplifier.

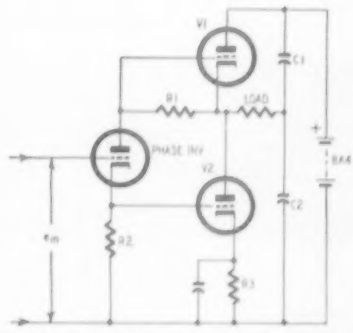


Fig. 4—Amplifier uses single battery.

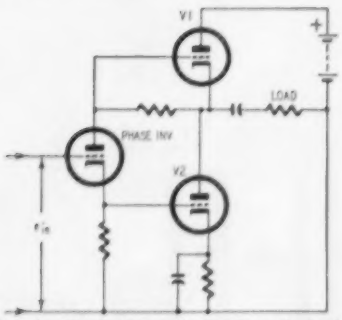


**Fig. 5—Variation of single-ended circuit—one side of the load is grounded.**

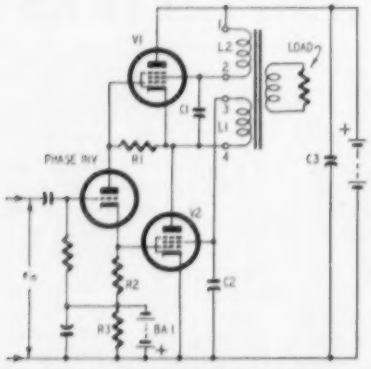


**Fig. 6—Single-ended circuit using pentodes transformer-coupled to the load.**

Refer to the simplified circuit in Fig. 7. Since the capacitors, at audio frequencies, provide a direct connection, the designers have in effect used capacitive unity coupling and eliminated the need for magnetic coupling. (The designers reported that they verified the fact that magnetic coupling is not needed by using separate chokes in place of the split primary.) Thus, switching transients and notch distortion caused by insufficient magnetic coupling can be eliminated with this circuit.

As in Figs. 2 and 3, V1 and V2 (Fig. 6) are excited by signal voltages applied between their grids and cathodes. The phase inverter tube take its plate supply voltage from the center of the series-connected output tubes. If its load resistor (R1) is connected directly to the B supply, V1's grid excitation voltage would appear between grid and ground thus causing it to operate as a cathode follower. In the Fig. 6 circuit the signal voltage for V1 develops across R1 and that for V2 across R2. Battery BA1 supplies a negative bias voltage that opposes the d.c. drop across R2 and prevents V2's grid from going positive with respect to the cathode. A large filter capacitor prevents an a.c. signal voltage from developing across BA1 and R3.

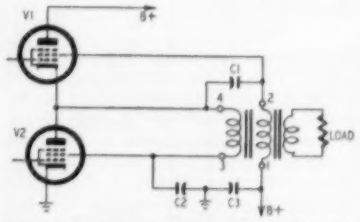


**Fig. 7—The capacitors effectively place the primary halves in parallel.**

The screen grid of V1 is supplied by current flowing through L2 from the B supply line, and V2's screen is supplied from the plate–cathode junction through winding L1. The connections are polarized so the magnetic fields produced by the screen currents oppose and cancel each other.

The circuit in Fig. 6 requires twice the voltage and half the current needed for the same tubes in a conventional circuit so the power input is the same for either type. But this particular variation has the disadvantage of requiring power supply and filter components with twice the normal voltage ratings.

### The Horizon series amplifiers

The need for twice-normal plate supply voltage is eliminated by wiring the circuit so direct tube currents flow through the primary windings as in National Company's Horizon 10 and Horizon 20 amplifiers. The circuit of the 10-watt Horizon 10 in Fig. 8 is a simplified version of the experimental 25- and 50-watt amplifiers described by Peterson and Sinclair in *The General*

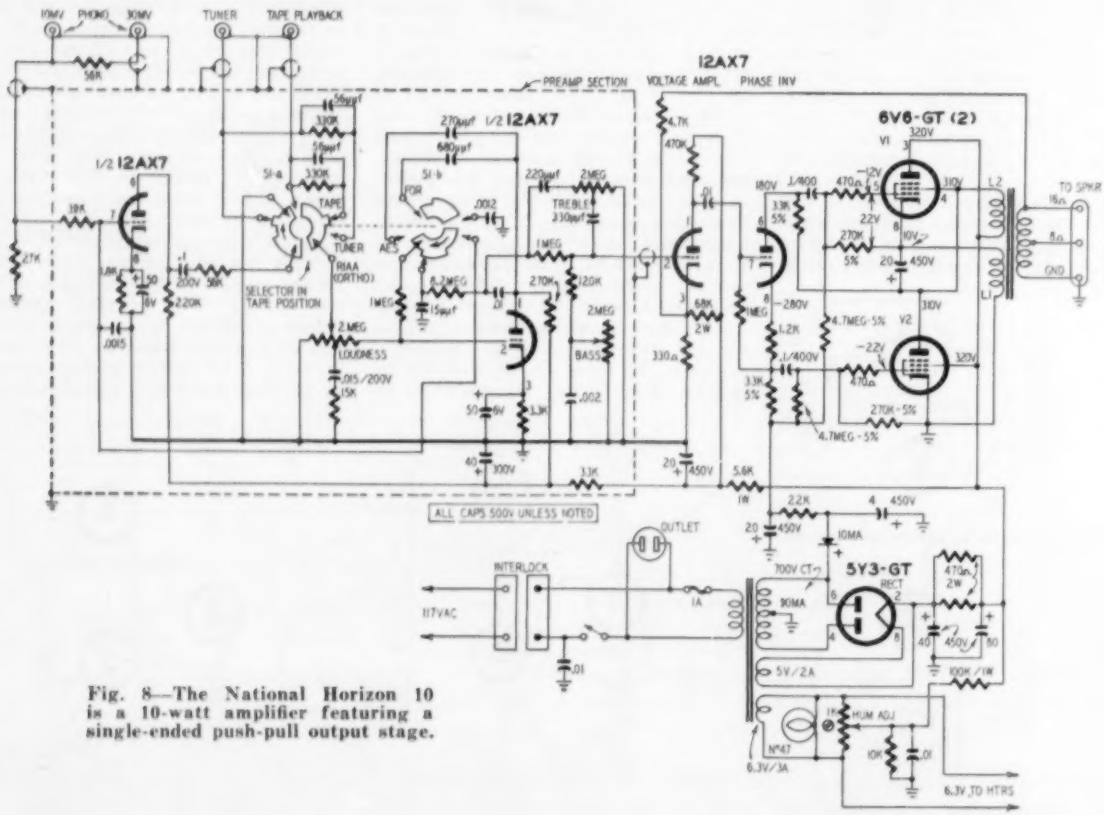


**Fig. 8—The National Horizon 10 is a 10-watt amplifier featuring a single-ended push-pull output stage.**

*Radio Experimenter*, October, 1951, and in the January, 1952, issue of *Proceedings of the IRE*.

Here the plate currents for the phase inverter and V2 and the screen current for V1 flow through L2. The cathode current (sum of plate and screen currents) of V1 flows through L1. This arrangement causes a difference in the direct-current flow in L1 and L2 and results in a d.c. drop across both windings that reduces the supply voltage for V1's screen and the plate of V2. This circuit and current unbalance is minimized by careful design to avoid flux unbalance in the transformer.

Unlike the basic circuits in Figs. 3 to 7, R-C coupling is used between the phase inverter and the grids of V1 and V2 in the Horizon amplifiers. Fixed grid bias is developed by a half-wave selenium rectifier and a simple R-C filter and applied to the output grids.

The plate supply for the phase inverter is taken from the plate–cathode junction of the output tubes. The output signal developed at the plate of V2 is in series with the phase inverter d.c. plate supply and the negative feedback voltage thus developed reduces the distortion and gain in this stage. The loss in phase inverter gain is minimized by returning its cathode load resistor to the bias supply to increase the effective plate voltage.

The voltage amplifier is conventional and uses fixed bias obtained by returning its cathode to a tap on a B plus voltage divider. Distortion in the power amplifier is further reduced by 16 db of negative feedback from the secondary of the output transformer to the voltage amplifier cathode.

### Preamplifier–equalizer

The preamplifier and equalizer section has four input channels. One for a radio tuner, one for playing back tape recordings and two for magnetic phonograph cartridges. The 10-mv phono input channel is for low-output cartridges such as the G-E variable-reluctance type; the 30-mv channel is for high-output types such as the Pickering and Audak. The tape input channel may be used for crystal cartridges and other devices delivering 0.5 volt or more.

The function selector switch has five positions. One for tape, one for radio tuner and three to select the phonograph input circuits and to provide equalization for AES, RIAA and foreign recording characteristics.

The bass control provides a boost beginning at 1 kc and rising to a maximum of 15 db at 30 cycles. The treble control provides a boost that begins at around 800 cycles and rises gradually to flatten out for a maximum of 12 db between 10 and 15 kc. Treble attenuation begins at 1,500 cycles, reaches 3 db at 5 kc and is a maximum of 17 db at 20 kc.

The next installment will discuss the circuitry in the output stages of the Circlotron amplifiers developed by Electro-Voice. END


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# FOR GOLDEN EARS ONLY

*National's Criterion FM-AM tuner; Heathkit audio analyzer; new records review*

By MONITOR

IN some of its advertising National claims a usable sensitivity of 0.5 microvolt for 20 db of quieting for its Criterion tuner (see photo). This seems so unlikely of realization, especially to those who have tried designing and building supersensitive FM receivers, that I have no doubt many informed readers dismissed the claim as an adman's dream. So the first thing I want to report is this: the Criterion is by a long shot the most sensitive FM broadcast receiver I have ever tested or used. It produced regular, reliable and completely acceptable and noise-free reception of stations radiating as little as 5 kw at a distance of 140 air miles (and at least 40 miles beyond line of sight) *with only the indoor antenna supplied with the receiver tacked on the wall 7 feet above ground.*

The Criterion uses a cascode r.f. stage plus no fewer than three stages of i.f. amplification and two limiters. Despite this very high gain, the tuner appears to be completely stable. The r.f. stage seems completely indifferent to the length, type or match of the transmission line, and in some two months of use I found no evidence of regeneration, let alone oscillation. The only spurious response noted was that of a local channel-6 TV station (probably a heterodyne with a very strong local FM station) and that was extremely weak and would not be evident at all on a less sensitive receiver.

The capture ratio is as good as the sensitivity. The claim is that any station 25% stronger than another on the same frequency will suppress the weaker. This claim, too, appears to be realized. In any case there is an unusual freedom from co-channel and adjacent-channel and even multiple-path interference. The selectivity is fully as good as one would expect it to be with four i.f. transformers. The wide-band discriminator, moreover, permits a somewhat narrower i.f. bandwidth for the same or lower distortion level. The combination provides highly satisfactory reception of adjacent-channel stations.

The Heathkit model AA-1 audio analyzer.

The National Criterion AM-FM tuner.

Despite this high sensitivity, selectivity and the absence of a.f.c., the Criterion is just as simple and uncritical to tune as receivers using a.f.c. and just as free of drift distortion. This latitude in tuning and the very low distortion are due to the new discriminator which has an operating curve 2 mc wide instead of the 400 or 500 kc of previous high-quality discriminators. The circuit (Fig. 1) is a sort of a cross between the discriminator and frequency-counting detector and might be called a frequency-differential counter. The discriminator curve is established by coils L1 and L2, one of which is self-resonant at about 9.7 and the other at 11.7 mc. With such a wide discriminator curve, the Criterion provides as good or better latitude against drift and casual tuning as tuners using a.f.c. which usually operate over a range of ± 500 kc. The detector resembles a counter detector at first glance (and has been mistaken for one by experts) but it differs entirely in action though it is just about as free of distortion.

The FM portion uses a squelch in the mutamatic position to suppress interstation noise which, with so sensitive a receiver, is very high. The squelch is adjustable with a control accessible when the name plate on top the cabinet is removed, and I have been able to set it to provide operation on the weakest station capable of giving an acceptable degree of noise-free reception. Like all squelch circuits it produces high subsonic switching transients as it goes in and out of operation. These may well be sufficient to produce momentary motorboating, breathing or overloading with some amplifiers and it might be good advice for National to include a filter to attenuate these transients in future models. (The National Horizon amplifiers have a filter in their input which will do this and minimize rumble and flutter as well.)

Owners of other amplifiers can reduce the transients to a probably safe level simply by adding another resistor of the same value as the present grid leak at the input of the amplifier. With the output capacitor of the tuner or control unit this will provide a double R-C network (which will increase the slope below turnover to 12 db per octave) as shown in Fig. 2.

The AM portion has a sensitivity of about 10 μv—more than sufficient for today's conditions on the broadcast

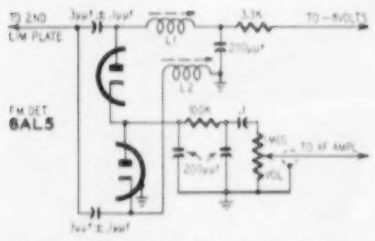



Fig. 1—Schematic of the FM detector.

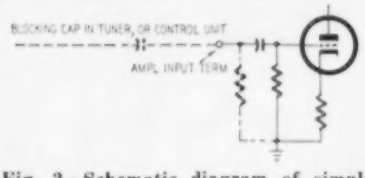
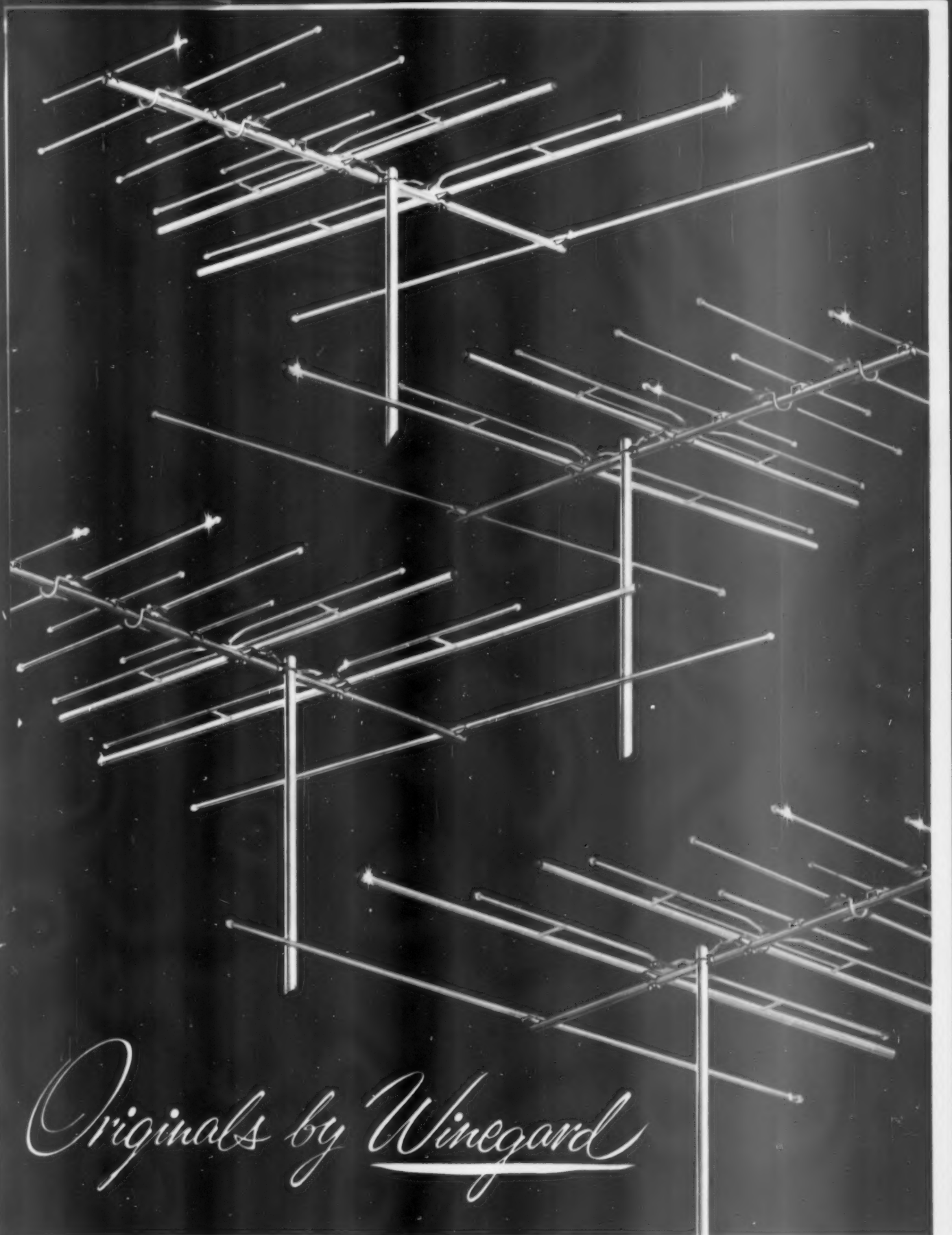



Fig. 2—Schematic diagram of simple circuit for reducing switching transients.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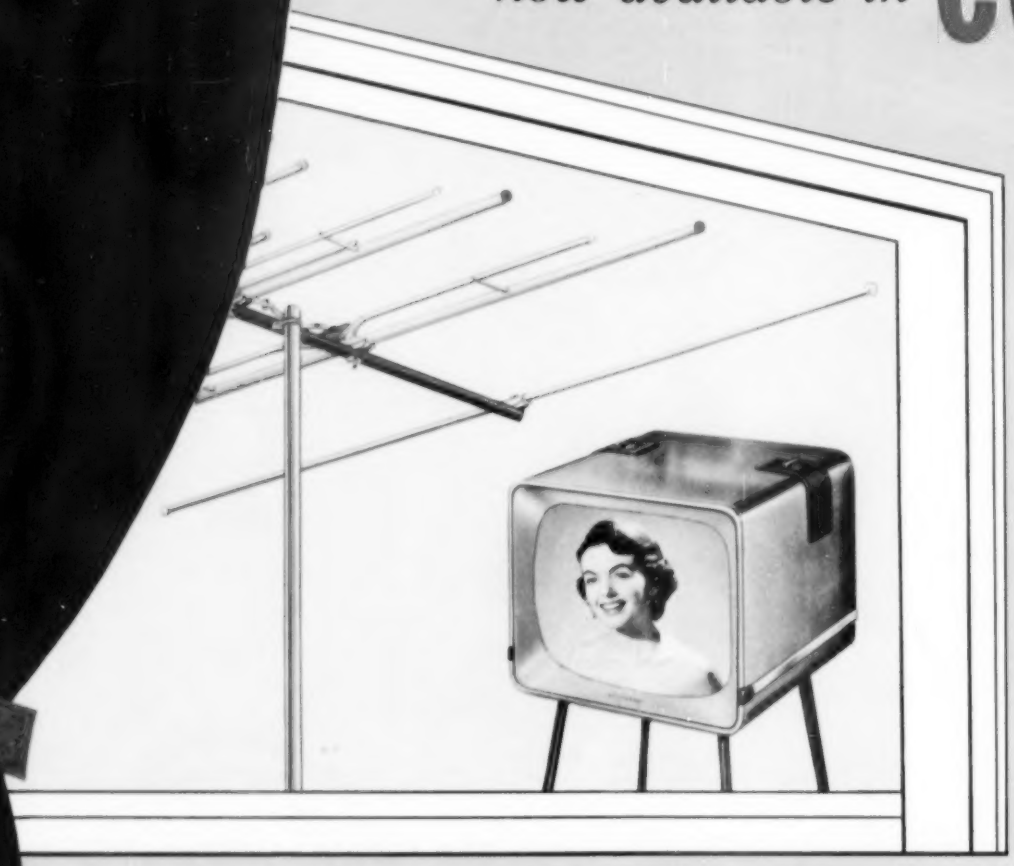

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band. In fact, in most locations it may be advisable to use nearly a 2- or 3-foot length of wire for the antenna, to reduce co-channel interference. A novel feature is that although both AM and FM use the same i.f. channel, both can be used simultaneously and independently. This provides a means for binaural reception in cities like New York where WQXR often offers binaural broadcasts with one channel on AM and the other on FM. AM and FM are tuned with separate knobs and have individual volume controls. Each has its individual dial scale and pointer. There is also an output to provide FM multiplex reception when and if such transmissions should become a reality, and there is a takeoff point for a tape recorder as well.

The Criterion will accept the National preamp control unit and with it makes a highly convenient and compact control center for a high-fidenity system. It is not quite as massively and impressively built as the National ham and communications receiver. This impression is partly the result of the printed or etched circuit construction which for all its virtues is not as handsome and rugged-looking as conventional construction. However, it probably does provide higher insurance that the high specifications will be met and maintained by individual tuners and probably also of higher stability, an important consideration with a receiver as sensitive as this. The good-looking new dial provides a logging accuracy about as good as possible with a broad-tuning receiver.

## Heathkit audio analyzer

The new Heathkit audio analyzer (model AA-1, see photo) combines in one instrument the functions previously performed by three: the intermodulation analyzer, a.c. v.t.v.m. and the audio wattmeter. The new combination (Fig. 3) offers better and more flexible performance than the old individual instruments and sells at a price ($59.95 in kit form) which puts it well within reach of every service technician and many amateur experimenters.

The IM analyzer portion is superior to the old Heathkit IM analyzer in every respect but one: when making rapid runs, the new model is a little less convenient in switching and more care is needed to avoid snapping the needle against the pin. However, the new model has a very much wider useful range and is far more sensitive and more accurate at low IM levels. The low-level sensitivity and accuracy of an IM meter are limited by the residual reading on the lowest scale. This represents partly the internal IM of the instrument itself but largely the hum picked up by the final lowpass filter.

In the old model this residual reading ran as high as 0.3%; in the one I tested it was only .07%, an improvement of more than 400%. This appears to be the result of much more careful and complete internal shielding. The specs list the lowest scale as 1%. In actual fact there are two lower scales: 0.3% and 0.1% full scale. If the residual distortion or reading is subtracted, it is therefore possible to make readings as low as .01%! Such readings are presumably not as accurate as those on the higher scales (and Heathkit is to be congratulated for not claiming them as part of the useful range) but the development engineer and experimenter will find them of great value since they indicate the slightest relative improvement from changes in adjustment or circuit parameters, especially when working with low-level audio stages where even 0.1% IM is high.

The new model offers a single set of internal frequencies—60 and 6,000 cycles—whereas the old one offered a choice of either 3,000 or 7,000 cycles at the high end. However, the new model has two sets of binding posts on the panel with jumpers through which it is possible to inject any external frequency within range of the filters: 10 to 500 cycles for the low end, 2 to 12 kc for the high end. Thus, with an external generator, almost any conceivable combination can be obtained. The same set of posts permits one to bring out either the 60- or 6,000-cycle signal for external signal tracing, while the output posts provide a combination of both, ideal for normal signal tracing because it gives some indication of overall frequency response.

The method of calibration is very simple and with minimum care can produce accuracy of 10%; while greater

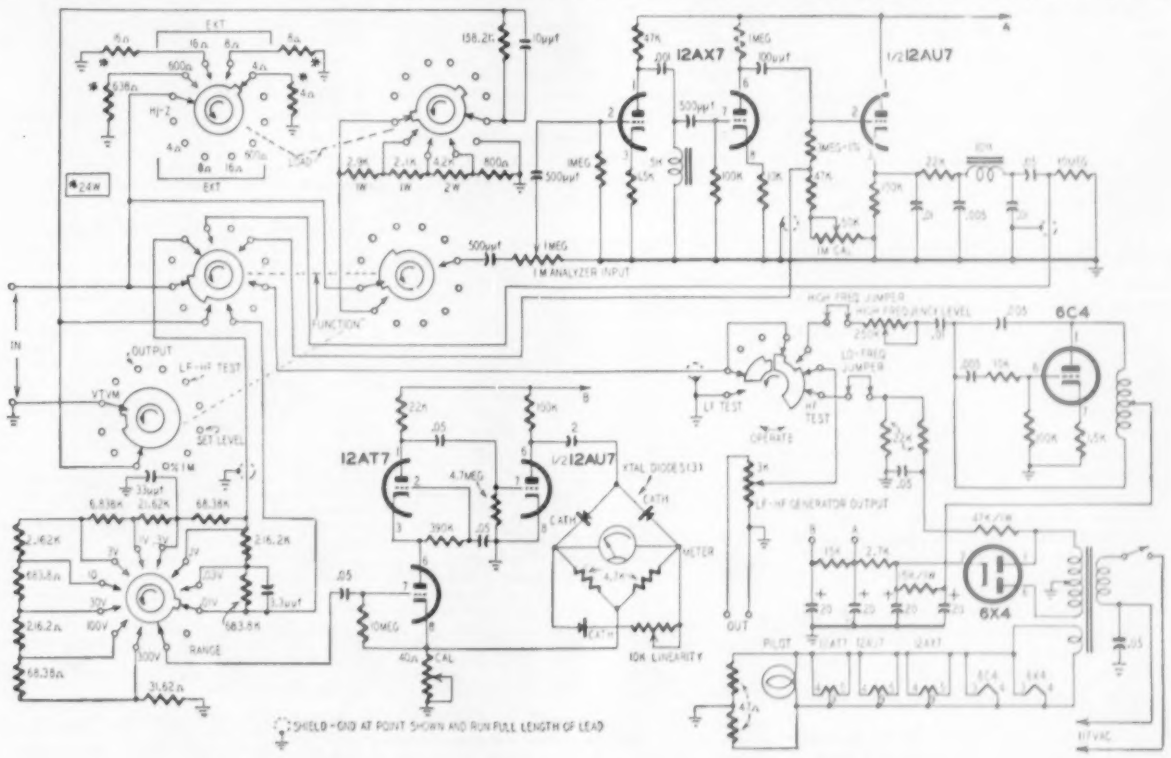


Fig. 3—The Heathkit model AA-1 audio analyzer—unit serves three functions.

care can bring the accuracy down to the tolerance of the meter or about 2 or 3% on the ranges above 1%. The kit includes the resistors needed for calibration.

The a.c. v.t.v.m. has similar superiorities over the older, independent model. For one thing it has a cascode amplifier which reduces residual noise to so low a level that even on the most sensitive scale (10 mv full scale and 200 μv per division) there is no perceptible reading with the input shorted. For another, the meter is much more linear. A new linearity adjustment has been added by shunting the meter with a crystal diode and a 50,000-ohm potentiometer. In the model I tested the adjustment produced linearity within 2 or 3%, not only on each individual scale but also on the two adjacent scales or ranges. The frequency response claimed, 10 cycles to 100 kc within ±1 db, if the wiring is duplicated exactly.

The wattmeter section also profits from the improved linearity and the useful range has been extended on the low end to provide on the lowest range a full-scale reading of 0.15 mw or 150 μw and a low reading of less than 1 μw. Technicians will find this most useful for balancing amplifiers without removing the amplifier from the cabinet or opening the chassis. Connect the wattmeter to the amplifier with a suitable load. Remove the driver or inverter tube to disable the feedback loop. The meter will show some reading on one of the low scales. This represents hum in the plate circuit of the output tubes which are fed relatively unfiltered voltage and depend on exact balance in push-pull to cancel hum. Therefore, adjusting the balance control for lowest hum reading will indicate exact balance. The IM analyzer section can also be used for obtaining *overall* dynamic or a.c. balance. Take a reading at between 1 and 5 watts (for home amplifiers) or just under maximum output for amplifiers operating at high levels. Now adjust the balance control for minimum IM. If the amplifier has a bias control, bias can also be adjusted for minimum IM at just under maximum output.

Very compact and light, the instrument is an ideal tool to take for servicing hi-fi systems at the installation. It can be used for signal tracing, troubleshooting, adjustment and even for tube testing. (Substitute front-end tubes while taking IM readings; if IM is reduced, the new tubes are better. For output tubes, take output reading at near maximum output; if output increases with new tubes, the new tubes are better.)

## New records review

**HOVHANESS: *Khadis Concerto for Piano, 4 Trumpets and Percussion***
***Six Piano Pieces***
**William Masselos, pianist**
**Izler Solomon conducting Chamber Ensemble**
**MGM E-3160**

The most novel and provocative recording I have received in many months and one which, though esoteric, will be a lot of fun at any hi-fi or record party and will interest anyone who likes the different in sound and tonal effects. Hovhaness, an American of Armenian descent who writes in a combination of Near Eastern and early polyphonic classical style, produces music unique in musical and tonal qualities.

The solo piano pieces on side 2, for example, involve, beside the ordinary fingering of piano keys, the production of tones by beating either the keys or the strings themselves with xylophone and tympani hammers, plucking the strings with a guitar pick and in one portion embodying the sound of piano keys hitting bottom into the melodic and tonal pattern as if it were produced by some independent percussion instrument. The piano is made to produce sounds resembling those of drums, organ, guitar, bells, etc.

The concerto on side 1 has some of the wildest or most inspired polyphony I have ever heard. I don't recall when I heard so many piano beat notes on any single record. All in all, this music could not be reproduced accurately without high fidelity. With the warning that the music is very different, though charming when one gets used to it.

**SIBELIUS: *Third Symphony***
**Stokowski and NBC Orchestra**
**RCA-Victor LM-1854**

If you (or more likely your family) would like to have a little good music with the demonstrations of big bass, this should go right at the top of your shopping list. Sibelius scored a lot of thunder and lightning (almost literally) into this work and Stokowski, the NBC Symphony and RCA engineers bring it forth just about as big as life and twice as awesome. Though we've had plenty of fine drums lately, the double basses have been rather overlooked.

Here we have a very big double-bass section speaking in full voice and in almost all the language of which it is capable. With some bass boost the effect can be overpowering. Furthermore, I don't think there is anything under 40 cycles in the grooves. Thus, it will produce nearly the full effect with any reasonably good speaker system, although it is very likely to show up any rattles that may have been built into the enclosure. In addition there are some mighty blasts of brasses in the characteristically fiery Sibelius choirs, including one in, I think, the third movement which will almost certainly make you jump. But don't buy this for demonstration purposes if you can't play it loudly; 90% of the effect is lost at low volume levels, though the musical effect remains good.

**BLOCK: *Four Episodes for Piano, Strings and Winds***
**Knickerbocker Chamber Players**
**BRITTEN: *Sinfonietta for Winds and Strings***
**MGM Chamber Ensemble**
**MGM E-290 (10-inch LP)**

Excellent test of system definition, especially for those who like chamber music. The Block piece has a very complex polyphony, some of it tonal polyphony. There is a fine bassoon, a nice gutty bass, and a big piano with vibrate and beat notes. In the first movement a very dull bass is ridden delicately by light strings in the top register, providing an excellent test for IM. The Britten has a very sweet but very naturally windy flute. The strings have a tone which I can only describe as "rosiny." The close-up double bass is of the very best on records and in one spot is sustained like an organ note and will provide a severe measure of wow. For modern music it is not at all hard to take

**RENÉ: *Passion in Paint***
**Andre René and his Orchestra**
**RCA-Victor LPM-1033**

This is modeled on the idea of Mussorgsky's *Pictures at an Exhibition*. Andre René gave his impression in symphonic-popular style of 12 famous paintings, no fewer than 6 of them nudes. Nobody, least of all René, would want to compare the music with Mussorgsky's, but the recording does approach the RCA-Victor recording of the *Pictures* in hi-fi quality and usefulness for demonstration. There is some very spectacular music here with odd and even unique sounds, including that of a choir of brasses giving forth a loud and clear Bronx cheer, some good drums, a plentitude of crashing cymbals, assorted percussives and a lot of high-high shimmer of various kinds. There are also some odd miking effects, as for instance, a harp which seems to leap out of the orchestra into your lap when it gets its brief moment of solo glory. Though this is a Black Label record, RCA engineers have clearly given it the Red Label works, and withal, it makes a first class sound on a hi-fi system.

***THE KING OF INSTRUMENTS***
**Vol. 1: *American Classic Organ***
**Vol. 2: *Organ Literature***
**Vol. 3: *Organ Recital***
**Aeolian-Skinner Organ Co.**
**Boston 25, Mass.**

Those who love the organ cannot conceivably justify not having one or more of these in their library. Between them they pretty well demonstrate the whole gamut of organ capabilities and with practically 100% verisimilitude. Those who own or sell the very few speaker systems capable of going down to 20 cycles or lower will also want these to demonstrate. (Volume 1 has two identified examples of the 16-cycle, 32-foot pipe very faithfully recorded, and also a sweep of the whole organ range which will do a better job of revealing resonances, doubling, rattling, etc., than anything else I know of.) But don't bother demonstrating this on anything less than the almost perfect speaker system; the doubling will be all too evident.

Volume 1 is a lecture with short snatches of musical illustration, on the various resources of the organ and how the individual tones are produced. Of great interest to the organ specialist, it is also an excellent introduction to the theory of musical formation. The recording provides an excellent measure of overall system quality, especially flatness—the cleaner and flatter the system, the greater the audible difference between the various stops.

Volumes 2 and 3, however, are all music and fine music. Both present a wide variety of demonstration and showoff material, with Volume 3 having a slight edge perhaps in Vierné's *Carillon Westminster* and amazing concatenation of sound which taxes the definition and dynamic range of the best of playback systems. Volume 2 has the better examples of Bach's polyphonic genius, which, too, requires superb definition. With the best systems, the reproduction of the organ is positively lifelike.

***GUITAR MUSIC OF SPAIN***
**Laurindo Almeida, unaccompanied guitar**
**Capitol P-8295**

The guitar music of Spain requires a virtuosity on the instrument probably unequaled except in the case of the violin playing the works of Paganini. The guitar is elevated in its tonal capacities to a level almost worthy of comparison with the classic organ. Mr. Almeida is not yet a Segovia and his renderings of an excellent sampling of guitar repertoire shows some signs of effort (Segovia is incredibly effortless) but that produces a particularly charming and worth-while hi-fi recording.

The guitar produces a very great variety of intentional or accidental transients. There is, for example, the very highly damped, very dull bass in some effects and the equally damped very high notes which though periodic are of such short duration that they resemble pulses with an echo. Much of Spanish guitar music calls for slapping or drumming on the guitar body and the sound produced this way is almost a pure transient. Furthermore, this music requires such superbly dextrous motions of the fingers that inevitably there is some trace of their passage in the form of squeaks in the range above 7 or 8 kc, the click of fingernails, etc. Finally in some of the bass passages several strings are plucked simultaneously and beat notes are often established. This recording presents samples of all these and this, together with a great faithfulness to the tone of the instrument and extremely fine definition, offers an absolutely first-class example of realism, presence and naturalness of which a fine hi-fi system is capable. END

***Note: Records above are 12-inch LP and play back with RIAA curve unless otherwise indicated.***

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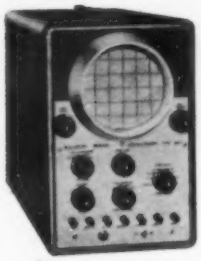

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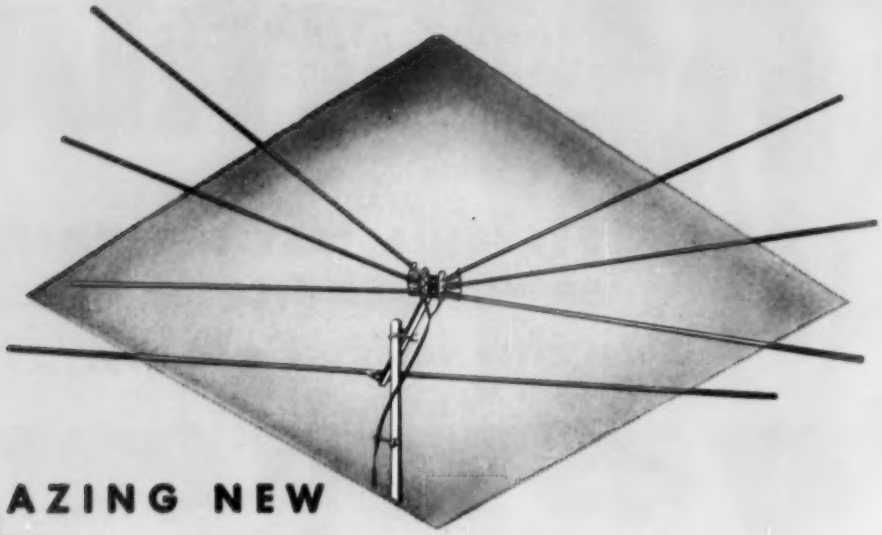

## AMAZING NEW

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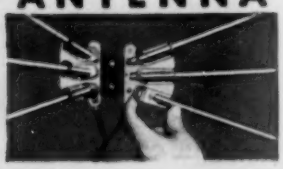

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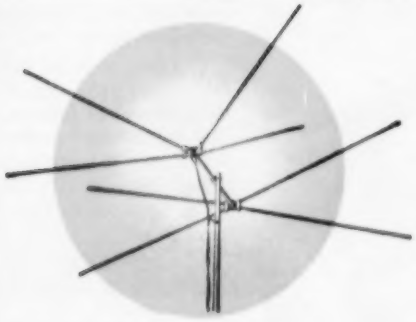

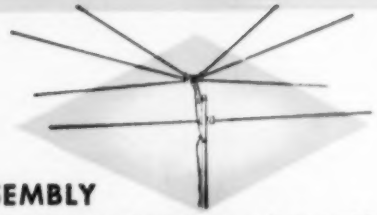

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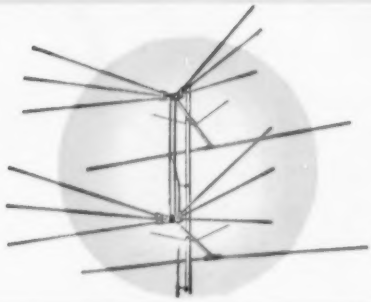

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*High-fidelity unit features low-distortion preamp and choice of speaker damping*

# *Designing an Ultra-Linear Amplifier*

By EDWARD S. MILLER*

SOME recent trends in high-fidelity amplifier design have been in the direction of smaller, more compact assemblies that can be made into attractive, self-cabineted units. This type of design can be developed without sacrificing performance in any way; in fact—with new tube designs and advanced circuitry—improved performance has often resulted.

Our own Sherwood S-1000 (see photo) is an excellent example. Its features had to include 20-watt output and single cabinet design. These were just the two of the most important factors governing its design. Others were that it must have low heat dissipation and be small. Within the limits of these specifications it was possible to include a choice of speaker damping (including negative damping); low-distortion tone controls; rumble and scratch filters; a low-noise, low-distortion phono preamplifier and a pushbutton-operated record equalizer circuit.

The new 6L6-GB tubes (Fig. 1) were used, not only because they are smaller than their predecessors the 6L6-G and 6L6-GA, but because of other constructional advantages such as the more reliable button type base. To economize on B plus requirements, only tetrode and tapped screen (Ultra-Linear) operation of the output tubes was considered. Restricting the B plus requirements to conform with the 125-ma maximum limitations of the 5Y3-GT not only made it possible to use the smaller rectifier, but also saved the 5 watts of additional filament drain that would have been required for the larger 5U4-G frequently used in such applications as this.

Output tube operation was based on an analysis of the typical plate characteristics of the 6L6 tube family. Fig. 2 shows these characteristics for triode and tetrode operation. These are static curves, taken with a laboratory power supply which varies the plate and screen voltages independently. Also shown are four intermediate degrees of tapped-screen (Ultra-Linear) operation.[1, 2, 3]

In determining tapped-screen plate characteristics, the screen voltage used in each case is a percentage of the difference between the plate voltage and the B supply or:

$$E_{c2} = E_b - \% (E_b - E_p)$$

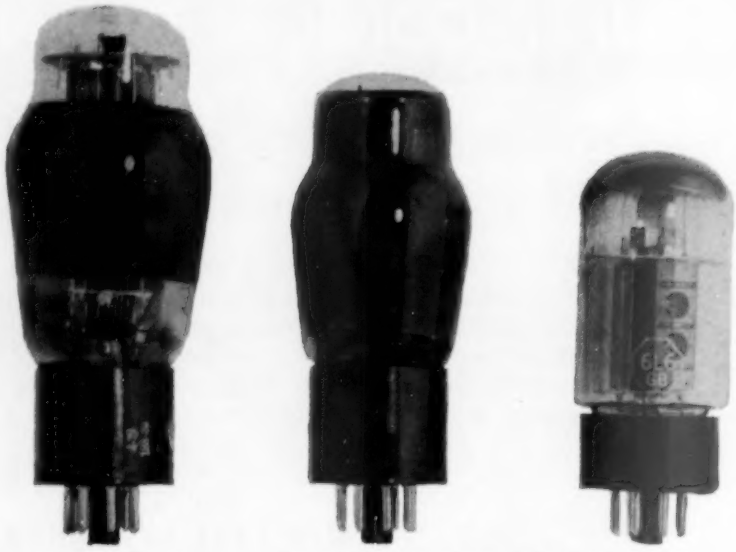


Fig. 1—Some members of the 6L6 family.

where % is the percentage of turns that the screen grid is tapped up from the transformer-primary center tap.

Substituting % = 100 (triode operation), this formula becomes:

$$E_{c2} = E_b - E_b + E_p = E_p$$

And if % = 0 (tetrode operation), the formula becomes:

$$E_{c2} = E_b$$

Values of $E_{c2}$ are shown below the curves (Fig. 2) for each plate voltage value. B supply voltage of 320 was used in the final Sherwood design. However, to simplify calculations, a voltage of 300 was used in these tests.

In calculating a push-pull class-A amplifier's maximum power output and optimum load line, it is necessary to know the exact zero grid characteristic. Therefore, to eliminate confusion, only the general direction of the other grid voltage curves are shown. Note that the curves for different degrees of screen tapping pass through common points on the constant $E_b$ coordinate.

Several interesting features of Ultra-Linear operation can be observed from the curves in Fig. 2. First, maximum push-pull class-A power output was calculated using each of the zero grid

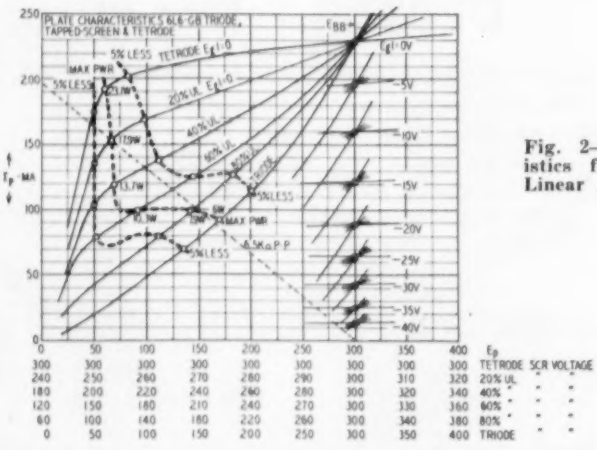
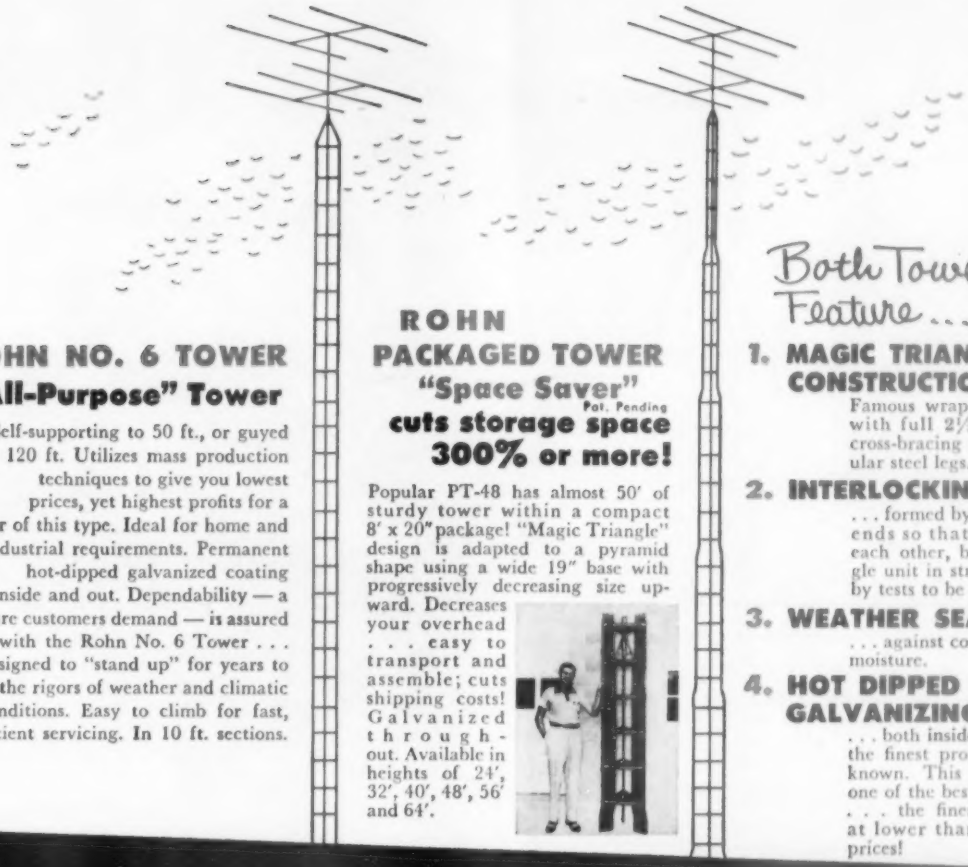



Fig. 2—Plate characteristics for triode, Ultra-Linear and tetrode operation.

* General manager and chief engineer, Sherwood Electronics Laboratories.



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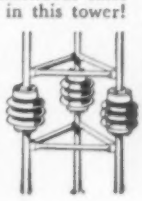

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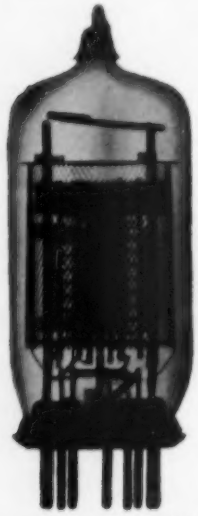
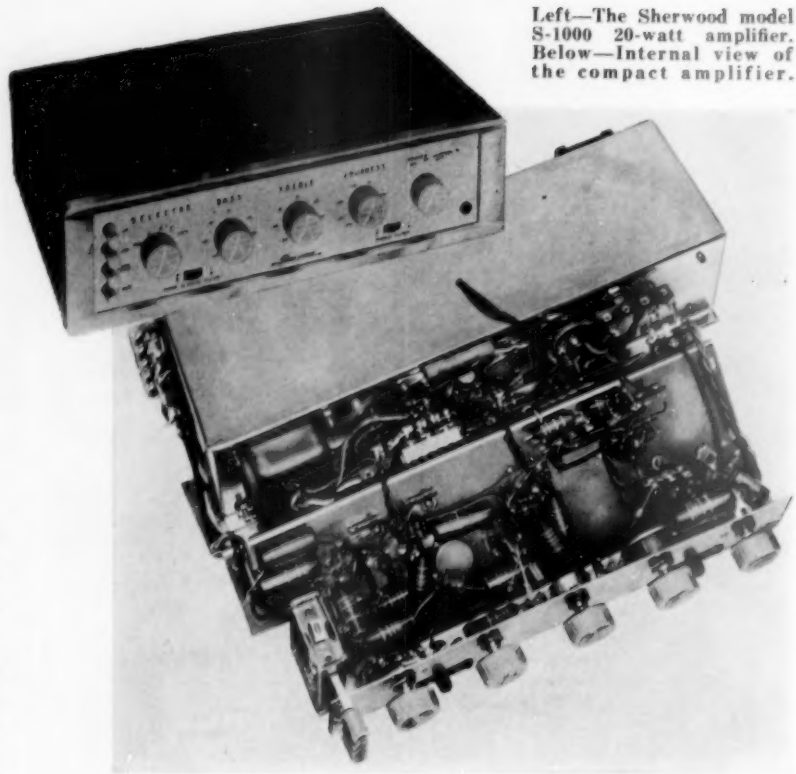


*Courtesy British Industries Corp.*

**X-ray view of the Z729. Shield screen around plate minimizes hum and noise.**

**Left—The Sherwood model S-1000 20-watt amplifier. Below—Internal view of the compact amplifier.**



characteristics shown. This power is approximately:

$$P_o = \tfrac{1}{2}(E_b - E_{min})I_{max}$$

where $E_{min}$ and $I_{max}$ describe a point either at the knee of a tetrode type curve or at the intersection of a line from $E_c$ which has the negative slope of a triode type curve. These points have all been indicated in Fig. 2 and have been connected by a dotted line.

Two similar lines have been drawn

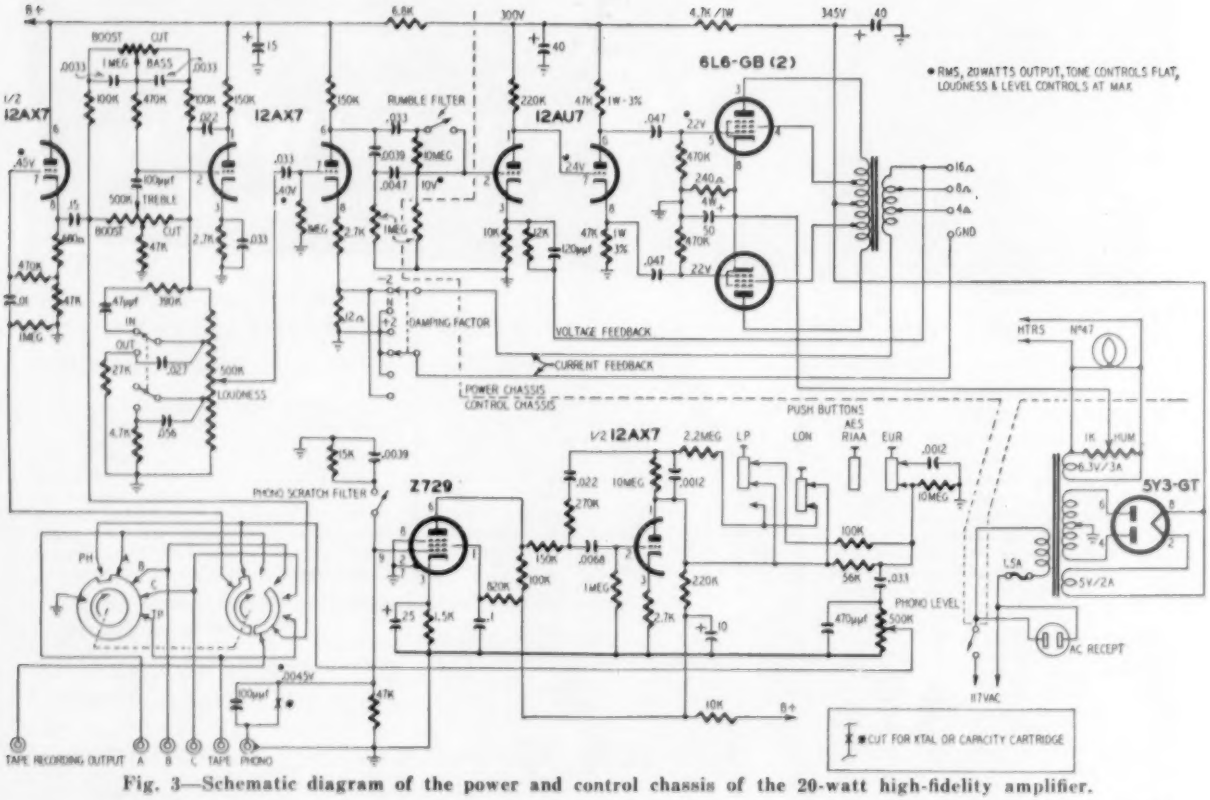



**Fig. 3—Schematic diagram of the power and control chassis of the 20-watt high-fidelity amplifier.**

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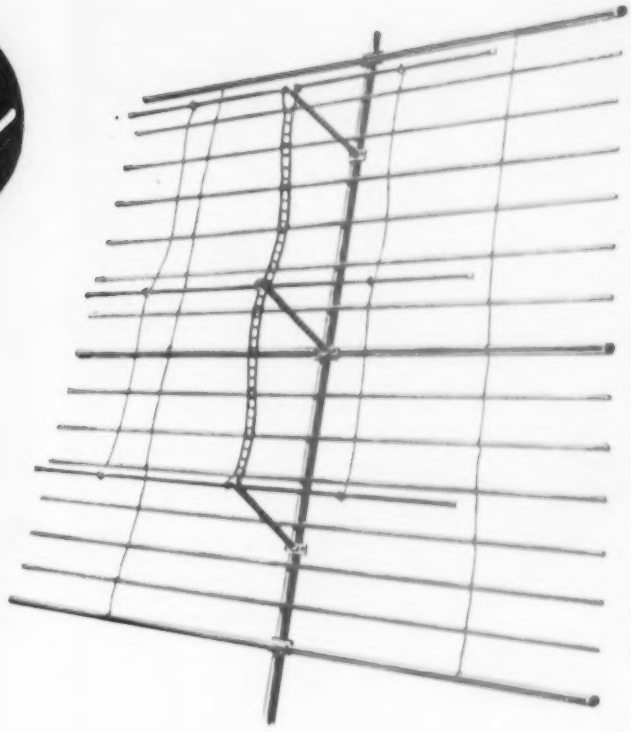

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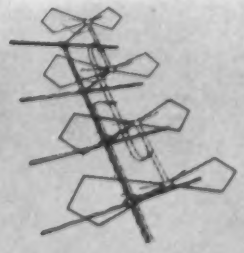

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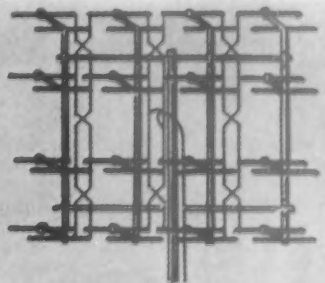

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through those points which are at 95% of the calculated maximum power output. Note how much farther apart these lines are as they intersect Ultra-Linear or triode $E_c = 0$ curves. The plate-to-plate load impedance line also passes through the maximum power points from the $E_p = E_b$, $I_p = 0$ point. The load line for 20% Ultra-Linear maximum power (6,500 ohms plate to plate) has been drawn on the diagram. Note how much greater variation (swing of the load line on the diagram around the point $E_p = E_b$, $I_b = 0$) the load values may have without losing power or causing distortion in the Ultra-Linear and triode cases.

There are other important factors which can be observed by more detailed study of these curves.

1. Ultra-Linear operation always results in a considerably lower plate resistance than that obtained with tetrode operation. Consequently, the speaker damping factor is correspondingly lower with Ultra-Linear operation. (This point is not as important as it was at one time. It has been found that low damping factors can be had by proper use of current feedback from the speaker coil. More on this later.)

2. The distortion at maximum power output for 20% Ultra-Linear operation is approximately one-third that of a tetrode connection.

3. The increase of anode current under sustained maximum-power-output conditions is higher with tetrode connection than with Ultra-Linear or triode. Of greater importance, although not indicated in Fig. 2, is the slower rise in screen current at maximum output with Ultra-Linear connection. With the Ultra-Linear circuit, the screen will operate at a more conservative dissipation than a similar tetrode operation. The useful power output from the screen in the Ultra-Linear case further lowers its actual dissipation and further increases the advantage of Ultra-Linear operation over tetrode. Moreover, the B supply and bias methods have less rigid regulation requirements with the reduced current variations.

These considerations seem to substantiate, in general, previous claims of superiority for tapped-screen operation. Consequently, this circuit (Fig. 3) has been used (with 22% taps) in the Sherwood model S-1000 amplifier.

The schematic shows a method of applying current feedback, either positive or negative, from the output transformer secondary. In the S-1000 this results in a damping factor choice of either −2, +2 or the +7 normally obtained without current feedback.

A 12-db-per-octave rumble filter, a continuously variable compensated loudness control and a modified Baxandall tone control system' also appear in the circuit. The feedback type control system, with its inherent low-distortion characteristics, is at its best when driven by a cathode follower. This same cathode follower (which precedes both the tone and loudness controls) then becomes an excellent low-impedance source to meet tape recording requirements. The recording jack, however, is interrupted by an open switch contact when the selector switch is in the tape position. This prevents a feedback circuit through the recorder.

The input capability of the high-impedance input circuit is 10 volts for less than 1% IM distortion. This data is not usually included in amplifier specifications. Poor input capability can lead to distortion which is frequently difficult to analyze (as in the case of an AM tuner producing a 5-volt signal while receiving a local broadcast).

Input capability is also important in considering phono preamplifier specifications since many high-level magnetic cartridges are still used. The model S-1000 can handle 150 mv with less than 1% IM distortion.

Equally important is adequate preamplifier sensitivity, which should be 5 mv or less to meet the requirements of the G-E Professional and the Fairchild cartridges. A Z729-pentode–12AX7-triode feedback pair, with a mid-frequency gain of 20 db, are used in the Sherwood.

Associated with high sensitivity in preamplifier systems are the requirements for minimum hum, noise and microphonics. The British Z729 (see photo), together with the use of proper circuitry and layout, met these requirements without resorting to the added complication of d.c. heater supplies.

The most commonly used preamplifier circuits are based on feedback pairs. Two common types are those with the first tube self-biased with a large grid resistor and a grounded cathode (Fig. 4) and those with feedback to an unbypassed cathode resistor (Fig. 5). In either case, because *both* the grid and the cathode are not at low impedance to 60 cycles, it is difficult to eliminate hum using a.c. heater supplies.

A more foolproof circuit (Fig. 6) is one with the grid at low impedance (determined by the cartridge), with a self-biased, *bypassed* cathode resistor. Electrostatic hum pickup by the grid and cathode is thus eliminated. Also, the high-impedance feedback resistor does not tend to load the second plate as is the case with the lower-valued feedback resistor required for cathode feedback.

A 1,000-ohm potentiometer across the

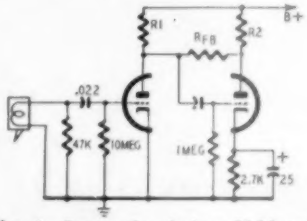


**Fig. 4—Input circuit is self-biased.**

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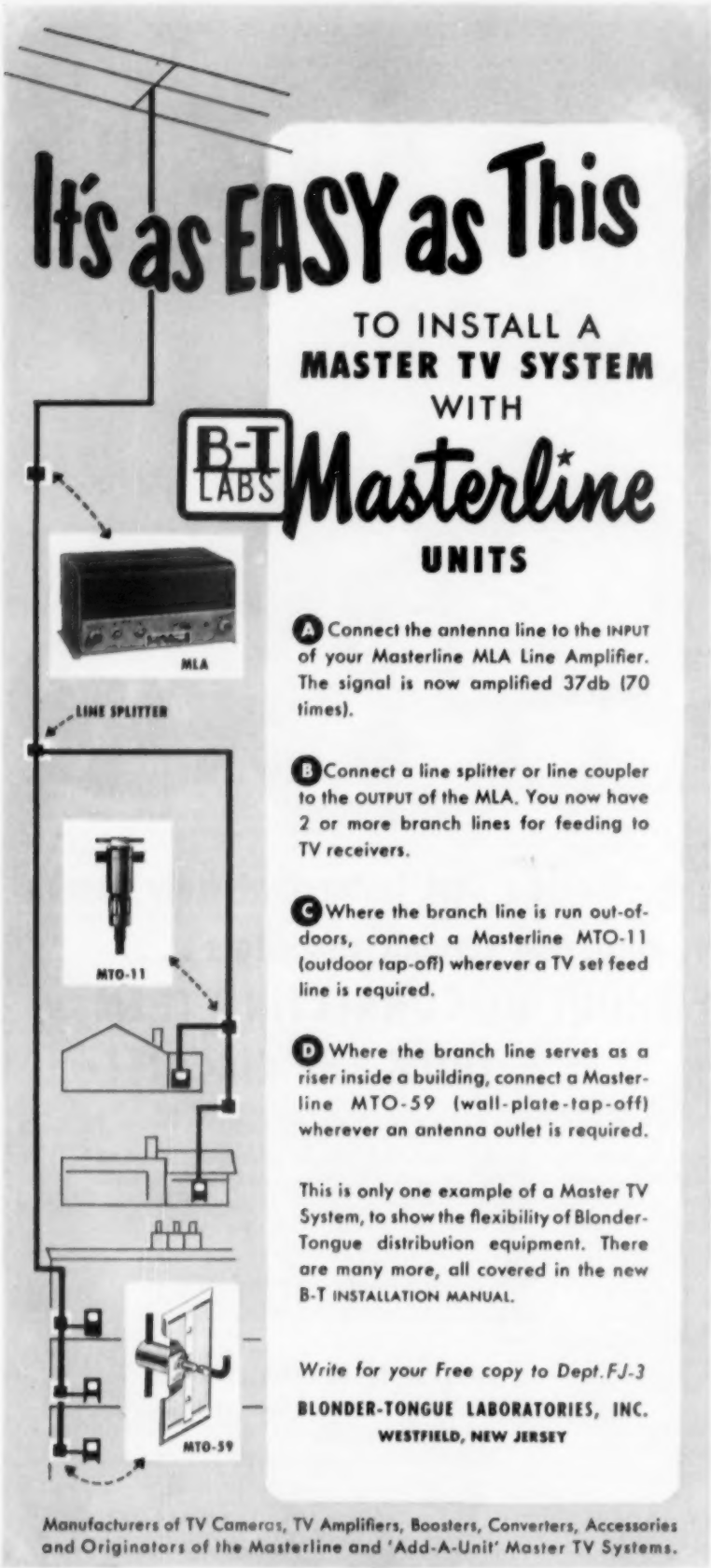
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heaters and returned to the positive voltage at the output tube cathode completes the circuit essentials. Careful twisting of the heater wires, which are dressed away from grids and plates, and the excellently shielded internal construction of the Z729 tube, make possible an equivalent of 1.5 $\mu$v of hum and noise at the input grid. (This is 60 db below maximum output.)

With this circuit it was a simple matter to add a four-button push type switch for record equalization.

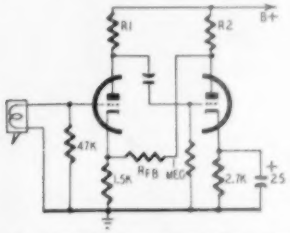


**Fig. 5—Feedback preamplifier circuit uses unbypassed cathode resistor.**

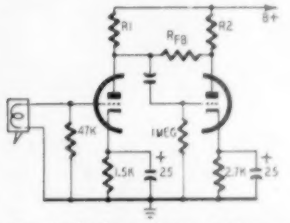


**Fig. 6—Cathode resistor is bypassed.**

The four-position equalization selector is a four-section locking-type circuit-transfer push-button switch. Each button locks in when depressed and remains latched until released by depressing another button. The equalization complements the RIAA and new AES recording curves when the EUR, LON and LP buttons are out (not depressed) so a dummy AES-RIAA button is added to simplify operation for the uninitiated.

The LON button is shown depressed on the diagram. It shunts a 2.2-megohm resistor across the 10-megohm resistor and .0012-$\mu$f capacitor in the feedback network and alters the response on the low end. The LP switch does the same thing and disconnects the 100,000-ohm shunt resistor so the response at 10 kc is −16 db. The EUR position disconnects the grounded .0012-$\mu$f capacitor from the circuit and provides more highs. The 10-megohm resistor eliminates the d.c. click as the circuit is opened and closed.

A 15,000-ohm resistor and .0039-$\mu$f capacitor can be switched across the pick-up cartridge to form a scratch filter with attenuation of 12 db per octave. END

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[2] D. Hafler and H. Keroes, "Ultra-Linear Operation of the Williamson Amplifier," *Audio Engineering*, June, 1952.
[3] A. D. Blumlein, British Patent No. 496883, May, 1937.
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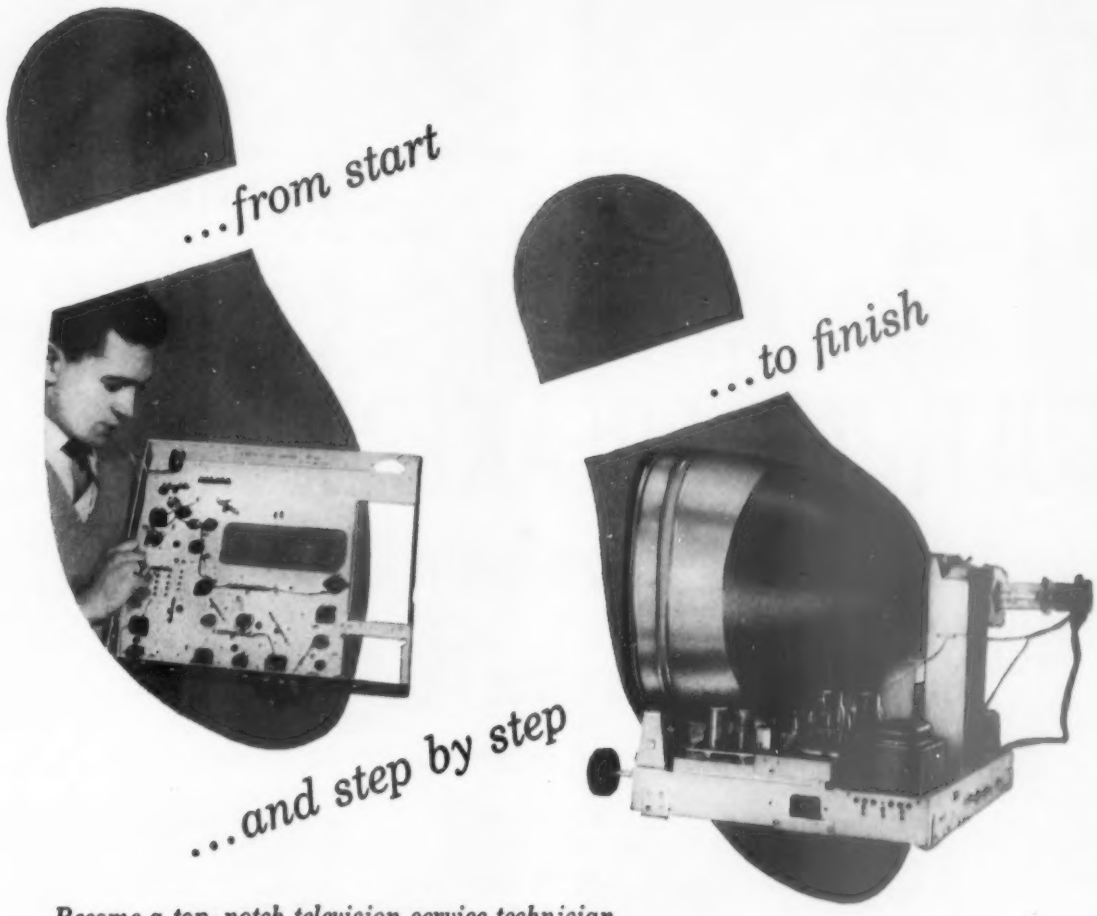


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# MULTIPLE SPEAKERS FOR HIGH-FIDELITY

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*Mutual coupling improves audio response*

MULTIPLE SPEAKERS

By JOSEPH MARSHALL

THE biggest difficulty in achieving the fullest possible fidelity in sound reproduction for most audiophiles is presented by the loudspeaker system. The problem is to obtain clean and adequate reproduction of the lowest two octaves, 16 to 64 cycles, and to maintain a smooth and undistorted response for the rest of the range.

Recently—in trying to obtain acceptable results with inexpensive and small systems—many old acoustic and radiation principles have been revived. One of the oldest, soundest and simplest, however, has received little attention. The principle is that of mutual coupling of multiple radiators. It is very simple and proceeds from the general theory of radiation. When two or more identical radiators are mounted close together, the efficiency of the combination at bass frequencies increases as the *square* of the increase in piston area. Thus, two identical speakers closely coupled are 4 times more efficient than either one would be alone in the same position; four speakers are 16 times more efficient, etc. *This is greater than the improvement provided by a horn in which the radiation efficiency increases as the square of the diameter of the mouth.* (In practice these theoretical efficiencies are only approximated but the relations are maintained closely enough to serve as guides.)

To appreciate the full significance of this, let us look at some other aspects of it. Although two 6-inch speakers have only one-half the piston area of a 12-inch speaker, they are as efficient when mutually coupled as a single 12-inch speaker of similar characteristics. Two 8-inch speakers have just a little more than half the piston area of a 15-inch speaker but provide greater efficiency. Attempts have been made to build cones 2 or even 4 feet in diameter in an effort to obtain large piston areas; but such large speakers have so much mass and require such large motors that as a rule they are impractical. However, two 15-inch speakers, having only half the area of a 30-inch speaker, will yield the same efficiency, and four of them would be equivalent to a single cone 5 feet in diameter. Also, the distortion characteristics are improved theoretically by the square of the improvement in efficiency.

Furthermore, every increase in horn mouth area requires a corresponding or greater increase in the depth or length of the horn. But in close-coupled multiple speakers, the increase in piston area is obtained with no increase in depth. Increased efficiency in a horn requires an increase in size in all three dimensions; the efficiency increase in multiple speakers is achieved with an increase in size in only two dimensions. So, if you held up your hands in horror at the thought of the space occupied by four 15-inch speakers, consider the space needed for a horn with a mouth 5 feet in diameter!

Finally, assuming that for various good reasons we use a wall type infinite baffle with our multiple speakers, there is another advantage over a horn. A horn has a very odd frequency curve. It is very flat above cutoff (the point where the mouth area is one-half-wavelength squared), but below cutoff it has a very steep slope, usually 18 db per octave. In an infinite baffle the slope below resonance is at the theoretical rate of 6 db per octave. So that, given a horn with a cutoff at 40 cycles and a multiple-speaker system with resonance at 40 cycles, the multiple-speaker system is superior in the octave below 40 cycles.

### Improving frequency response

So far we have considered the effect at low frequencies of mutual coupling of two or more *identical* speakers. There are excellent reasons, however, for departing from similarity or identity. The response curves of speakers, even in anechoic chambers, are noted for their raggedness. One cause of this is speaker resonance which produces harmonically related peaks that are indicated with exaggeration in Fig. 1. Furthermore, more valleys and humps are produced by cancellations and additions due to reflections of the wave at the termination of the cone; others are caused by cone breakup at higher frequencies.

Multiple speakers provide a means of correcting, compensating or, at least, ameliorating some of these effects. For example, speakers with different resonances will have peaks spaced differently; the peaks of one may fall into the valleys of another. I indicate this in Fig. 1a.

Designing speakers of suitable dissimilarity to provide a perfectly smooth curve may or may not be possible.

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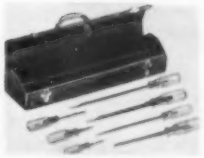

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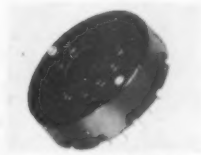

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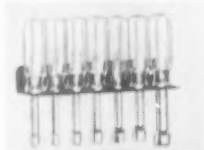

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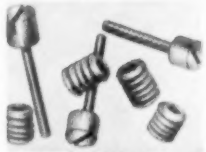

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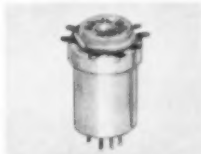

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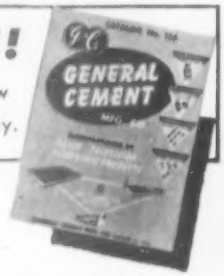


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Multiple speakers provide a simple means of obtaining a smooth extension of the range downward. Several speakers might be chosen having resonances differing by 10 cycles—a 30-, 40- and 50-cycle speaker for example. The resonances will combine to produce a fairly smooth curve down to the lowest frequency as indicated in *b* of Fig. 1 (assuming the amplifier provides enough damping to level the peak).

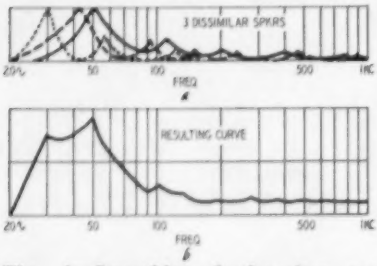


**Fig. 1—Smoothing loudspeaker response by using dissimilar speakers**

The property of mutual coupling has been extensively applied in the use of "images" of the radiator to increase bass efficiency. When a speaker is positioned close to a flat surface such as a wall or floor so that some of the sound waves are reflected from the surface toward the ear, the effect is precisely the same as if there were another speaker where the floor is. Thus, one speaker close to the floor acquires the same efficiency it would obtain if it were coupled to another speaker. If located in a corner, where images are provided by floor and walls, it has the same efficiency as if coupled to three other speakers. (This does not mean that a single speaker in a corner is as good as four closely coupled speakers —simply that it is as good as *one* of the four speakers in a cluster of four, which in effect makes it four times as good as a single speaker in the middle of a wall.) A good portion of the efficiency of reflex enclosures is due to mutual coupling of port to piston and of both to the floor or walls. Similarly, a good part of the efficiency of corner horns is due to coupling of horn mouths to the walls.

The curve resulting from mutual coupling of multiple speakers or speakers and images varies with the pattern in which they are arranged. Thus, four speakers mounted in a square pattern have only slightly more efficiency (Fig. 2) at 40 cycles than four speakers mounted in a vertical line, one above the other. But the four speakers mounted in a vertical line will have a crossover some 200 cycles lower. That is, the point at which the boost begins is lower and more of the boost is concentrated below 100 cycles. This arrangement affects the mid-frequencies less and the low bass can be increased greatly with less effect on voices. The radiation pattern is also affected by the shape of the cluster. The square radiates more or less uniformly in all directions; the vertical slot has a much wider horizontal directivity because a slot spreads radiation in the direction at right angles to its longest dimension. Therefore, vertical stacking makes the point source at low frequencies very much wider.

There is one danger with multiple coupling. When two or more radiators are separated by some multiple of the radius of the cones, cancellation and addition effects are produced due to phase differences. These effects can be used to obtain special slopes, but the relationships are so complex that the experimenter should avoid any spacing between speakers (or speakers and images) which is any multiple of the radius of the cone. Using speakers of different sizes also helps because the radii of the cones will differ.

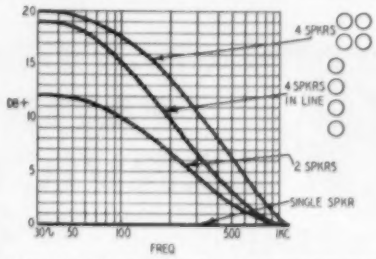


**Fig. 2—Theoretical improvement through mutual coupling of speakers.**

## Application of mutual coupling

The principle can be applied to any of the familiar speaker baffling arrangements from the infinite baffle to the horn. For example, Permoflux in one of the few commercial applications (Diminuette) uses two 6-inch speakers in a very small bass-reflex enclosure. In the Largo they use a pair of 8-inch speakers mutually coupled as direct radiators in front and mutually coupled to load a horn in the rear. The Baruch-Lang system is another similar one. In such cases, the size of the enclosure, the flare of the horn, the size of the reflex port, etc., are determined by the *actual* combined piston area of the speakers used. In general this means that multiple speakers will provide the same efficiency in a much smaller enclosure.

I am not able to give guidance in the application of the principle to such enclosures. My work has been entirely with the infinite baffle provided by mounting the speakers in a wall. Such wall mounting has several advantages. It is a simple way to get good baffling at low frequencies. It is usually the least expensive means of extending bass response, especially when combined with multiple speakers. If the speakers are mounted in a wall between two rooms or two portions of a house, the method provides good distribution of sound into both areas. Finally, the slope below speaker resonance is more favorable than in a horn.

The basic principle of wall mounting is that of increasing the distance from front to back of the speaker cone and thus eliminating or minimizing the loss at low frequencies which occurs when front and back waves meet out of phase. Cancellation effects set it at a frequency whose wavelength is equal to the distance from the front to back of the cone. (Incidentally, the wavelength of any *sound* frequency is determined by dividing the velocity of sound in air, about 1,100 feet per second, by the frequency. Thus the wavelength of 50 cycles is 1,100/50 or about 22 feet.)

The speaker mounting requires very few precautions and is not critical. It should be rigid, nonresonant and free of vibration. If the walls are of gypsum board ⅜ inch or more thick, one or two small speakers may be mounted directly on it. Gypsum board is fairly nonresonant up to a point. If the wall is of plaster-and-lath construction (or if large speakers are to be used), the best procedure is to cut a square or oblong hole between the 2 x 4 framing somewhat larger than the size needed for the speaker or speakers. Since walls are usually 4 inches deep, and speakers usually exceed this depth, a box will have to be extended into one room or the other. If the opening is furred in with 2 x 6's or 2 x 8's, the box will be rigid.

The speaker board can be ¾-inch plywood of a size to fit the opening. It would be an excellent idea to use strips of foam rubber between baffle board and frame to damp the mounting board and prevent dissipation of low-frequency energy in wall vibration. When several speakers are to be used, an entire section between adjacent 2 x 4's in the wall should be cut out and replaced with ¾-inch plywood in which the speaker holes are cut. If the insert is full length, it should be braced with furring at least very 2 feet.

If it is not possible to use the wall between two rooms, the back radiation can be confined to a closet. Closets usually have enough volume so that the air column formed in them will not have a significant effect on the speakers. The door of the closet can be used as a mounting board and then sealed against air leakage with rubber of the type used to seal automobile doors—this can be purchased in long lengths. A good weatherstrip could also be used. If the closet contains a lot of clothing, its interior will not require any treatment since the clothes will absorb most of the back wave.

In choosing a location for wall-mounted speakers, keep in mind the increase in radiation efficiency obtained by coupling with images of the speaker. Speakers located close to the floor, ceiling or an adjoining wall will be re-

(*Continued on page* 105)

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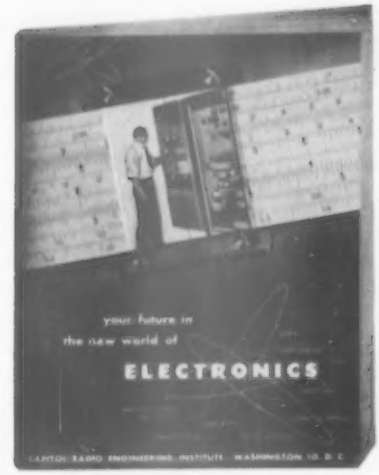


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enforced at low frequencies. When multiple speakers are used, some caution is necessary. The combined efficiency of multiple speakers plus images can produce overpowering effects in most rooms and intolerable effects in some. I would not advise corner mounting if more than two speakers are used. And when more than two speakers are used I recommend stacking them vertically rather than lining them up horizontally close to the floor.

The most effective location is along the narrow side of rectangular rooms, for in this position the nodes of the room are most completely energized and directional effects minimized. However, when multiple speakers are used, these effects are not so important because of the higher efficiencies. In my own instance, the only practical location was in the middle of one of the long walls of a long narrow room—theoretically a poor location. Yet the results are exceedingly good.

A good way to probe a room is to use any small enclosure and move it around the room, noting the effect of each location on overall quality. The effects will be much the same in any position with multiple speakers, except that effects on the bass will be compounded several times. Be careful, therefore, not to choose a position which with a single speaker produces a very high bass or a boom or sets up standing waves in the room. When this is compounded by the additional efficiency of multiple speakers, it may be completely intolerable. But location in a room is not very important when multiple speakers are used, and it is fairly safe to choose the location most convenient for cutting into the walls.

One virtue of wall mounting is that it can be progressive. You can start with one speaker and improve the installation by adding others as the budget permits. It is wise when making the original installation, no matter how small, to provide for expansion by putting in a larger mounting board, re-enforcing the wall, etc.

### Combining speakers

The benefits of mutual coupling apply to any speakers, from the finest to the cheapest. The better the speakers the better the overall result. But a special virtue of this method is that amazingly good results can be obtained with fairly inexpensive ones. For example, I have used this method in my home for nearly 20 years. I started with two good-quality public-address type 12-inch speakers and later added a 5-inch tweeter. The results were spectacular by the standards of those days. I added two other speakers obtained at bargain sales and this combination was used until a few years ago and produced an overall quality superior to that of systems costing many times more.

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We were FORCED to make this "give-away" offer . . . for only by putting our recordings in your hands can we convince you how extraordinary their tonal quality is. Performed by internationally-renowned orchestras, conductors, and soloists. Custom-pressed on the purest vinyl plastic. Reproduced with a fidelity of tone which encompasses *the entire range of human hearing* . . . 50 to 15,000 cycles!

**HOW CLUB OPERATES:** As a trial member, you are not obligated *ever* to buy any recordings from us. You do, however, have the right to try—free of charge—any of the Society's monthly selections which interest you. You receive prior notice of these. You pay nothing in advance. And you are not obligated to keep those you try . . . even after you have played them and read the interesting music notes which accompany each selection. You pay only for those which—*after having tried them*—you decide you really want to own. And for these, you pay only the low member's price of $1.65 per long-playing disc, embodying on the average about 40 minutes of music by the great masters. *A saving of about ⅔ off the usual retail price!*

Think how much beauty and serenity these recordings will add to your life—at a trifling cost. Think what a cultural advantage your children will gain by having great music as an everyday inspiration.

***Mail Coupon Now***

We obviously cannot keep "handing out" such magnificent long-playing recordings indefinitely. Production capacity limits the membership rolls; once filled, the offer has to be withdrawn. So avoid disappointment. Mail coupon with only 25¢ to help cover postage—today! *The Musical Masterpiece Society, Inc., Dept. 52-9 43 West 61st Street, New York 23, N. Y.*

**Internationally Acclaimed!**

"The recording is of such perfection it seems to bring the artists into your living room" —*Glorious Sounds, Amsterdam, Holland.*

"Excellent series of records" —*The Saturday Review, New York.*

The Musical Masterpiece Society, Inc. Dept. 52-9
43 West 61st Street, New York 23, N. Y.

**ALL 10 MASTERPIECES — FREE!**

I enclose 25¢ to help cover cost of postage. Please send me ALL 10 of the masterpieces listed above and enroll me as a trial member. Send me notice of *future* selections which I may try for 5 days without cost or obligation. For those *future* l.p. discs I decide to keep after I have tried them, I will pay only the special member's price of $1.65 each, plus few cents shipping. I may cancel my trial membership at any time. This offer restricted to new Trial Memberships—only one sample package per family.

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# Sensational!

## Retract·O·Matic

***—the new, foolproof replacement***

## Pickup

**Even if you drop it...or *slide* it...**

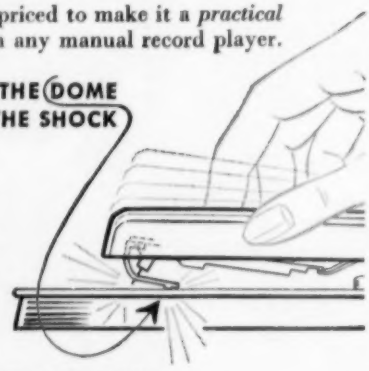
**Retract·O·Matic protects records and needles from damage!**

WEBSTER ELECTRIC proudly offers the new, exclusive RETRACT·O·MATIC—the sensational crystal pickup that provides positive protection to record and needle, *even when it is dropped or slid* across the record surface.

Retract·O·Matic is priced to make it a *practical replacement* for installation on any manual record player.

**THE DOME ABSORBS THE SHOCK**

The unique spring-mounted construction gives absolute insurance against damage to cartridge, needle, or record. The slightest pressure on the arm automatically lifts the needle from the record's surface, and lets Retract·O·Matic's rounded "dome" absorb the shock.



## A BIG PROFITABLE MARKET

Retract·O·Matic is a "natural" as a pickup replacement for record players, children's and portable phonographs. List price of complete assembly (tone arm, cartridge, arm rest and all parts needed for installation) is only $6.95—little more than the price of the cartridge alone. Order a stock today. Step up your sales with Retract·O·Matic!

**WEBSTER ELECTRIC**
RACINE WISCONSIN




bass. Since that time I have tried many combinations of very fine and cheap speakers. At the moment I am using a pair of Hartley 215's and an RCA LC1A. Down to 25 cycles I consider this to be equal in response and superior in definition to any horn I have ever heard. However, I have never obtained poor sound, even with the cheapest speakers.

In choosing speakers for multiple coupling apply these basic principles:

1. Use speakers as good individually as you can afford and particularly speakers with low resonant points. (However, I am not sure that the woofers designed for Klipsch type horns will work well in an infinite baffle of this type.)
2. Choose dissimilar speakers. Speakers of the same cone size but different make almost invariably differ in resonance and other characteristics.
3. Stagger the resonance of the speakers. Even if you use speakers with very low resonant points (30 to 45 cycles), it is preferable to have the resonant points of the different speakers vary by from 5 to 10 cycles. (I am presuming that the amplifier used will have a good damping factor to level the resonant peaks.)

Personally I prefer to use wide-range speakers without crossovers—except the blocking capacitor needed to protect a tweeter from low-frequency overloads. It is true that a *single* wide-range speaker will probably have more intermodulation distortion than a system of two or three speakers with divided frequency range. However, when multiple speakers are used, the individual speakers operate with higher efficiency and at a much lower output level and, therefore, the individual speakers operate over a much more favorable portion of their dynamic curve. Distortion is thus reduced. Elimination of crossovers also eliminates the phasing effects and the distortion produced by the crossover filters.

When it is necessary to limit the frequency range of any speaker, I prefer the simplest possible filter—a capacitor for tweeters and a series inductance for woofers. Unless the individual speakers used have an extremely wide range it will be necessary to add a tweeter or a super-tweeter to cover the upper octave or two. In such cases I use a capacitor chosen to produce rolloff at the low end close to the point where the main speakers begin to roll off at the high end, and an L or T pad to control the tweeter response.

If one or more of the speakers are coaxial or triaxial combinations with dividing networks, use the combination as one unit, paralleling it with other speakers or units.

The speakers are hooked up in series-parallel to make up a net impedance satisfactory for the amplifier in use. By varying the position of the individual speakers in the series-parallel

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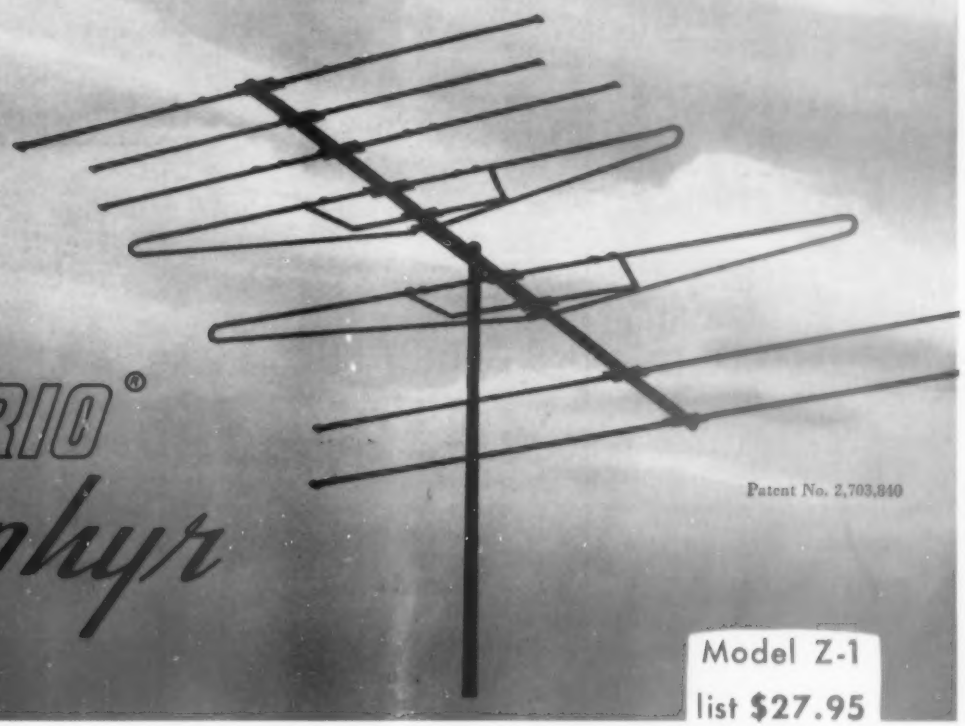

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Zephyr

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Superior Performance  Fast Assembly
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Millions of Insta-loks used! Tested and proven to be the best, both here and abroad.

The Trio Zephyr gives top performance on all VHF channels with its revolutionary "Wing Dipole"—three half-wave elements in phase combined with an integrated director element makes each dipole a unidirectional antenna on the high channels.

The two driven elements are self-resonant to a different frequency and the elements are so spaced and so connected with respect to each other that during operation of the array on any one of the frequencies for which an element is resonant all of the elements are energized as active, or driven elements and at the same time each element is also operative as a parasitic element with respect to each of the other elements.

Single bay out-performs bulky stacked arrays but may be stacked in exceptional fringe areas.

TRIO Manufacturing Company
GRIGGSVILLE, ILLINOIS

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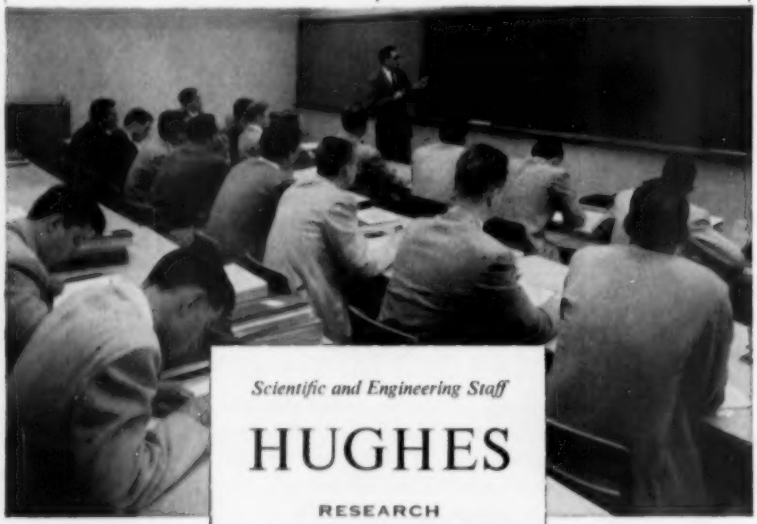
# Apply Your Electronics Experience

ENGINEERS AND PHYSICISTS WITH ELECTRONICS TRAINING ARE NEEDED TO CONDUCT CLASSROOM AND LABORATORY PROGRAMS ON ADVANCED SYSTEMS WORK IN THE FIELDS OF RADAR FIRE CONTROL, ELECTRONIC COMPUTERS, GUIDED MISSILES.

*The proper functioning of the complex airborne radar and computer equipment produced by Hughes requires well-trained maintenance crews in the field.*

At Hughes Research and Development Laboratories in Southern California engineers assigned to this program are members of the Technical Staff. As training engineers they instruct in equipment maintenance and operation for both military personnel and field engineers.

*Prior to assignment, engineers participate in a technical training program to become familiar with latest Hughes equipment. After-hours graduate courses under Company sponsorship are available at nearby universities.*



*Scientific and Engineering Staff*

HUGHES

RESEARCH AND DEVELOPMENT LABORATORIES

*Culver City, Los Angeles County, California*




network, it is possible to proportion the input voltage to each speaker to match its sensitivity or to manipulate the frequency response. For example, just before using the LC1A and the Hartleys, I used an RCA 515S2, two 12-inch speakers of the PA type and a tweeter. These were hooked up as in *a* of Fig. 3. At one point I used an 8-ohm woofer, the two 12-inch speakers and a tweeter and hooked them up as in *b* of Fig. 3. The total impedance at mid-frequencies was about 6 ohms, but at low frequencies the woofer received a higher proportion than the two 12-inch speakers. The present combination of the LC1A and the Hartleys is hooked up as in *c* of Fig. 3 so that the input is divided 50% to the LC1A and 50% to the two Hartleys.

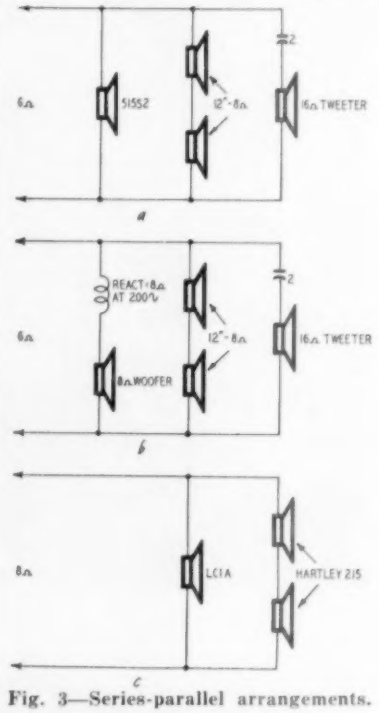



**Fig. 3—Series-parallel arrangements.**

The speakers have to be in phase, of course. This is easily adjusted by feeding the speakers through the amplifier with a low-frequency tone or manipulating amplifier and preamp controls to produce the highest hum and changing speaker leads to produce highest output.

The principle of mutual coupling can be applied to complete speaker systems. Thus two small bass-reflex systems can be stacked or used side by side to provide a considerable increase in bass efficiency. Two of the small K5 horns could be stacked in a corner, one above the other, to obtain an even more dramatic improvement.

In any case I commend the mutual-coupling principle to experimenters and engineers as well. Very little work has been done with it and its capabilities are far from explored. END

# How to hand yourself more business

Whenever you replace a tube, it's smart to hand the lady the CBS carton . . . and yourself more business.

It's smart because CBS tubes are advertised to *women* in Life, Good Housekeeping and on Arthur Godfrey's Talent Scouts.

And it's good business for you because *women* have greater confidence in CBS tubes . . . the tubes with the Good Housekeeping Guaranty Seal.

*There are no better tubes made than CBS tubes.*

Guaranteed by Good Housekeeping

**CBS-HYTRON,** Danvers, Massachusetts

A DIVISION OF COLUMBIA BROADCASTING SYSTEM, INC.

Measures 6¼" x 9½" x 4½"

*Superior's new Model 670-A*

# SUPER METER

## *A COMBINATION* VOLT-OHM MILLIAMMETER PLUS CAPACITY REACTANCE INDUCTANCE AND DECIBEL MEASUREMENTS

**SPECIFICATIONS:**

**D.C. VOLTS:** 0 to 7.5/15/75/150/750/1,500/7,500 Volts
**A.C. VOLTS:** 0 to 15/30/150/300/1,500/3,000 Volts
**OUTPUT VOLTS:** 0 to 15/30/150/300/1,500/3,000 Volts
**D.C. CURRENT:** 0 to 1.5/15/150 Ma. 0 to 1.5/15 Amperes
**RESISTANCE:** 0 to 1,000/100,000 Ohms 0 to 10 Megohms
**CAPACITY:** .001 to 1 Mfd. 1 to 50 Mfd. (Good-Bad scale for checking quality of electrolytic condensers.)
**REACTANCE:** 50 to 2,500 Ohms 2,500 Ohms to 2.5 Megohms
**INDUCTANCE:** .15 to 7 Henries 7 to 7,000 Henries
**DECIBELS:** −6 to +18 +14 to +38 +34 to +58

**ADDED FEATURE:**
**Built-in ISOLATION TRANSFORMER reduces possibility of burning out meter through misuse.**

The Model 670-A comes housed, in a rugged crackle-finished steel cabinet complete with test leads and operating instructions.

**$28.40 NET**

*Superior's new Model TV-11*

# TUBE TESTER

**SPECIFICATIONS:**

★ Tests all tubes including 4, 5, 6, 7, Octal, Lock-in, Peanut, Bantam, Hearing Aid, Thyratron Miniatures, Sub-miniatures, Novals, Sub-minars, Proximity fuse types, etc.

★ Uses the new self-cleaning Lever Action Switches for individual element testing. Because *all elements are numbered according to pin-number in the RMA base numbering system*, the user can instantly identify which element is under test. Tubes having tapped filaments and tubes with filaments terminating in more than one pin are truly tested with the Model TV-11 as any of the pins may be placed in the neutral position when necessary.

★ The Model TV-11 does not use any combination type sockets. Instead individual sockets are used for each type of tube. Thus *it is impossible to damage a tube by inserting it in the wrong socket.*

★ Free-moving built-in roll chart provides complete data for all tubes.

★ Newly designed Line Voltage Control compensates for variation of any Line Voltage between 105 Volts and 130 Volts.

★ NOISE TEST: Phono-jack on front panel for plugging in either phones or external amplifier will detect microphonic tubes or noise due to faulty elements and loose internal connections.

***EXTRA SERVICE*** — The Model TV-11 may be used as an extremely sensitive Condenser Leakage Checker. A relaxation type oscillator incorporated in this model will detect leakages even when the frequency is one per minute.

The model TV-11 operates on 105-130 Volt 60 Cycles A.C. Comes housed in a beautiful hand-rubbed oak cabinet complete with portable cover

**$47.50 NET**

## *About Testing Picture-Tubes . . .*

*Of course you can buy an "adapter" which theoretically will convert your standard Tube Tester into a picture-tube tester. Sounds fine—but—it simply doesn't work out that way!*

*We do not make nor do we recommend use of C.R.T. adapters because a Cathode Ray Tube is a very complex device and to properly test it, you need an instrument designed exclusively to test C. R. Tubes and nothing else. As compared to a make-shift adapter, which sells for about five dollars, our Model TV-40 C.R.T. Tube Tester sells for $15.85. But, if you believe that Television is here to stay, then you must agree that the difference in price is more than justified by the many years of valuable service you will get out of this indispensible instrument.*

*Incidentally, the Model TV-40 is the ONLY low-priced C.R.T. Tube Tester, which includes a real meter. Neons are fine for gadgets and electric-line testers, but there is no substitute for a meter with an honest-to-goodness emission reading scale.*

*Superior's New Model TV-40*

# C.R.T. TUBE TESTER

**Tests ALL magnetically deflected tubes . . . in the set . . . out of the set . . . in the carton ! !**

- Tests *all* magnetically deflected picture tubes from 7 inch to 30 inch types.
- Tests for quality by the well established emission method. All readings on "Good-Bad" scale.
- Tests for inter-element shorts and leakages up to 5 megohms.
- Test for open elements.

**EASY TO USE:** Simply insert line cord into any 110 volt A.C. outlet, then attach tester socket to tube base (tan trap need not be on tube). Throw switch up for quality test . . . read direct on Good-Bad scale. Throw switch down for all leakage tests.

Model TV-40 C.R.T. Tube Tester comes absolutely complete —nothing else to buy. Housed in round cornered, molded bakelite case. Only

**$15.85 NET**

# SHIPPED ON APPROVAL

# *NO MONEY WITH ORDER — NO C.O.D.*

Try any of the above instruments for 10 days before you buy. If completely satisfied *then* send down payment and pay balance as indicated on coupon. **No Interest or Finance Charges Added!** If not completely satisfied return unit to us, no explanation necessary.

**MOSS ELECTRONIC DISTRIBUTING CO., INC.**
**Dept. D-159, 3849 Tenth Ave., New York 34, N.Y.**

Please send me the units checked. I agree to pay down payment within 10 days and to pay the monthly balance as shown. It is understood there will be no finance, interest or any other charges, provided I send my monthly payments when due. It is further understood that should I fail to make payment when due, the full unpaid balance shall become immediately due and payable.

Name .....

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City ..... Zone ..... State .....

☐ Model 670-A ..... Total Price $28.40 — $7.40 within 10 days. Balance $3.50 monthly for 6 months.

☐ Model TV-11 ..... Total Price $47.50 — $11.50 within 10 days. Balance $6.00 monthly for 6 months.

☐ Model TV-40 ..... Total Price $15.85 — $3.85 within 10 days. Balance $4.00 monthly for 3 months.

# The Model TV-50 GENOMETER

A versatile all-inclusive **GENERATOR** which provides ALL the outputs for servicing:

**A. M. Radio  F. M. Radio  Amplifiers  Black and White TV  Color TV**

## 7 Signal Generators in One!

- R. F. Signal Generator for A.M.
- R. F. Signal Generator for F.M.
- Audio Frequency Generator
- Bar Generator
- Cross Hatch Generator
- Color Dot Pattern Generator
- Marker Generator

## SPECIFICATIONS:

### R. F. SIGNAL GENERATOR:

The Model TV-50 Genometer provides *complete* coverage for A.M. and F.M. alignment. Generates Radio Frequencies from 100 Kilocycles to 60 Megacycles on fundamentals and from 60 Megacycles to 180 Megacycles on powerful harmonics. Accuracy and stability are assured by use of permeability trimmed Hi-Q coils. R.F. is available *separately*, modulated by the fixed *400 cycle sine-wave* audio or modulated by the *variable* 300 cycle to 20,000 cycle variable audio. Provision has also been made for injection of any external modulating source.

### VARIABLE AUDIO FREQUENCY GENERATOR:

In addition to a fixed 400 cycle sine-wave audio, the Model TV-50 Genometer provides a variable 300 cycle to 20,000 cycle peaked wave audio signal. This service is used for checking distortion in amplifiers, measuring amplifier gain, trouble shooting hearing aids, etc.

### BAR GENERATOR:

This feature of the Model TV-50 Genometer will permit you to throw an actual Bar Pattern on any TV Receiver Screen. Pattern will consist of 4 to 16 horizontal bars or 7 to 20 vertical bars. A Bar Generator is acknowledged to provide the quickest and most efficient way of adjusting TV linearity controls. The Model TV-50 employs a recently improved Bar Generator circuit which assures stable never-shifting vertical and horizontal bars.

### CROSS HATCH GENERATOR:

The Model TV-50 Genometer will project a cross-hatch pattern on any TV picture tube. The pattern will consist of non-shifting, horizontal and vertical lines *interlaced* to provide a stable cross-hatch effect. This service is used primarily for correct ion trap positioning and for adjustment of linearity.

### DOT PATTERN GENERATOR *(For Color TV)*:

Although you will be able to use most of your regular standard equipment for servicing Color TV, the one addition which is a "must" is a Dot Pattern Generator. The Dot Pattern projected on any color TV Receiver tube by the Model TV-50 will enable you to adjust for *proper color convergence*. When all controls and circuits are in proper alignment, the resulting pattern will consist of a sharp white dot pattern on a black background. One or more circuit or control deviations will result in a dot pattern out of convergence, with the blue, red and green dots in overlapping dot patterns.

### MARKER GENERATOR:

The Model TV-50 includes *all* the most frequently needed marker points. Because of the ever-changing and ever-increasing number of such points required, we decided against using crystal holders. We instead adjust each marker point against precise laboratory standards. The following markers are provided: 189 Kc., 262.5 Kc., 456 Kc., 600 Kc., 1000 Kc., 1400 Kc., 1600 Kc., 2000 Kc., 2500 Kc., 3579 Kc., 4.5 Mc., 5 Mc., 10.7 Mc. (3579 Kc. is the color burst frequency.)

The Model TV-50 comes absolutely complete with shielded leads and operating instructions. Only

**$47.50 NET**

# SHIPPED ON APPROVAL

## NO MONEY WITH ORDER — NO C. O. D.

Try it for 10 days before you buy. If completely satisfied *then* send $11.50 and pay balance at rate of $6.00 per month for 6 months. **No Interest or Finance Charges Added!** If not completely satisfied return unit to us, no explanation necessary.

**MOSS ELECTRONIC DISTRIBUTING CO., INC.**
**Dept. D-159, 3849 Tenth Ave., New York 34, N.Y.**

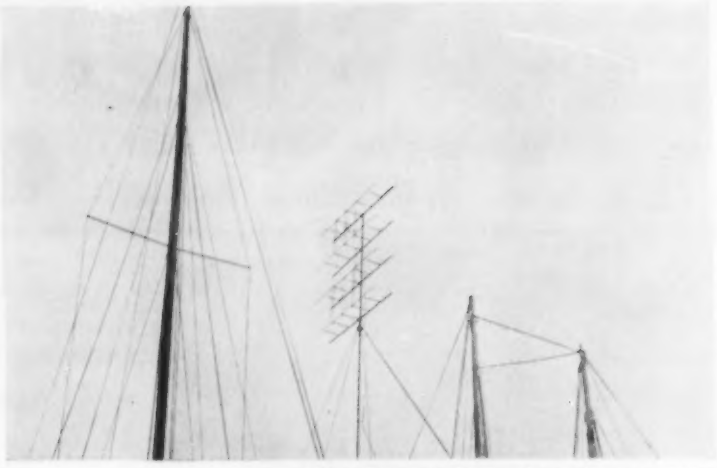
Please rush me one Model TV-50. I agree to pay $11.50 within 10 days and to pay $6.00 per month thereafter. It is understood there will be no finance, interest or any other charges, provided I send my monthly payments when due. It is further understood that should I fail to make payment when due, the full unpaid balance shall become immediately due and payable.

Name _____

Address _____

City _____ Zone _____ State _____

*Analyzing and eliminating this seagoing scourge*



TV antennas between the main and mizzen.

# BOAT ELECTROLYSIS

By ELBERT ROBBERSON

YOU can find pleasure boats almost anywhere. And on these boats, TV masts are sprouting between the main and the mizzen. As a result, radio service technicians are called on for more and more marine electronic work. This is not restricted to marine radiotelephones. If you handle TV, record players, clock radios or battery chargers, some boatmen may call on you for service. The marine market is good, *provided you're checked out on electrolysis.* If not, it can be dangerous. A mistake can sink a boat!

As applied to marine electronics, electrolysis is the decomposition of underwater metal by an electric current. While this condition is most prevalent in salt water, action can also take place in dirty or polluted fresh water. "But all I'm going to do is install a TV set," you say. "How am I involved?"

One of the peculiarities of boat installations is that no matter what kind of electronic equipment you bring aboard, there is a chance that what you do *can* cause electrolysis. And in any event, boatmen are inclined to blame any underwater corrosion on the last piece of electronic gear installed. So if all you do is to sell some skipper an electric razor, if a dirty spot shows up on the boat's propellor you may be called upon to defend the razor and your knowledge of matters marine.

Shipboard electrolysis is of two kinds, which for the sake of simplicity we will call *natural* and *forced*. We are concerned with both of them.

*Natural electrolysis* occurs when two dissimilar metals are placed underwater and then provided with a connection for current flow. The amount of electrolytic activity depends upon the position of the metals in the Galvanic series shown in the table. The farther apart in the series a pair of metals are, the greater the action between them. Of any two metals in such a combination, the higher one on the list will corrode.

The action can be shown with a simple cell composed of a copper and a galvanized-iron electrode immersed in sea water. The open-circuit voltage of such a cell is about 0.7 volt. When the two electrodes are connected together by a low-resistance conductor, a current of several milliamperes per square inch will flow between them, and the galvanized iron wastes away. Disconnect the electrodes, and the flow of current and deterioration of the "base" metal electrode will no longer continue.

**METALS IN GALVANIC SERIES***

*Corroded end (anodic, or least noble)*
Magnesium
Magnesium alloys
Zinc
Aluminum 2S
Cadmium
Aluminum 17ST
Steel or iron
Cast iron
Chromium-iron (active)
Ni-Resist
18-8 stainless (active)
18-8-3 stainless (active)
Lead-tin solders
Lead
Tin
Nickel (active)
Inconel (active)
Brasses
Copper
Bronzes
Copper-nickel alloys
Monel
Silver solder
Nickel (passive)
Inconel (passive)
Chromium-iron (passive)
18-8 stainless (passive)
18-8-3 stainless (passive)
Silver
Graphite
Gold
Platinum
*Protected end (cathodic, or most noble)*

*Groups of metals indicate they are closely similar in properties.

*Forced electrolysis* is caused by the external application of voltage between underwater metals. With a battery of only 6 volts connected between two underwater boat fittings, the one on the positive side of the battery begins to disappear at an alarming rate—25% per hour is not uncommon. If the disappearing metal belongs to an underwater fitting such as an engine cooling-water intake, water soon starts coming into the boat. In time, it could sink. Knowing this to be the case, you might think anyone would be stupid to connect a battery between any underwater metals. But if you aren't acquainted with some of the peculiarities of small-boat electrical hookups, accidents such as battery cross-connection are easy.

## Natural electrolysis

This form will attack any metal exposed to weather or in contact with water. Any metal, such as antennas, guys, ground plates and fittings, installed under these conditions must be noncorrosive in a salt solution. This rules out using any material such as iron or untreated aluminum, which rusts or corrodes by itself. (Anodized aluminum, galvanized iron are treated to resist corrosion.)

Use only materials which the manufacturers will certify for salt water. The usual hardware-store brass does not qualify. The reason is simple: brass is compounded of copper and zinc. Copper is noble, zinc is base. And as soon as the alloy is wet the closely connected molecules start acting like a battery of zinc–copper cells. De-zincing takes place rapidly, and the metal turns into a soft reddish mass you can cut with a fingernail.

Fastenings are most critical because they can least afford to lose any metal.

**Formerly galvanized shackle was connected to a stainless-steel mooring pennant for one season—blamed on technician.**

Typical electrolysis "protector" installation with zinc blocks on propeller strut, ground plate and zinc collar on shaft.

Use only certified marine fastenings, such as marine bronze, "Everdur," "Monel" or stainless steel. They are more expensive and they may be hard to get in some localities, but they won't pull apart in your hands a month after they are installed on a boat.

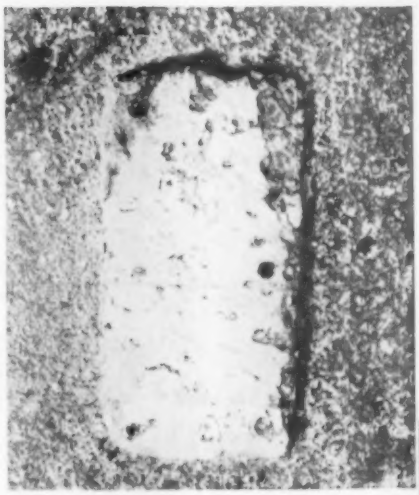
Some electronic installations require a ground. This is often done by a connection to the boat's engine, with its cooling-water inlet, the propeller shaft and "wheel" furnishing the required path to "earth." For a better ground, a "ground plate" is fastened on the hull.

Ordinarily, using an engine ground will have no effect on any natural electrolysis which may be going on. If something was dissolving before you brought your gear aboard, it will go on dissolving. A bronze propeller will continue to lose metal to a Monel shaft; iron fittings will give away material to almost anything else around and brass screws will keep on disappearing.

But installing a ground plate on the bottom of a boat can somewhat disturb existing relations. Most underwater metal, such as water scoops, outlets, propellers, rudder fittings, etc., are cast or forged of some alloy. Even the best alloys are not absolutely homogeneous—pockets of impurities are scattered throughout the smoothest-appearing metal. When these impurities face only a small amount of other metal in water, decomposition is slow. But place a pure copper ground plate of several feet area close by, connect the system together electrically and the loss of base metal will accelerate. The closer nonhomogeneous metal is to the ground plate, the more rapid decay will be.

This effect is seldom extensive or rapid enough to cause damage. However, it will cause surface pitting and discoloration, depending upon the amount of impurities involved. Usually, the main effect is psychological. The boatman, knowing that electrolysis can be dangerous, will be upset to find any traces of increased activity.

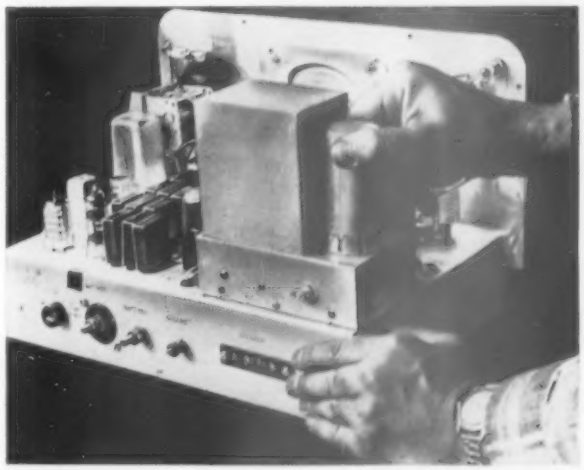
The magnitude and direction of ground-plate current can be measured with a milliammeter. Although the relation of metal transfer to current



**Badly eroded zinc block after much use.**

**Screws missing from stern —the result of electrolysis between dissimilar metals.**

**Electrolysis in poor alloy propeller.**



**Polarity-sensitive marine equipment such as this radiotelephone can be adapted for boat's ground by reversing vibrator.**

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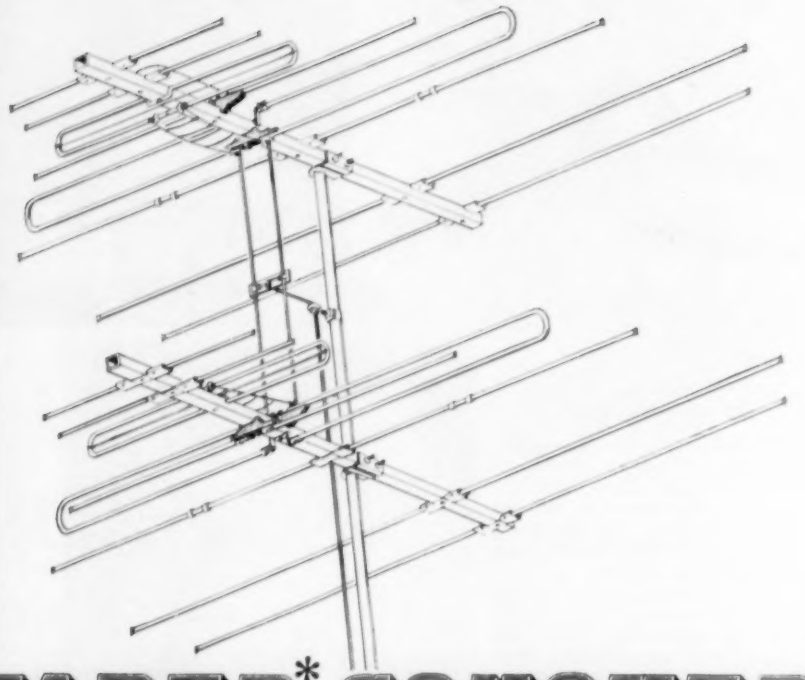

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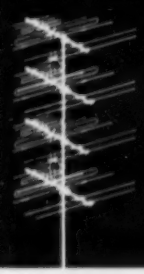

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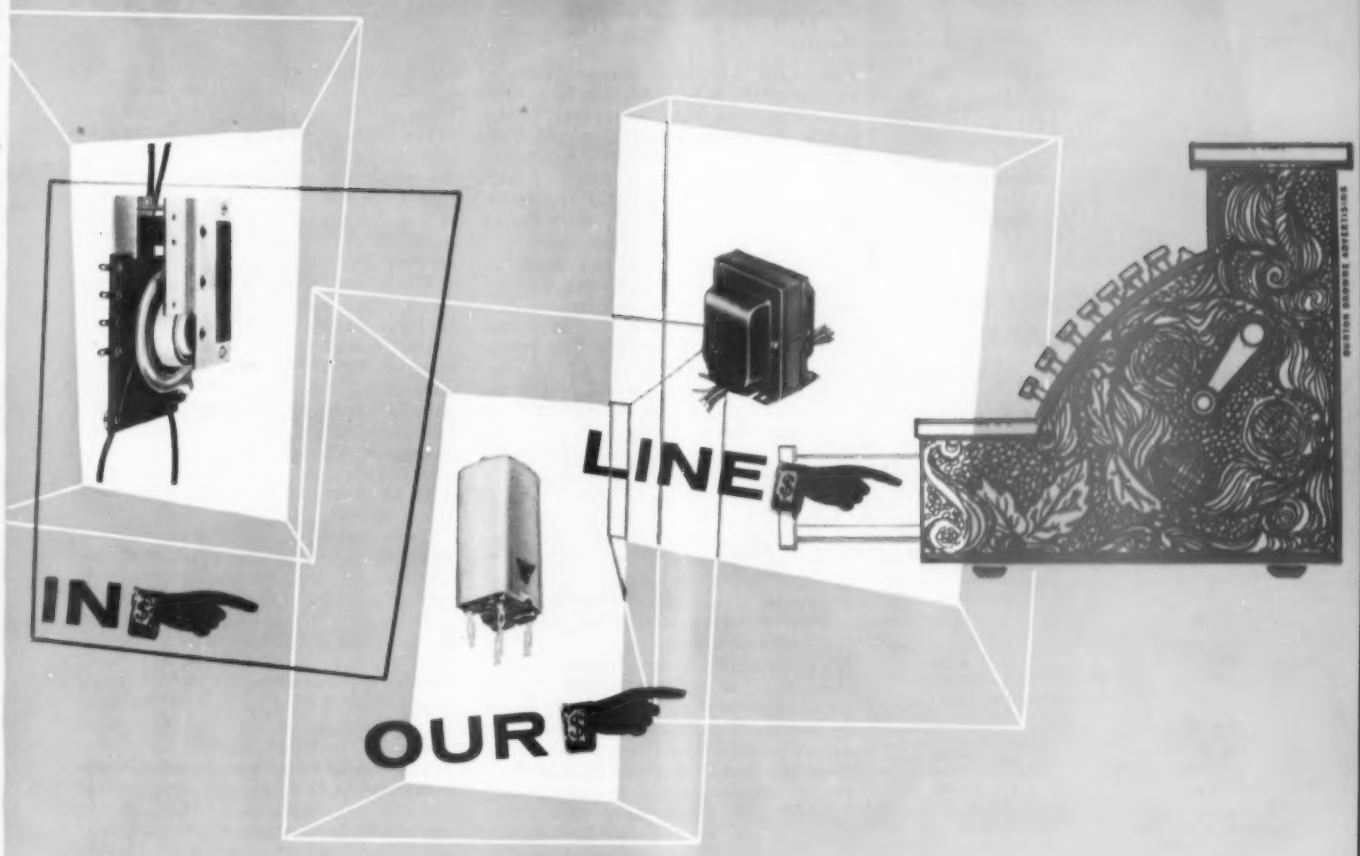


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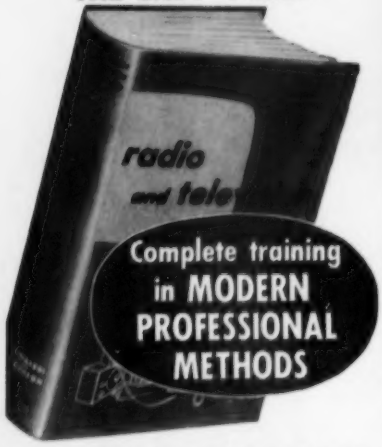


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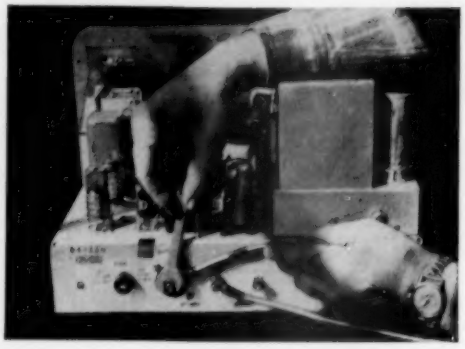

**Cross-connections can be avoided by using distinctive marking for "hot" supply wires. In this unit a tape square is used.**

flow varies with electrode composition, an idea of the safe limits may be gained from the fact that a typical fitting tested showed a weight loss of about .00005 ounce per milliampere per hour: a rate of 1 ounce per 2 years of constant action. A current of a few milliamperes is common and won't harm reasonably heavy fittings for years.

Many attempts have been made to devise a method for reducing natural electrolysis. The seriousness of the problem is pointed up by the fact that during one stage of shipbuilding evolution electrolysis would eat whole rows of rivets out of ship bottoms, even causing ships to drop plates! One of the remedies attempted, still with us, is the use of a zinc (or now that the newer metals are plentiful, aluminum and magnesium) "protector" (see photo) in the form of a plate, collar or cap. Having higher electrolytic activity than other nearby metals, the protector is intended to divert activity to itself, absorbing the major flow of current.

There is little evidence that such protectors divert much more than the viewer's attention by their extreme deterioration, but you will find boats with zinc plates plastered all over the hull and its fittings. Naturally, if you install a copper ground plate, base metal facing it in the water is going to disappear faster. The owner will become greatly alarmed. You might have to convince him that the easiest way to keep the zinc plates from disappearing so fast is to leave them on the hardware store's shelf.

### Forced electrolysis

The most spectacular form of electrolysis is the kind forced by externally applied voltage. Accidents leading to this condition are due to the fact that one side of the battery is almost invariably grounded. In performance, ground polarity makes no difference. And in safety from electrolysis, the ground polarity is likewise unimportant—as long as every other device connected has the same ground polarity.

All ground returns must be heavy enough to prevent voltage drops from appearing between grounded points. To prevent insulation failure from making things "hot," motor frames, shells of fixtures and any metal which can contact the water should be bonded to the main ground with wire of at least No. 10 gauge. Of course, this connection can cause a new flow of natural electrolytic current which did not exist before, but the small amount of metal deterioration from this activity is a low price to pay for protection against the much more dangerous possibility of battery current between underwater fixtures.

While the electrical equipment on small boats operates from the engine battery, larger vessels carry auxiliary battery banks of 12, 32 or 120 volts, charged by a separate engine-driven generator. The auxiliary system is usually grounded on the negative side, but installations will be found where the opposite is the case. The largest vessels usually are more wisely designed, with an underground or "floating" electrical system.

Twin-engine boats will have two identical engine electrical systems, with the above auxiliary system. However, twin-engine boats will also be found with the positive side of one engine battery and the negative side of the other grounded. This gives 12 volts between the "hot" sides of the two batteries for lights and accessories. With this circuit, the electrical midpoint of the system is connected to the boat's ground.

The main thing for the electronics technician is to make sure what ground polarity the boat uses. Then, if the equipment has one side of the input circuit grounded, the polarity must agree with that of the vessel. In boats having the battery midpoint grounded, neither side of the auxiliary equipment's input can be grounded for d.c.

Most equipment with grounded input can be modified for either ground polarity by reversing switches, turning vibrators around in their sockets or by wiring changes. Any equipment that can or must be grounded, but which cannot conform to the boat's ground polarity, is unsafe.

You can test for cross-grounds and stray battery current which might cause electrolysis. Turn off everything electrical aboard. Disconnect one lead at the battery post, then insert an ammeter in the circuit at this point. A volt-ohm-milliammeter having a 10-amp range is best for this purpose. If no current flow shows on the 10-amp

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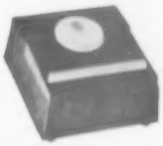

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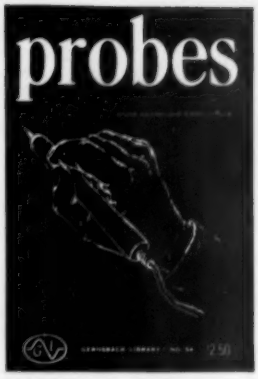


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range, drop down to the 500-ma range. If no current shows, drop down again and continue until the scale is reached where leakage current can be measured. There will usually be some leakage, except in a very new and dry boat. The importance of battery leakage depends upon the current flow, just as in the case of natural electrolysis measuring, described earlier. A few milliamperes won't harm anything — but leakage above a very small value should be traced and eliminated, if possible. Leakage of a good fraction of an ampere or whole amperes means danger—disconnect at once and find the cross-connection before a diving suit is needed!

Modern "marine living" has spawned large fleets of boats using shoreline a.c. while they are tied to the dock. Battery chargers, vacuum cleaners, TV sets and hi-fi systems are only a few of the devices used on such boats. Great care must be used not to ground any part of such equipment's circuits unless the gear is specifically engineered for marine service.

An example of dangerous equipment is a battery charger using an autotransformer to step the line voltage down to battery level. Connect the charger output to boat batteries, and a.c. up to 117 volts will appear between underwater boat fixtures and the shore. It won't take long for massive destruction of metal to take place! Such equipment must have an isolating transformer.

Another example is the usual radio or TV, which has noise-filter capacitors between the a.c. input and the chassis. These capacitors form a voltage divider, placing the chassis one-half the line voltage above ground. Connecting the chassis to a boat ground puts about 50 volts underwater where it shouldn't be. Ground connections required for such devices should be made only through a mica capacitor just big enough to pass the desired r.f. current.

The a.c. ground currents can be measured in the same manner as d.c. currents. Use the procedure described, with an a.c. meter for heavy flow and an a.c. (or the r.f. variety will work very well) milliammeter to check for smaller currents. If a.c. flow of sizable proportions is detected, the source should be localized and stopped off.

A peculiar case can exist where a well-bonded and blameless boat can lie adjacent to a boat or a dock having improperly grounded a.c. fixtures. Current flowing through the water from the "culprit" can pass through the fittings and ground system of the blameless boat on its path to shore and cause electrolysis. This can be detected by an a.c. reading of ground-plate current. If such a condition is found, the only remedy is to move to a safer location.

The whole matter of preventing electrolysis amounts simply to the prevention of the flow of current through an electrolytic path. On a boat, this means current through the water. Prevent this flow by any means available, and the boat's metal will stay in place. END

# telrex THUNDERBIRDS

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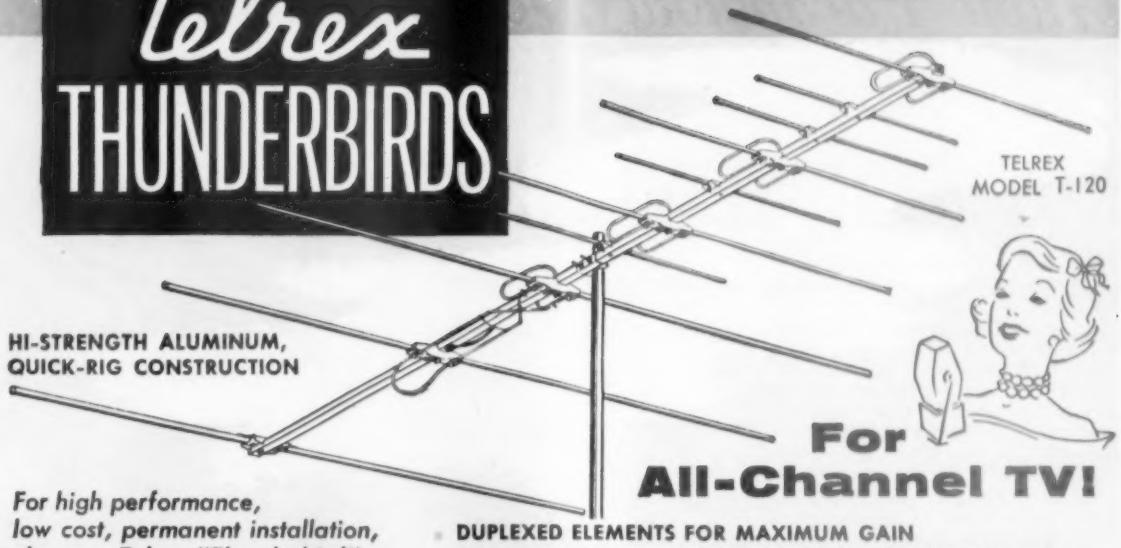

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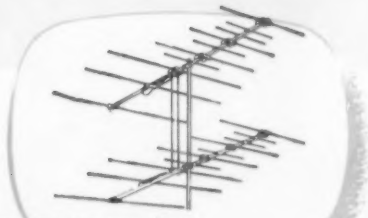
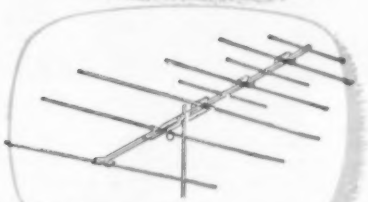
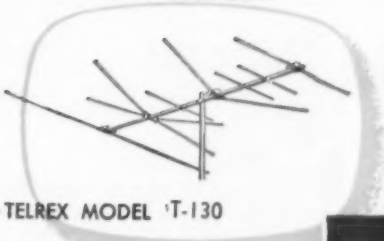


• TELREX MODEL T-122



• TELREX MODEL T-110



• TELREX MODEL T-130

**Super Thunderbird Model T-120** is the finest wide-band, multi-element array ever developed. A system of variable impedance phasing loops permit precision tuning and the duplexing of element functions to provide the equivalent of 6 operating elements on the LO channels; 13 elements on the HI channels. Element for element, they develop greater gain and directivity than many single channel arrays. **Model T-120** is accurately matched to 200-300 ohm transmission line for both HI and LO channels with compensated "trombone" sections to yield exceptionally highgain and optimum signal transfer efficiency. LO band gain averages better than 5.5 db; HI band gains exceed 12 db, while front-to-back ratios range to 25 db.

For brilliant, interference-free signals under toughest reception conditions, choose the Telrex **Super Thunderbird T-120!** Available also in 2 bay units—**Model T-122,** 1/4-wave stacked for gain increases averaging 3 db on all channels; and **Model T-122S,** 1/2-wave stacked to provide gain increases up to 4.5 db on LO channels, over single bay units.

**Thunderbird Model T-110** incorporates all the high-performance features of the **Super Thunderbird T-120** including variable impedance loop phasing, compensated "trombone" matching sections and in-line low wind resistance configuration plus high strength, all aluminum, quick-rig construction for dependable, high performance, low cost, long lasting installations. Duplexed elements are equivalent to 5 effective elements on LO channels for average gains exceeding 5 db; and 11 operating elements on the HI channels for gains exceeding 10 db. Front-to-back and front-to-side ratios of better than 22 db minimize interference.

Available stacked 1/4-wave, **Model T-112,** for all channel gain increases of 3 db; and 1/2-wave stacked, **Model T-112S,** for increased gains to 4.5 db on LO channels.

**Thunderbird T-130** employs Conical Dipole and "V" Beam quadrature phased driven elements to achieve virtually flat, stepless gain characteristics on all VHF channels with minimum number of elements. **Model T-130** also employs variable impedance phasing loops, duplexed elements and Telrex compensated "trombone" matching sections. Four effective LO channel elements; 9 operating elements on HI channels, produce gains to 5 db on 2-6, and up to 11 db on channels 7-13. Special trap circuitry used in all Thunderbirds, attenuates interference arising outside the assigned TV bands to assure crisp, smear-free picture quality and full sound response.

**Model T-132,** stacked 1/4-wave gives average gain increase of 3 db on all channels; 1/2-wave stacked **Model T-132S** provides up to 4.5 db gain on LO channels over single bay.

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# *Giant Paraboloid Detects Radio Stars*

*Huge "telescope" detects signals from the far reaches of the universe*

By R. HANBURY BROWN*

MOST of man's knowledge of the universe has been gained by the use of his eyes. The human eye is sensitive to electromagnetic waves of lengths between about $7 \times 10^{-5}$ cm (red) and $4 \times 10^{-5}$ cm (violet). We can see the sun and the stars because waves of this length are transmitted through the earth's atmosphere with little loss. Fig. 1 shows how the transmission through the atmosphere varies with wavelength. There are two main bands in the spectrum through which electromagnetic waves can reach the earth from outer space. The first band extends from ultra-violet waves through the region of visible light to the infra-red. At each end of this band the transmission is shut off by absorption in the earth's atmosphere. The second band lies in the region of radio waves and extends from waves of about 1 cm to about 60 meters in length. This band is bounded at the shortwave end by absorption in the water vapor and other gases of the earth's atmosphere, and at the long-wave end by absorption high up in the ionosphere.

In 1932 Karl Jansky, working on atmospherics at the Bell Telephone Laboratory, discovered that radio waves are reaching the earth from outer space and that they apparently originate in the Milky Way. This discovery pointed the way to a new branch of science now called "radio astronomy." Today, radio astronomers are exploiting the radio "window" through the earth's atmosphere to gain new knowledge of the universe beyond. Perhaps the most interesting discovery that they have made is the existence of the so-called "radio stars." About 150 have been found and the majority of them have not been identified with any known celestial object. They appear to emit radio waves but give little or no light. They present a fascinating problem to modern astronomy.

To collect visible light from the stars the astronomer builds large mirrors which focus the light onto the eyepiece or onto the photographic plate of his telescope. The largest mirror in existence today is the 200-inch mirror of the Hale telescope at Palomar Mountain. The radio astronomer, working with much longer waves, uses large antenna systems to collect radio waves and calls his instrument a radiotelescope. The largest radiotelescope in existence is at the Jodrell Bank Experimental Station of the University of Manchester (England).

**The giant paraboloid — 218-foot diameter.**

*Jodrell Bank Experimental Station, Crewe, Cheshire, England.

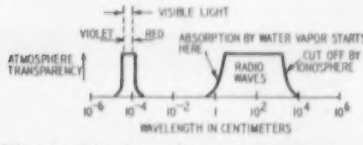



**Fig. 1—Diagram shows transmission of electromagnetic energy in atmosphere.**

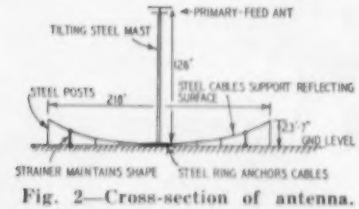



**Fig. 2—Cross-section of antenna.**

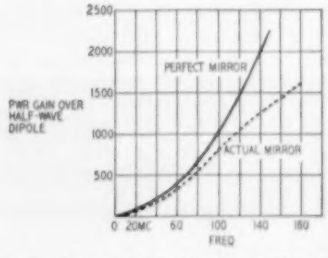
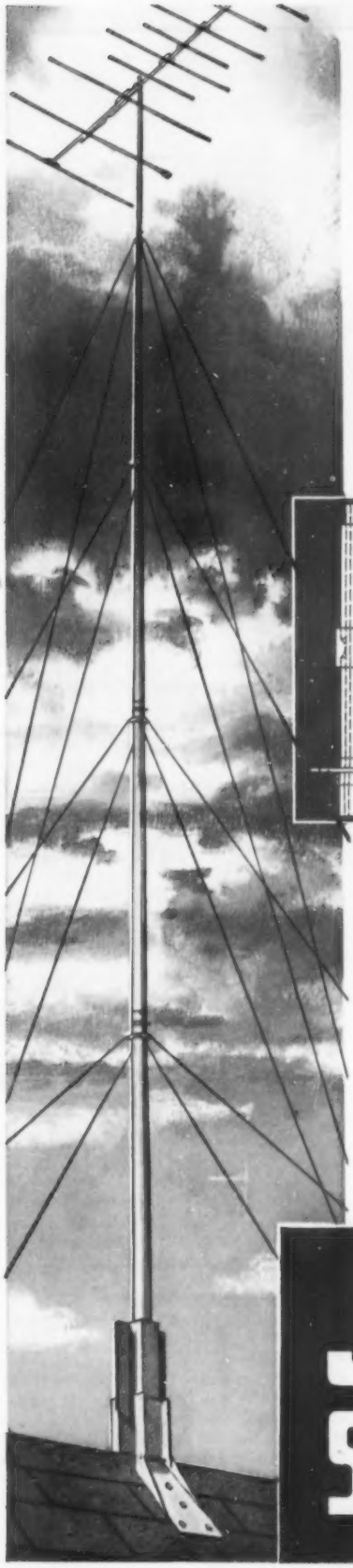



**Fig. 3—Power gain of the paraboloid.**

## Jodrell Bank radiotelescope

This large antenna or radiotelescope has a circular paraboloidal mirror 218 feet in diameter. Fig. 2 shows a cross-section of the antenna. The reflecting surface is fixed to the ground with its axis vertical and is supported by a steel ring and three concentric circles of steel posts mounted in concrete blocks. The posts support a web of steel cables which form the outline of a paraboloid. Since the cables run in straight lines



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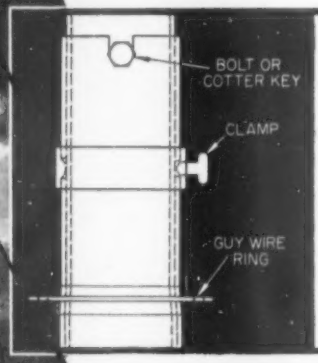


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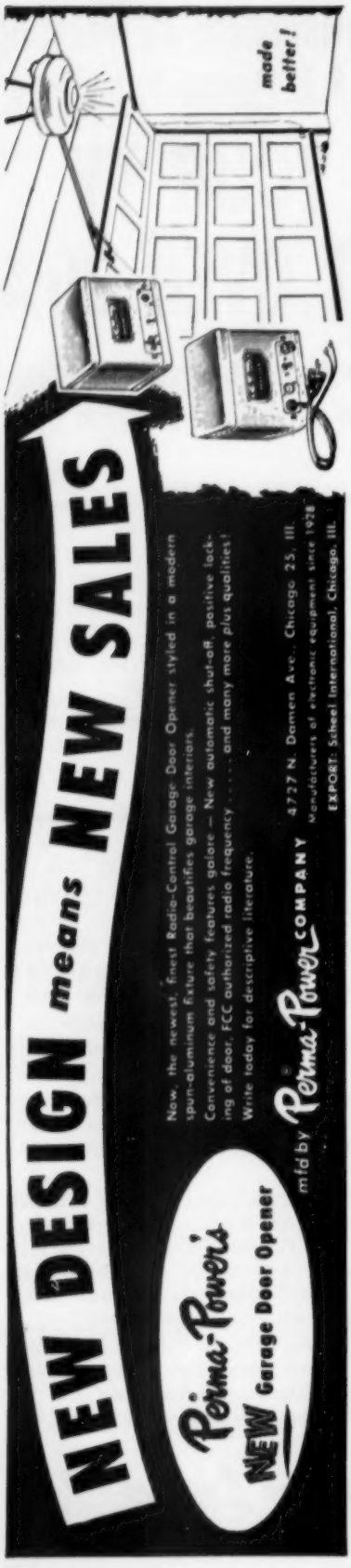
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between the poles, the outline of the web is not truly paraboloidal but is an approximation to the correct shape made up of short straight lines.

The actual reflecting surface of the mirror is laid on the steel cables and is formed by a grid of galvanized iron wires parallel to each other and running across the mirror in curves which follow the direction of current flow in the surface. The spacing between adjacent wires in the grid is 8 inches, and the deviation of the reflecting surface from a true paraboloidal shape is nowhere greater than 5 inches. Since the mirror surface is made up of wires running in only one direction and is not a true mesh, it reflects best the component of waves polarized in an east–west direction and is almost transparent to waves polarized in the north–south plane.

The focal length of the mirror is 126 feet, and the reflected energy is collected at the focus by a small antenna system known as the "primary feed." This consists of two half-wave dipoles and their reflectors arranged to have a

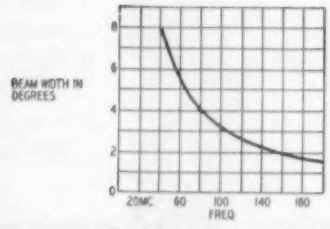


**Fig. 4—Bandwidth of the paraboloid.**

polar diagram suitable for the reception of energy reflected by the mirror. The primary feed is supported at a height of 126 feet above the center of the mirror by a sectional steel mast guyed by three sets of steel ropes spaced round the mast at intervals of 120°. The base of the mast is supported on a horizontal axle running east–west. By adjusting the length of the supporting guys, the mast can be tilted to 15° north or south of the vertical. The energy received at the primary feed is carried down the mast in an air-spaced coaxial cable which runs to a receiving laboratory close to the rim of the mirror. The photo shows part of the mirror and the central mast carrying the primary feed antenna (which at the time of the photograph was tilted).

The power gain of the antenna is very large. It is shown in Fig. 3, plotted against frequency. The full line shows the theoretical gain calculated on the assumption that the mirror is a perfect paraboloid with a 100%-efficient reflecting surface. The broken line shows the gain after allowing for errors in the shape of the paraboloid and for the loss of energy through the reflecting grid of wires. As the frequency increases, more and more of the energy falling on the mirror passes straight through the mirror surface and is lost. For example, at 75 mc efficiency is about 90%, at 160 mc it has fallen to 70% and at 300 mc the mirror would be almost transparent. The highest frequency which can be used is governed by this factor and is limited to about 200 mc.

The beamwidth of the instrument varies inversely as the frequency (Fig. 4). At 160 mc it is 2° between points of half-power (3 db down from maximum gain). The shape of the beam has been measured at 75 mc using a transmitter carried in an aircraft and also at 160 mc by observations of a radio star. Fig. 5 shows the beam shape measured at 160 mc.

Since the mirror is fixed to the ground with its axis vertical, the beam will normally be directed straight upward. As the earth rotates, it will scan a strip of sky equal in width to the beam. To scan a different strip of sky the beam must be tilted. The only available method of moving it is to displace the primary feed by tilting the central tower. If the primary feed of a circular paraboloid is tilted by an angle $\theta$, then the beam will move in the opposite direction by an angle $\phi$, where $\theta = K\phi$. The value of K depends mainly on the ratio of the focal length to the diameter of the mirror; for the 218-foot mirror K = 0.915. Thus by tilting the central mast to 15° from the vertical, the beam can be swung about 12½°.

If the beam of an antenna is swung too far by displacing the primary feed from the axis, its shape will be seriously distorted. The principal feature of

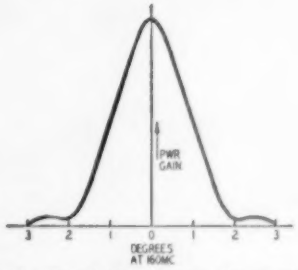


**Fig. 5—Paraboloid beam shape at 160 mc.**

the distorted shape is the appearance of a subsidiary lobe which corresponds to the "coma" distortion in optical instruments. Experience shows that the beam of the big paraboloid can be swung to at least six times its own width (i.e., about 12° at 160 mc), without serious distortion.

## The receiving equipment

The radio astronomer is usually concerned with the detection of extremely weak signals. Thus in the u.h.f. band the power received from an average radio star is well below the noise power of the best receiver even when used with the big paraboloid. Thus, one of the main problems in designing the receiving equipment is to maintain the gain of the receiver constant so that minute variations in the received power may be recorded. In the present equipment this problem has been solved by

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## ELECTRONICS

the use of a "servo" type receiver (Fig. 6). The "signal," which from a radio star resembles thermal noise, is fed through an adjustable matching unit to a rotating capacitance switch. This switch revolves at 1,200 r.p.m. and connects the input of the receiver alternately to the antenna and to a noise generator. The rectified output from the receiver is fed to a low-frequency amplifier tuned to the switch rotation frequency (20 cycles), which in turn feeds a phase-sensitive (synchronous) detector. If there is any difference between the power output from the antenna and the output from the noise generator as the switch rotates, the receiver output will vary at 20 cycles.

This 20-cycle component is amplified by a low-frequency amplifier and fed to a phase-sensitive detector. The detector is synchronized by a reference wave generated by a photocell in conjunction with a rotating shutter mounted on the shaft of the switch. It produces a positive or negative d.c. output according to the relative phase of the reference wave and the 20-cycle component in the receiver output. This output is used to increase or to decrease the noise power generated by the noise generator.

The polarity of the circuit is arranged so that the d.c output from the phase-sensitive detector controls the output from the noise source so that the power received at the input of the receiver in both positions of the switch is equal. Thus the whole equipment forms a servo loop which controls the output of the noise generator, making it closely equal to that from the antenna. The actual record of the variations in the antenna power is made by a recording milliammeter connected to the noise generator.

The function of the receiver is to detect any difference between the output of the antenna and the noise generator, and it thus acts like a null detector in the circuit of a bridge. Provided that the gain of the receiver remains high, small variations in this gain have little

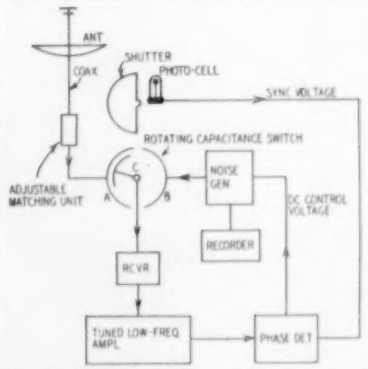


**Fig. 6—Block diagram of receiver used for detecting signals from radio stars.**

effect on the recorded value of the antenna output power.

The circuit of the rotating r.f. switch is shown in detail in Fig. 7. It consists

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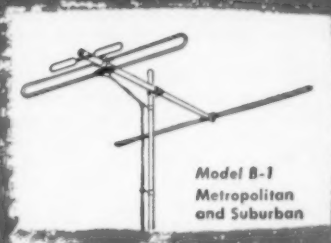

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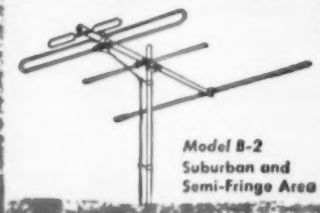

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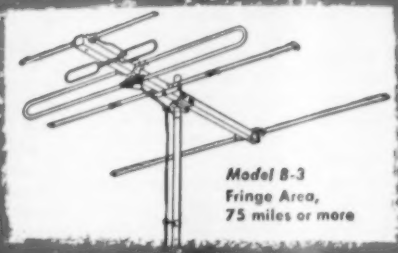

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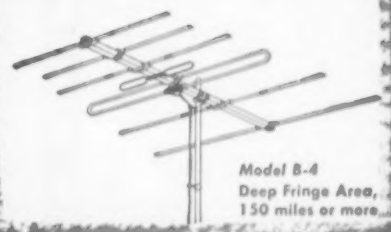

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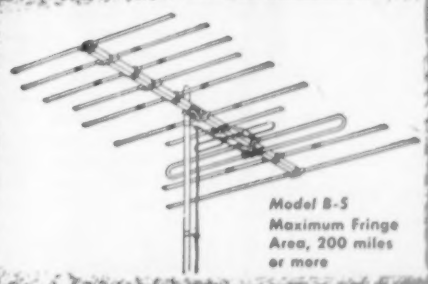

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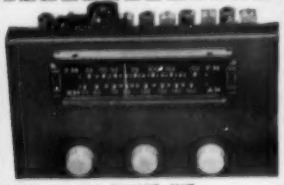

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Thus in the position of the switch

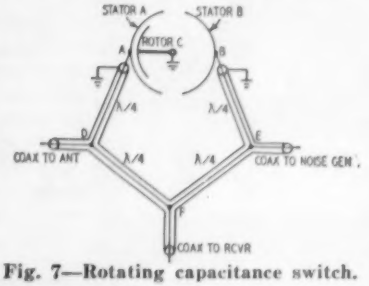


**Fig. 7—Rotating capacitance switch.**

shown in Fig. 7, the receiver is connected to the antenna and the noise generator is shut off. When the switch rotates so that the rotor engages the opposite set of stator plates, the whole cycle is reversed and the receiver is connected to the noise generator instead of to the antenna. The particular virtue of this type of switch is that it is completely noisefree since there are no rubbing contacts. Its performance can be judged from the following figures: at 160 mc with the switch on, the measured loss between either input terminal of the switch and the receiver input is less than 0.5 db, and with the switch off, the attenuation through the switch is greater than 20 db.

The receiver in use at the present time has five stages of r.f. amplification at 160 mc. The input stage uses a cascode circuit and consists of a type 6AK5 pentode connected as a neutralized triode and followed by four grounded-grid triode amplifiers. These r.f. stages feed a diode mixer and a 30-mc i.f. amplifier of conventional design. The local oscillator works at 130 mc and is crystal-controlled. The overall bandwidth of the receiver is 1 mc and the noise factor is 5.5 db. The selective low-frequency amplifier is tuned to 20 cycles by a "twin-tee" bridge feedback circuit. The phase-sensitive detector is of conventional design and uses a ring of four germanium crystal diodes.

The circuit of the noise generator is shown in Fig. 8. It contains a tungsten-filament diode (British type CV172) connected across a 72-ohm resistor. The diode is operated at a plate voltage of 120 so that the plate current is limited

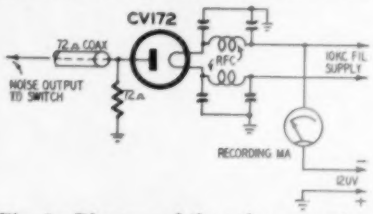


**Fig. 8—Diagram of the noise generator.**

only by the temperature of the filament and not by space charge. Under these conditions the noise power generated by the shot noise across the load resistor can be calculated exactly and is directly proportional to the plate current.

The plate current of the diode, and hence the noise power output, is controlled by varying the filament voltage which is supplied at 10 kc. (A frequency of 10 kc is used to avoid supply frequency modulation of the noise output by variations in the temperature of the filament whose thermal time constant is very short.) The 10-kc supply is generated by a triode-hexode whose output is controlled by applying the d.c. voltage from the phase-sensitive detector to one of the hexode grids.

All the heater and plate supplies to the equipment are stabilized. The heater supplies are from storage batteries floated across the output of a constant-current charger. The plate supplies are from high-gain regulated packs which stabilize the a.c. power line by a factor of 2,000 times.

In operation, the equipment has proved to be extremely stable and sensitive. When operating at full gain, the recording pen draws a wavy line (Fig. 9). The small ripples in this line correspond to the basic noise in the receiver itself after it has been smoothed by the time constant of the circuits after the receiver. This time constant is adjusted by a simple resistor and capacitor across the output of the phase-sensitive detector and is usually set so that the whole servo loop has a time constant of about 10 seconds. The minimum power which the equipment can detect must produce a deflection of the recording pen at least equal to the small ripples on the record due to the receiver noise. It can be shown that this value of receiver noise power is given roughly by the formula:

$$\text{MDP} = \text{NP} \times \sqrt{\frac{1}{\text{TC} \times \text{r.f. bandwidth}}}$$

where MDP, NP and TC are abbreviations for minimum detectable power, noise power and time constant, respectively.

Thus for an r.f. bandwidth of 1 mc and a time constant of 10 seconds the minimum detectable power is about 1/3,000 of the receiver noise. This corresponds to a signal power 35 db below receiver noise and to a power at the receiver input of $5 \times 10^{-15}$ watts.

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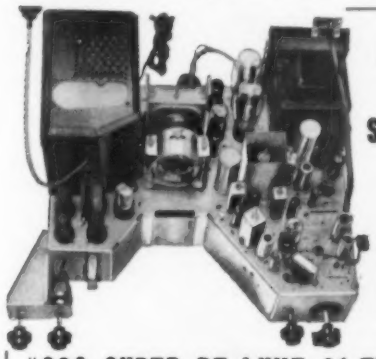

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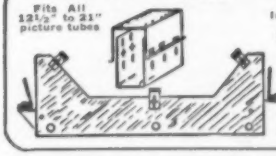

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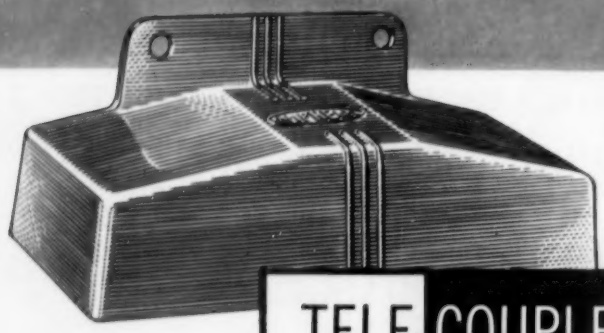

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of course, gained at the expense of the effective bandwidth. Thus, although the present equipment has an r.f. bandwidth of 1 mc, the time constant of the circuits after the receiver restrict the low-frequency bandwidth to about 0.1 cycle. Thus, the equipment cannot follow any modulation or change in the received power which occurs in a time short compared with 10 seconds. For most work with the paraboloid this response time is satisfactory since a radio star takes about 15 minutes to pass through the aerial beam. If more rapid observations are required, the response time can be decreased at the expense of the sensitivity.

### Results

During the past four years the big paraboloid and its receiving equipment have been operated at 160 mc and used to survey the strip of sky (about 25° wide) which lies within its field of view. The survey was made by fixing the central mast at some selected angle and recording the intensity of the power received by the antenna over a period of at least 24 hours. When a satisfactory record or series of records had been obtained the mast was moved to a different angle and the observations repeated. This process was continued until the whole of the strip of sky had been covered.

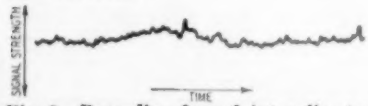


**Fig. 9—Recording from faint radio star.**

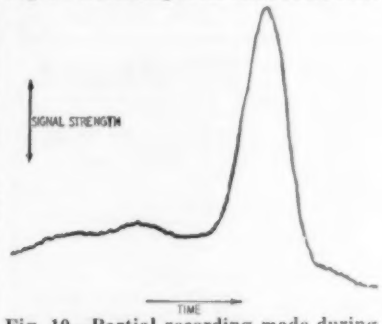


**Fig. 10—Partial recording made during passage of Cygnus through aerial beam.**

The results have been used to draw a contour map of the intensity of the radio waves from the strip. The map confirms that the bulk of the radio energy comes from the Milky Way and it also shows, superimposed on the diffuse background of radiation, a number of localized sources of radio waves which are the so-called radio stars. It happens, by a fortunate coincidence, that the two brightest radio stars in the whole sky lie in the field of view of the paraboloid. The brightest is in the constellation of Cassiopeia. The second brightest is in the Swan (Cygnus).

Fig. 10 shows a section of chart recorded during the passage of Cygnus through the aerial beam. The large peak in the center of the record cor-

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- 6AB4 oscillator • 6AU6 1st I.F. amplifier
- 6AU6 2nd I.F. amplifier • 6AU6 1st limiter
- 6AU6 2nd limiter • 6AL5 detector
- 6C4 cathode follower output • AM tuning range 530-1650 kc • Frequency response AM-20-7,500 CPS ± 3DB
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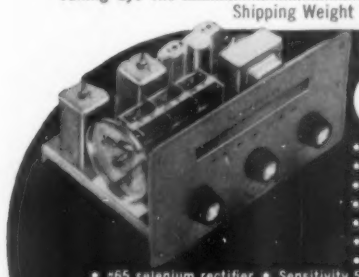

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- 6AU6 2nd I.F. amplifier
- 6AU6 1st limiter
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- 6AL5 detector
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responds to the power from Cygnus and the shape of the peak represents the polar diagram of the antenna. The general rise of the curve toward the left of the diagram is because, directly after the transit of Cygnus, the beam crossed the Milky Way, giving the picture an asymmetrical appearance. The intensity of the radiation can be found by a simple measurement of the height of the peak.

Cassiopeia and Cygnus can be received easily with the big paraboloid and the record in Fig. 10 shows little trace of receiver noise. In fact, the equipment was operating at a reduced gain. The power flux from the stronger of the two radio stars (Cassiopeia) has been measured and found to be $9 \times 10^{-25}$ watts per square meter of earth's surface per cycle of bandwidth.

The power received by any antenna and receiver can be found by multiplying this figure by the effective collecting area of the antenna in square meters and by the bandwidth of the receiver in cycles. The value of power flux given is for 160 mc and the few experiments which have been done suggest that the power flux varies almost inversely with the frequency. The radiation from these radio stars appears to be constant in intensity and unpolarized.

The majority of the radio stars are much fainter than the two mentioned above. Fig. 9 shows a record of a very faint radio star (160 times weaker than Cassiopeia) which has been identified with the Great Spiral Nebula in Andromeda. This nebula is called by astronomers a "galaxy" and is a system of stars containing perhaps $10^{11}$ (100,000,000,000) stars at a distance from us of about 1,000,000 light years. The detection by radio of this nebula was made with the big paraboloid and showed conclusively that radio waves are generated in other star systems besides our own Milky Way.

What are radio stars? So far there is no satisfactory answer to this question. Some of them, such as that corresponding to the Great Spiral Nebula in Andromeda, are known to be caused by the emission of radio waves from distant galaxies. But the mechanism responsible for this emission and for the radio stars in our own Milky Way remains a mystery. It is known that the radio stars are not associated with any common type of visible star. In fact, the only star which has been identified as a source of radio waves is our sun. Furthermore, searches with telescopes have so far revealed that in the majority of cases no visible object can be associated with a radio star. This search must be extended and requires that the celestial coordinates of the radio stars should be measured more precisely and that many more radio stars should be detected. Both these requirements present a challenge to the new science of radio-astronomy and ensure that all the available radiotelescopes will be busy for a long time to come. END

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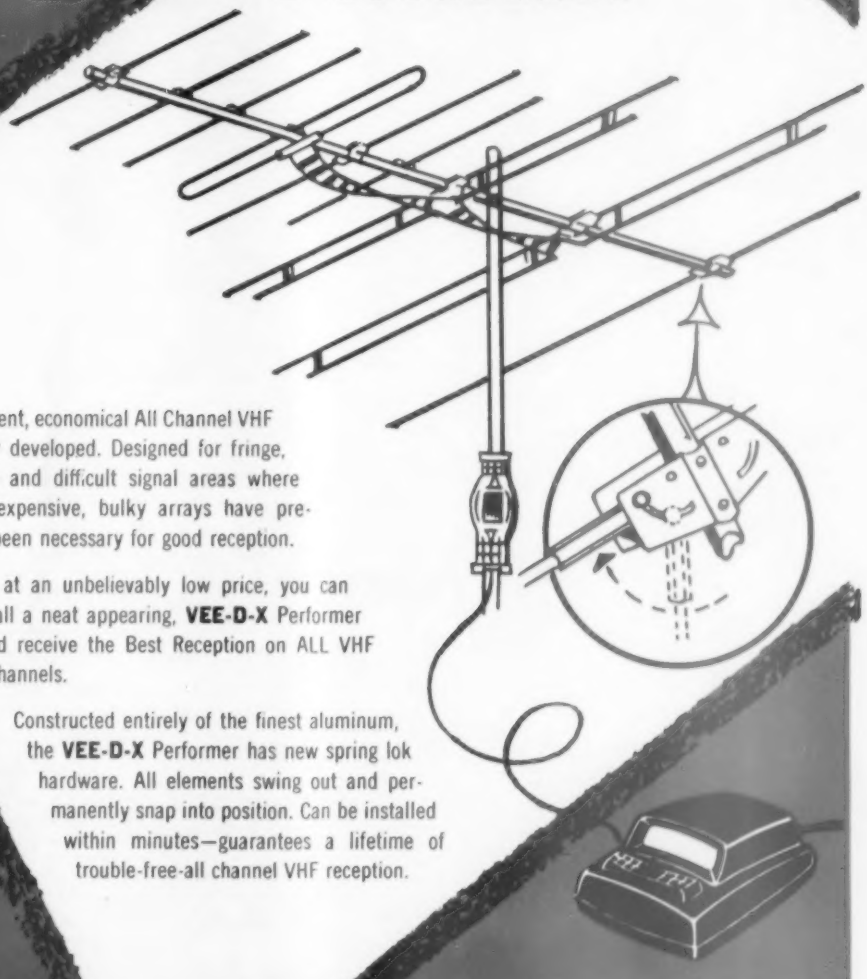

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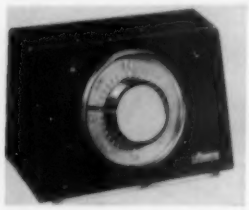

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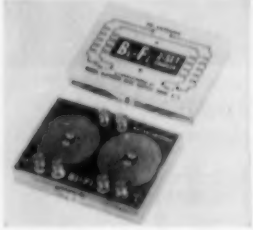

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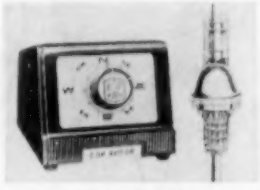

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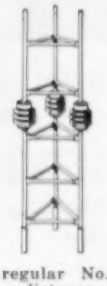

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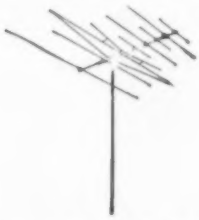
Individual insulators rated 7.5 kv; wet flashover voltage 40 kv.—**Rohn Manufacturing Co.**, 116 Limestone, Bellevue, Peoria, Ill.

**GLOBE-TENNA,** *Telco Electronics Mfg. Co.*, indoor v.h.f.–u.h.f. TV antenna in form of 12-inch globe with full-color

map. Bright brass base. Rotates to any position for best reception. 3-way connector on lead-in for connecting to all TV sets.—**Telco Electronics Mfg. Co. (Div. of General Cement Mfg. Co.)**, 919 No. Wells St., Chicago 6, Ill.

**FRINGE-AREA ANTENNA,** *Pixie*, for weak-signal TV reception. Sharp directivity, unilobe pattern on v.h.f. channels, high front-to-back ratio, high

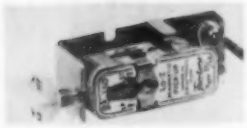


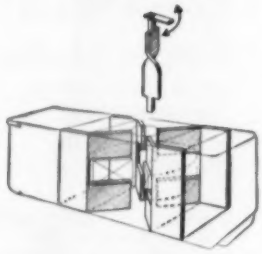
uniform gain, very high signal-to-noise ratio. Aluminum and stainless steel construction, preassembled.—**Winegard Co.**, 3000 Scotten Blvd., Burlington, Iowa.

**LOUDSPEAKER SYSTEM,** *Patrician IV*, high-fidelity 4-way unit minimizes intermodulation and transient distortion. Three

controls permit balance to room acoustics.—**Electro-Voice, Inc.**, Buchanan, Mich.

**PHONO CARTRIDGE,** *Fen-tone B & O Lo-Z*, 8-pole magnetic type of Danish manufacture. Frequency range flat ±2 db 20–16,000 cycles, then rises gradually to over 20,000 cycles.





Tracking force: microgroove, 5–7 grams; 78 r.p.m., 9–12 grams. Equivalent stylus mass 4.5 milligrams for dual and 3.5 mg for single stylus. Output voltage 30 mv at 4.4 cm/sec; d.c. resistance to 530 ohms. Cartridge weight about 14 grams. No optimum load necessary; any resistance greater than 1,000 ohms suitable.—**Fenton Co.**, 15 Moore St., New York 4, N. Y.

**2-STATION INTERCOM,** *RMS Double Talk model DT-100*, in mahogany Bakelite cabinets. Master has 4-inch PM speaker, 12AT6 voltage amplifier, 50C5

power amplifier with 1.8 watts output, 35W4 rectifier, volume control, press-to-talk and on-off switches. Switch on remote can be locked in talk position for baby sitting and similar applications. Third station with pushbutton selector switch optional. Similar unit, *model DTI-100*, in ivory cabinets.—**Radio Merchandise Sales Inc.**, 2016 Bronxdale Ave., New York 62, N. Y.

**TRANSCRIPTION TURNTABLE,** *Collaro 2010*, 4-pole, dynamically balanced, hum-shielded induction motor. 33⅓, 45, 78 r.p.m. Motor shock-mounted. Nonmagnetic turntable cast and machined; weighs 8½ lb.; most weight in rim for added flywheel effect; covered with rubber mat. Low-mass, nonresonant arm houses crystal cartridge with 2 mechanically isolated sapphire turnover styli. Response smooth 40 to beyond

16,000 cycles. *Model 2010* accommodates discs to 16 inches.—**Rockbar Corp.**, 215 E. 37 St., New York 16, N. Y.

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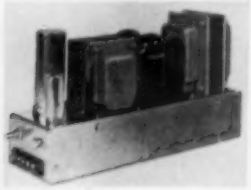
EXPORT DEPT. 270 BROADWAY, N. Y. 13, N. Y.

**14-WATT AMPLIFIER,** *Sargent-Rayment SR-14B,* uses Ultra-Linear circuitry for high output with low distortion. Harmonic distortion 0.2% at 10 watts, less than 1% at 14 watts; IM distortion 0.8% (40



and 12,000 cycles mixed 4:1). Hum and noise better than 86 db below rated output; sensitivity 0.85-volt input for 10-watt output. Output does not rise more than 0.3 db between full load and no load. Output impedances: 4, 8, 16 ohms. 12½ x 4 x 6¼ inches. Tubes: 12AU7, 6C4, 5Y3 and two 6L6-GB's. Power consumption 90 watts from 110-120-volt 50-60-cycle line. — **Sargent-Rayment Co.,** 1401 Middle Harbor Rd., Oakland 20, Calif.

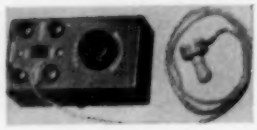
**MIDGET MICROPHONES,** *Shure,* for applications where small size and low weight are important. Available in controlled-reluctance types. New *series MC* furnished in 1-inch

round and rectangular shapes. They are designed for manufacturers of original equipment, but available also to service technicians and laboratories.—**Shure Brothers,** 225 W. Huron St., Chicago 10, Ill.

**7½-INCH SCALE V.T.V.M.,** *Precise Development model 9071,* available as kit or factory-wired. VR tube for voltage regulation. 5 voltage ranges: 5, 25, 250, 500 and 1,000; +d.c.,

—d.c. and a.c. (separate 5-volt a.c. scale). 5 resistance ranges from 0.2 ohm to 1 billion ohms. Decibels from −20 to +55. True zero-center scale for aligning FM and TV discriminators. 25-megohm input impedance on d.c. Weighs 11 lb. —**Precise Development Corp.,** Oceanside, N. Y.

**REMOTE TV LISTENER,** *Lafayette Silent Viewer Model MS 125,* permits listening without disturbing others. Also excellent for hard-of-hearing persons, who can adjust volume level to their needs. On-off switch, volume control and jacks

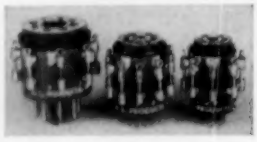


for 2 headphones. Provided with 20-foot cable. Supplied with one pair of headphones; additional pair available at extra cost. **Lafeyette Radio,** Dept. J., 100 6th Ave., New York, N. Y.

**TV AMPLIFIERS,** *Transvision,* 8 models for master antenna installations and for repeater and distribution service in community systems. Broadband distribution amplifiers and repeaters with choice of

low band only, high band only or full coverage of channels 2 to 13 with built-in cable-loss equalizers. Dual outputs are provided for systems requiring more than one main line.— **Transvision Inc.,** 460 North Ave., New Rochelle, N. Y.

**TUBE ADADPTERS,** *Adapter,* inserted in vacuum-tube socket, become integral part of circuit. Test points for voltage, resistance measurements. Removing rod breaks circuit, allowing component or meter insertion. Color-coded terminals; com-



pact; no soldering.—**A L Products,** Kearny, N. J.

**CAPACITORS,** *Astron Series X* high-voltage types. Operate up to 150°C without derating, up to 200°C with proper derating and adjustment, as well as from —65° without derating. Characteristics due to combination of Mylar and other dielectric materials including a solid polyester impregnant. Available in wide range of hermetically sealed tubular, metal and bathtub cases with glass-to-metal closure. Excellent radio-frequency

and retrace characteristics.— **Astron Corp.,** 255 Grant Ave., East Newark, N. J.

**CONNECTORS,** printed-circuit applications. 10, 18, 22, 28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## WHAT THE "EDU-KIT" OFFERS YOU

Our Kit is designed to provide a fundamental background in radio, with the basic facts of Radio Theory and Construction Practice expressed simply and clearly. You will gain a knowledge of basic Radio Principles involved in Radio Reception, Radio Transmission and Audio Amplification.

You will learn how to identify Radio Symbols and Diagrams; how to build radios, using regular radio circuit schematics; how to mount various radio parts; how to wire and solder in a professional manner. You will learn proper chassis layout. You will learn how to service and trouble-shoot radios. You will learn code. You will receive training for F.C.C. Novice License. You will learn High Fidelity.

In brief, you will receive a practical basic education in Radio, worth many times the small price you pay.

## THE KIT FOR EVERYONE

The Progressive Radio "Edu-Kit" was specifically prepared for any person who has a desire to learn Radio. The Kit has been used successfully by young and old in all parts of the world. It is not necessary that you have even the slightest background in science or radio.

The Progressive Radio "Edu-Kit" is used by many Radio Schools and Clubs in this country and abroad. It is used by Armed Forces Personnel and Veterans throughout the world.

The Progressive Radio "Edu-Kit" requires no instructor. All instructions are included. All parts are individually boxed, and identified by name, illustration and diagram. Every step involved in building these sets is carefully explained.

## PROGRESSIVE TEACHING METHOD

The Progressive Radio "Edu-Kit" comes complete with instructions. These instructions are arranged in a clear, simple and progressive manner. The theory of Radio Transmission, Radio Reception, Audio Amplification and servicing by Signal Tracing is clearly explained. Every part is identified by illustration and diagram. You will learn the function and theory of every part used.

The Progressive Radio "Edu-Kit" uses the principle of "Learn by Doing". Therefore you will build radio circuits, perform jobs, and conduct experiments to illustrate the principles which you learn. These circuits are designed in a modern manner, according to the best principles of present-day educational practice. You begin by building a simple radio. The next set that you build is slightly more advanced. Gradually, in a progressive manner, you will find yourself constructing still more advanced multi-tube radio circuits and doing work like a professional Radio Technician. You will build Receiver, Transmitter, Code Oscillator and Signal Tracer Circuits—15 in all. These sets operate on 105-125 V. AC/DC. For use in Foreign Countries having 210-250 Volt Source, an Adaptor for 210-250 V. AC/DC operation is available.

## THE PROGRESSIVE RADIO "EDU-KIT" IS COMPLETE

You will receive every part necessary to build 15 different radio circuits. The "Edu-Kit" contains tubes, tube sockets, variable, electrolytic, and paper condensers, resistors, tie strips, coils, hardware, tubing, instruction manuals, etc. No wire or solder included.

Every part that you need is included. These parts are individually packaged, so that you can easily identify every item. A soldering iron is included, as well as an Electrical and Radio Tester. Complete, easy-to-follow instructions are provided. All parts are guaranteed, brand new, carefully selected and matched.

In addition, the "Edu-Kit" now contains lessons for servicing with the Progressive Signal Tracer, F.C.C. instructions, quizzes, High Fidelity instructions.

## TROUBLE-SHOOTING LESSONS

Trouble-shooting and servicing are included. You will learn how to recognize and repair troubles. You will build and learn to operate a professional Signal Tracer. You receive an Electrical and Radio Tester, and learn to use it for radio repairs. While you are learning in this practical way, you will be able to do many a repair job for your neighbors and friends, and charge fees which will far exceed the small cost of the "Edu-Kit". Here is your opportunity to learn radio quickly and easily, and have others pay for it.

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or 44 gold-plated phosphor-bronze or beryllium contacts. Current rating, 5 amp. Polarized by deleting one or more contacts.—**Cannon Electric Co.**, P. O. Box 75, Lincoln Heights Station, Los Angeles 31, Calif.

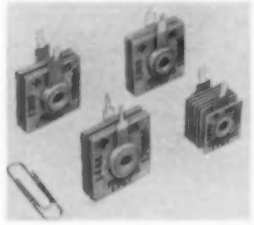
**PLUG-IN TUBULARS,** *type BC*, phenolic-cased paper units, printed-circuit applications. Two parallel-lead wire terminals brought out from end of

capacitor, spaced fixed distance, plugged directly into printed circuits and dip-soldered.—**Cornell-Dubilier Electric Corp.**, South Plainfield, N. J.

**TUNER CLEANER,** *Electronic Chemical Tuner-Tonic* for cleaning, lubricating, restoring old tuners, including wafer types. Nontoxic and nonflammable,

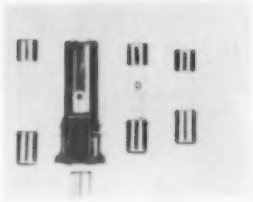
will not harm insulation or precious metals, nor attack plastics. Does not affect capacitance, inductance or resistance of components. — **Electronic Chemical Corp.**, 813 Communipaw Ave., Jersey City, N. J.

**SELENIUM RECTIFIERS,** *Federal Telephone & Radio*. 3 terminal types: square-tipped for printed-circuit boards up to 1/16-inch thick; tapered for boards up to ⅛ inch; snap-in for places where board is sub-



ject to vibration or may be inverted before soldering. Ratings up to 150 ma and for line inputs up to 175 volts a.c.—**Components Division, Federal Telephone & Radio Co.**, 100 Kingsland Road, Clifton, N. J.

**FUSE HOLDERS,** *Littelfuse LC*, accept only correct size Littelfuse LC fuses. Different lengths of fuses and different widths of bayonet locking tabs make insertion of wrong LC fuses



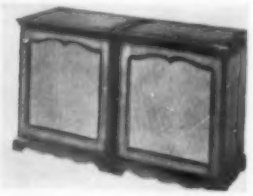
impossible. For example, 1-amp. fuse is 1.25 inches long with 0.115 to 0.120 width tabs. Its holder accepts only slo-blo fuses between ¾ and 1¼ amp. LC fuses not replaceable with regular types.—**Littelfuse, Inc.**, 1865 Miner St., Des Plaines, Ill.

**STURDY CAPACITORS,** *Pyramid Glasseal* types, withstand severe mechanical shock, vibrations and stresses of high acceleration. Solid dielectric type. Compression type glass-to-metal solder-seal terminals

will not rotate nor work loose under any operating conditions. Capacitor values from .001 to 1.0 μf with d.c. voltage ranges of 100 to 600. Both inserted tab and extended foil.—**Pyramid Electric Co.**, 1445 Hudson Blvd., North Bergen, N. J.

**MICROPHONES,** *American Microphone Co.*, for use with tape recorders. Low-cost, high-quality units are small (3¼ x 2⅛ x 1⅜ inch) and light (2 ounces). Crystal type has response 100–7,000 cycles, output −55 db. Ceramic type has response 100–6,000, output −62 db. Omnidirectional.—**American Microphone Co.**, 370 South Fair Oaks Ave., Pasadena, Calif.

**MATCHING CABINETS,** *Standard Wood Products*, for speaker and audio equipment stand together or apart as desired. High-grade ¾-inch select-grain stock; authentically styled, carefully hand-rubbed. *Model 200A* acoustic cabinet T-braced, Kimsul-padded, vented for smooth low-frequency response



down to 30 cycles. *200E* equipment cabinet; universal mounting arrangement to accommodate any combination of electronic equipment; open design for ventilation and convection cooling. In fruitwood or mahogany.—**Standard Wood Products**, 47 W. 63d St., New York 23, N. Y. END

**All specifications given on these pages are from manufacturers' data.**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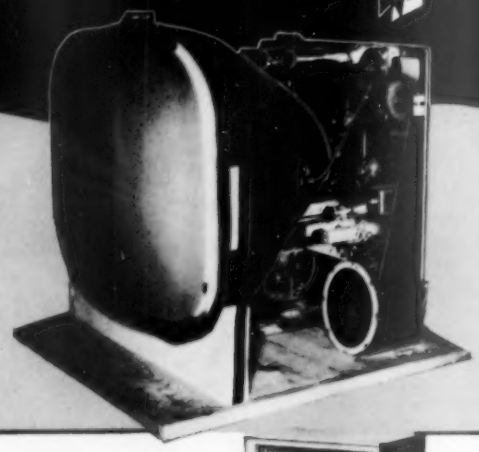


**SPECIAL FOR SEPTEMBER!**

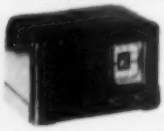
**Arkay Model 14T21 Advanced design T. V. Kit Featuring — Modern Vertical Chassis construction; transformerless operation; turret type tuner (Factory wired and tested); Full 14kv, electrostatically focused 21" picture tube operation; field tested circuitry of latest design and innovation for stable, clear, trouble free reception under all conditions; excellent fringe area performance. A first rate Kit anyone can easily assemble at a low price anyone can afford.** $70.50

**Arkay FL-10 High Fidelity Amplifier Pre-Amp Kit;** Unity coupled pushpull 12 watt output; frequency response ±2db 20-20,000 cps with extremely low IM and Harmonic distortion; 5 position input selector with record equalizer; loudness, bass, and trebie controls; tapped output; extremely low noise level; completely enclosed—no cabinet problem; for clean, flexible, brilliant audio. $28.95

**Arkay Model 65X 2 Band AC/DC Radio receiver Kit.** Broadcast 550-1700kc and short wave 6-18mc bands; superheterodyne circuit of modern design; special tone chamber for utmost realism in listening; magic glow lucite dial actuated by pilot light when set turned on; a smart functional set. $19.95

**Arkay Model T82X — 2 band Battery operated Portable Radio Kit;** receives broadcast band 550-1700kc plus short wave band 6-18mc; superheterodyne circuit operated from a long life (1000 hour) battery pack; handsome cabinet with slide rule dial; low battery drain miniature tubes throughout. $19.95

**Arkay Model 55K superheterodyne receiver Kit;** designed especially for the beginner — educational as well as functional; 5 tube AC/DC radio with built in loop antenna and plastic cabinet, as in all Arkay Kits, contains detailed manual with exclusive 3D Eye-O-Gram technique for simple assembly. $14.95

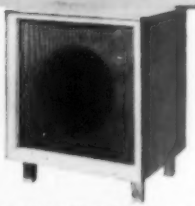


**Arkay 2X4 3-way 2 band portable receiver Kit.** Foreign Band of 6-18mc; broadcast band 550-1600kc; excellent for beach or camping; indoors or out; foreign stations marked on semi-airplane dial; housed in handsome leatherette cabinet; superheterodyne circuit with low battery drain tubes. $24.95

**Arkay 3W10P 3-way portable receiver Kit.** 4 low battery-drain miniature tubes in an efficient superheterodyne circuit of extreme sensitivity; AC, DC, and battery operation for utmost convenience; selenium rectifier for instantaneous operation on AC or DC; 2 tone attractive plastic cabinet; built in loop antenna. $18.95

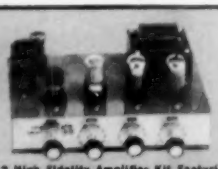
**Arkay Model P120 3 Band Radio Receiver Kit.** Frequency range 550kc-18mc in 3 bands; police, fire, amateur and foreign stations; slide rule dial; special tone control and phono switch on front cabinet; 6" speaker; quality throughout; latest transformerless design. $25.75

**Arkay Model 10-1 Electronic Experimenters Kit.** 10 projects to construct include, a broadcast receiver, audio amplifier, phono oscillator, code practice oscillator, home broadcast station, capacity relay, photo cell relay, signal tracer, electronic timer, electronic switch; learn circuitry the practical way. $13.95



**Arkay Model B12 Baffle Kit.** Infinite impedance type for 12" speaker maximum size; cabinet is exact replica of very expensive commercial sound chamber giving excellent full frequency sound response; enclosure is acoustically tuned; this unit is attractive and is mounted on Hollywood legs; assembled by anyone with hammer and nails; easily finished. $11.95

**SPECIALS FOR SEPTEMBER!**



**Arkay A-12 High Fidelity Amplifier Kit Featuring** — 12 watt output-push pull 6V6's; frequency response ±1db 20-20,000 cps with low distortion; 5 inputs, master controlled at front panel; tapped output transformer; separate bass and treble control, each with maximum db boost and cut; built-in Pre-Amplifier; ideal for home installations. $22.95

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# new Tubes & Transistors

Sylvania has announced three new 21-inch, aluminized, electrostatic-focus, glass, rectangular picture tubes rated for 20-kv operation. The 21ALP4A/B, 21AUP4A/B and 21AVP4A/B have been produced in line with the higher operating voltages required for greater contrast and brighter television pictures. Other than the 20-kv high-voltage rating, the tubes meet all specifications previously registered with the 18-kv tube types (no B designation).

The 21ALP4A/B has a 90° deflection angle and an outer conductive coating which when grounded forms a 500–750-$\mu\mu$f capacitor with the inner coating. The 21AUP4A/B has a deflection angle of 72° and forms a capacitor of 500–750 $\mu\mu$f. The 21AVP4A/B has a deflection angle of 72° and forms a capacitor of 1,200–1,500 $\mu\mu$f.

### 4BC8

A miniature twin-triode, the 4BC8, has been announced by Sylvania. It is a miniature medium-mu semiremote cutoff twin triode, for use in sets with controlled-warmup 600-ma series heater strings. Except for its heater ratings (4.2 volts, 600 ma) it is identical to the 6BC8 described in the May issue. It is intended for use as a v.h.f. cascode amplifier, functioning very effectively in a.g.c. circuits and minimizing cross-modulation under both strong- and weak-signal conditions.

### 3D22-A

An improved version of the 3D22 featuring a greatly strengthened mount structure has been announced by RCA. The tube is a sensitive, four-electrode, xenon thyratron for use in relay and grid-controlled rectifier applications, particularly those involving motor-control service.

Like the 3D22, the 3D22-A has a negative-control characteristic essentially independent of ambient temperature over an operating range of −75 to +90° C. It also has small preconduction currents, low control-grid-to-anode capacitance and low control-grid current.

When used for d.c. voltage control, two 3D22-A's, in a full-wave circuit with a resistive load, are capable of handling up to 660 watts at a d.c. output voltage up to about 410. When used for a.c. voltage control, two 3D22-A's in a full-wave circuit are capable of handling up to 800 watts.

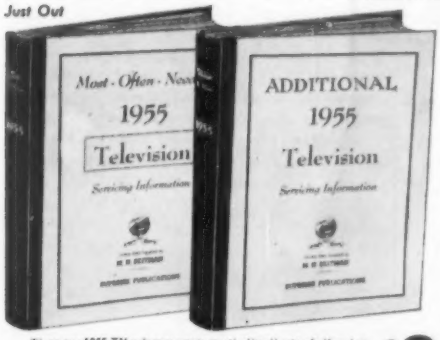
### 5R4-GYA, 6L6-GB

Straight-sided button-stem versions of two popular receiving type tubes have been announced by G-E. The 5R4-GYA has the same electrical characteristics as the 5R4-GY, but is ½ inch smaller in diameter. The 6L6-GB is about ¼ inch shorter and ¼ inch smaller in diameter than the 6L6-GA and a lot smaller than the 6L6-G. Electrical characteristics remain the same.

### Silicon diodes

Designed for extremely accurate voltage reference, four new types of silicon diodes have been announced by Texas Instruments. With reverse breakdown voltages (measured at 5 ma) ranging from 3.7 to 8, the silicon voltage reference diodes feature extremely small breakdown-voltage temperature coefficients from −55° to +150° C. This temperature coefficient, which can be positive or negative, is


Just Out

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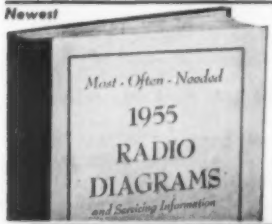


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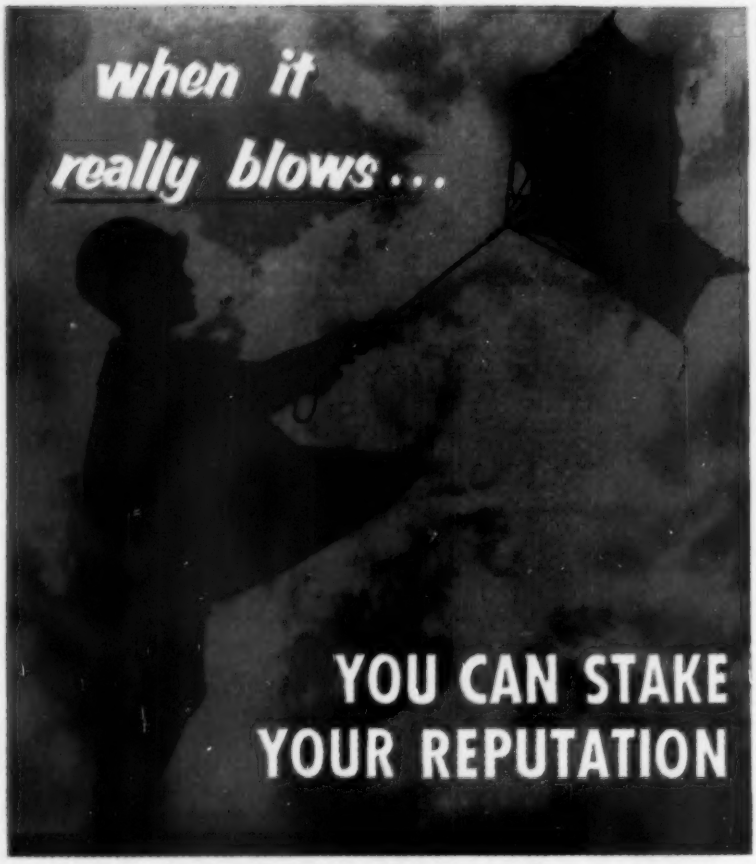


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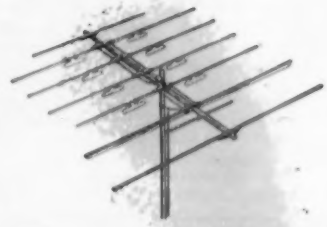

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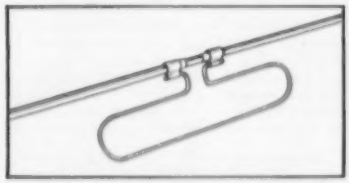

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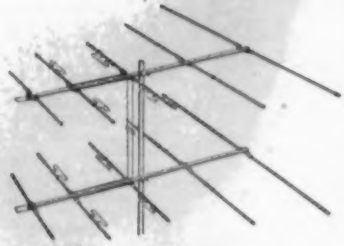

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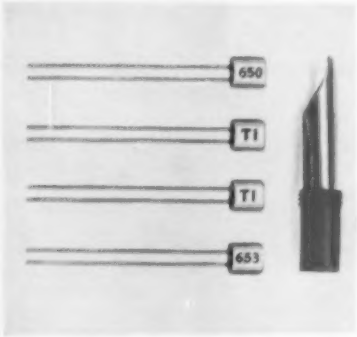
combined with very low dynamic resistance in the breakdown region to provide an ideal device for constant voltage reference purposes.

The diodes (see photo), types 650, 651, 652, 653, have a power dissipa-

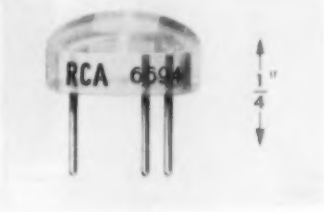



tion rating of 150 mw at 25° C and 40 mw at an ambient temperature of 150° C. Maximum average rectified forward current ranges from 90 to 125 ma at 25° C. Maximum reverse current is 0.1 μa at −1 volt at 25° C.

The new diodes are expected to have wide application wherever there is a need to stabilize accurate electronic circuits.

### 6694

Just released by RCA is a very tiny (see photo), cadmium-sulfide photoconductive cell of the head-on type. Designated as the 6694, this cell features high luminous sensitivity, very low dark current, extremely low background noise and signal output directly proportional to the incident light intensity. The characteristics are not substantially affected by wide changes




in operating temperature.

Because of its tiny size and high sensitivity, the 6694 is especially useful in light applications where a single tiny photosensitive device is desired—in light-controlled relays, computers and light meters for measuring the brightness of small luminous spots. It can also be used in X-ray intensity measurements.

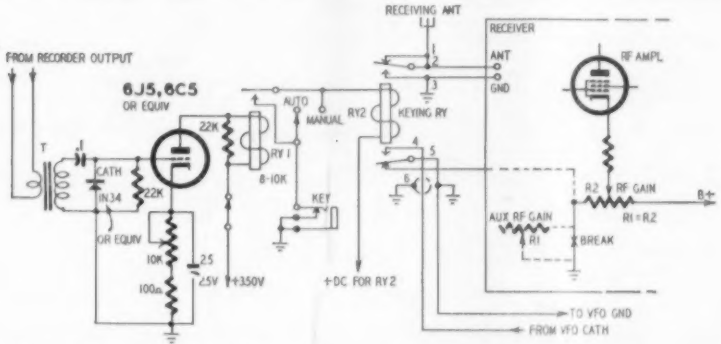
The spectral response of the 6694 covers the visible range from about 3,500 to 5,500 angstroms, maximum response occurring at about 5,000.

The frequency response of the 6694 falls off with increase in frequency. Its upper limit is about 500 cycles. A wider response is obtained with high light levels than with low. END

# radio-electronic Circuits

## AUTOMATIC CW KEYER

Hours before a week-end WAS or WAZ contest or sweepstakes is over the average CW operator is pretty tired of pounding the key. This is particularly true when he sends a lot of long directional CQ's. This type of operating can be much less tiring if you follow the lead of G2NS and use a tape recorder as an automatic keyer for calling. Calls such as CQ DX, CQ Nevada, CQ SS and the like are sent on a code oscillator and recorded on selected sections of the tape so they can be played back into the automatic keyer.




The diagram shows the keying system described in *The Short Wave Magazine* (London, England).

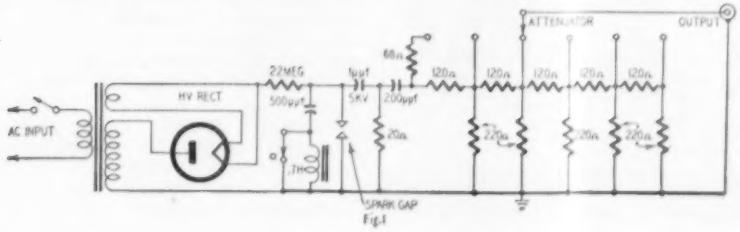
The signal from the recorder is taken from the voice-coil winding and fed into the grid of a 6J5 or similar triode used as a trigger tube. Transformer T can be an intercom input or single-ended output type with a primary of about 20,000 ohms. Output transformers should be connected in reverse with the high-impedance winding feeding the grid. The variable resistor in the cathode circuit is set so the tube is biased close to cutoff and RY1 does not close. The germanium diode rectifies the keyed tone and develops a positive voltage on the grid. This increases the plate current and operates RY1. RY2 is a d.p.d.t. keying relay.

The receiver circuit is modified for break-in operation by removing the ground connection from the receiver's r.f. gain control (R2) and inserting an auxiliary control (R1) of the same resistance, as shown. R1 limits the strength of the transmitter signal to a convenient level for monitoring.

When the keying relay is operated, either with the key or automatic keyer, contacts 2 and 3 short the receiver's ground and antenna terminals, 5 and 6 open to lower the set's sensitivity and 4 and 5 close to key the v.f.o.

## IMPULSE NOISE GENERATOR

In many instances laboratories and home experimenters need an inexpensive source of ignition type impulse noise for testing noise limiters and checking noise-immunity characteristics of various TV sync circuits. This simple spark type noise generator was described in *Electronic Engineering* (London, England). The generator in Fig. 1 consists of an a.c. type scope or TV high-voltage power transformer delivering about 5 kv, a 500-$\mu\mu$f high-voltage charging capacitor and a variable spark gap made from a spark plug modified as in Fig. 2. The setting of the screw varies the gap and breakdown voltage from about 1,000 to 3,000 volts.





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When the gap is at maximum, the capacitor takes longer to charge to the gap's breakdown voltage and the frequency of the noise pulses is relatively low—as when an automobile is idling. Opening the switch cuts in a 0.7-henry inductor. This causes damped oscillations that produce a chain of lesser-amplitude pulses after each main spark discharge.

The generator should be enclosed in a tightly shielded box with the line cord entering through suitable filters.

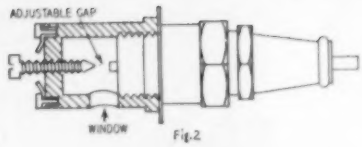
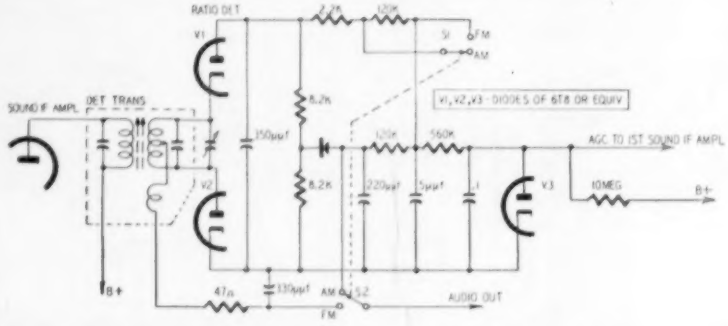


Fig. 2

## UNUSUAL FM–AM DETECTOR

A TV set designed for universal reception of European TV stations is necessarily complicated because of the differences in bandwidth standards, number of lines, video modulation polarity and sound transmission. The diagram shows the sound detector of a Philips multistandard receiver described in *La Radio-Télévision Professionnelle* (Paris).



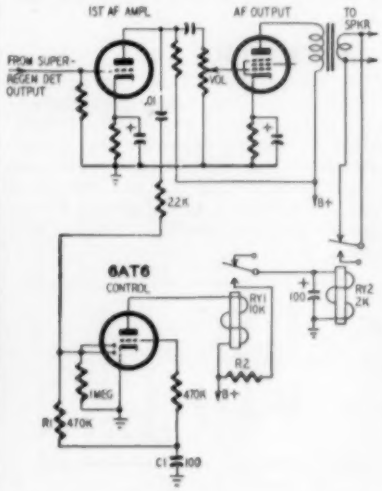

V1 and V2 are in a ratio detector circuit for FM signals. When the switch is set to FM, the 120,000-ohm resistor is shorted out by S1, the FM signal is detected and a d.c. voltage is applied to the a.g.c. line. When the switch is thrown to AM, the ratio detector is unbalanced to the point that it will handle an AM signal. The germanium diode limits impulse type noise that exceeds the level of 100% modulation.

Experimenters will probably be able to adapt this circuit to 30–50- and 150–175-mc inexpensive FM receivers.

## AUDIO SQUELCH FOR SUPERREGENERATOR

The August, 1954, issue contained an Australian codan circuit for automatic band scanning with a 2-meter superregenerative receiver. I modified this circuit for use as an audio squelch for short-range superregenerators used on emergency and CD frequencies.

The first a.f. amplifier—a 6C4 or equivalent—is run wide open to insure ample hiss voltage to operate the control tube. A portion of the audio voltage is tapped off and fed to the diodes of the 6AT6 control tube through a .01-μf capacitor and 22,000-ohm resistor. This voltage is rectified to provide a negative bias voltage for the triode grid. The bias voltage is filtered by R1–C1 a short time constant.




When no signal is coming in, the hiss from the superregenerator is high enough to develop sufficient bias on the 6AT6 triode to hold the relays open so the speaker voice coil is shorted. When a carrier is tuned in, the negative bias drops and the relays (RY1 and RY2) operate to remove the short from across the speaker.

When the carrier is modulated, the bias voltage varies at an audio rate because of the short time constant so RY1 chatters. However, RY2 stays closed because of the long time constant formed by the 100-μf capacitor and the resistance of the coil. The resistance of RY2 and the capacitor value were selected to hold in during normal pauses in speech. R2 is selected for positive action of RY2 while limiting current to the manufacturer's specs.

*—Richard G. Strippel*

## LOSS-TYPE MODULATOR

Sometimes a modulated signal is needed for a test or experiment when a modulated-signal generator is not readily available. This device provides means for using one ordinary signal generator to modulate the signal from another. Construction is simple and most of the parts needed could be found in an experimenter's junkbox.

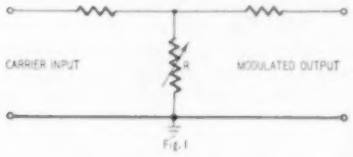



Fig. 1

This is a loss-type modulator. Fig. 1 shows the principle used. Essentially, it is a T-attenuator in which the shunt resistor (R), is varied by the modulating signal. Thus the attenuation is varied and with it the level of output from the modulator, which is what is desired.

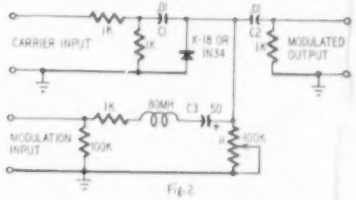



Fig. 2

Fig. 2 shows the circuit actually used. The controlled resistance is a germanium diode (a Transistor Products X-18 was used; other types, such as 1N34 are also suitable). The carrier and modulating signals are both applied to the diode, the modulating signal controlling the resistance it offers to the carrier signal. Capacitors C1 and C2 block the modulating signal from the carrier channel, while the choke blocks the carrier frequency from the modulating signal channel. The diode's rectifing action charges C3 to a voltage that depends on the setting of potentiometer R. Thus, by controlling the point about which the diode operates, R controls the modulation. The values shown are for a 50-kc carrier. If the carrier frequency were around 500 kc or higher, as would be more usual, C1, C2 and the choke could be reduced say to one-tenth the indicated value.

In operation, the carrier signal is set at the desired level and the modulating signal is adjusted, along with R, to give the desired amount of modulation. It is helpful to observe the modulated output on an oscilloscope during adjustment. This device does not produce really high-quality modulation, but the result is still acceptable for many test purposes.

For convenience, the circuit was built in a Bud HB-1621 *Handi-Box* and equipped with three terminal post pairs (Millen 37222) for the inputs and outputs.—*H. L. Armstrong* END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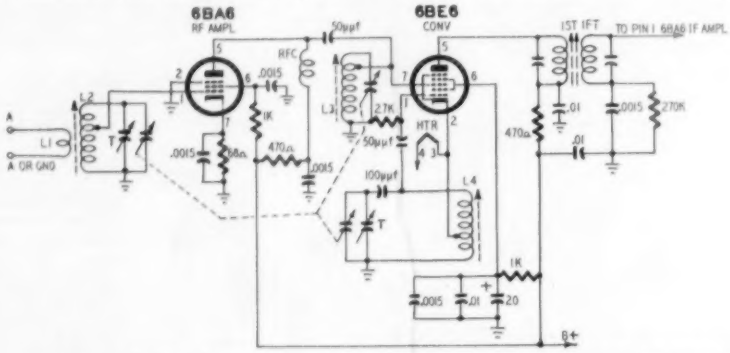
# Question Box

## PILOTUNER ON 30 TO 50 MC

*I have a Pilotuner model T-601 that I'd like to modify for reception on 30 to 50 mc. Please show the necessary circuit changes.—Y. G. R., Minneapolis, Minn.*

The diagram shows the front end of the T-601 FM tuner as modified with new coils for the 30–50-mc band. L2, L3 and L4 are each seven turns of No. 20 enameled wire closewound on CTC (Cambridge Thermionic Corp.) type LSM forms. Grid taps on L2 and L3 are made one turn from the top end of the winding and the cathode tap on L4 is two turns from the bottom. L1 is three turns of No. 28 enameled wire closewound over the ground end of L2 and separated from it by a double layer of cellophane tape.




A grid-dip oscillator and a signal generator are used for front end alignment. Use the grid-dip oscillator to adjust the trimmer and slug of L2 and the slug of L3 so the antenna and r.f. circuits tune from 30 to 50 mc. Next, adjust the oscillator trimmer and the slug in L4 for a tuning range of 40.7 to 60.7 mc.

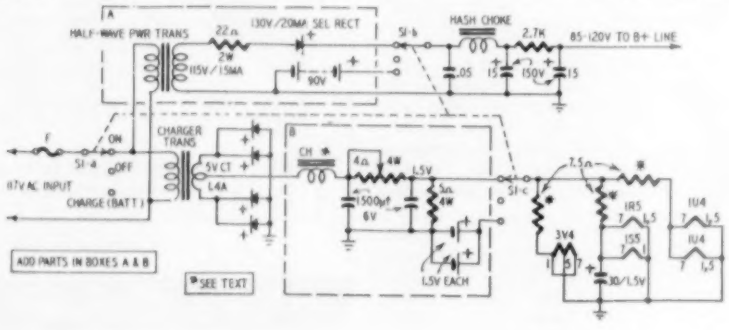
After completing these preliminary adjustments, align the front end with the signal generator. It may be necessary to replace the 100-$\mu\mu$f fixed oscillator padder with a variable type and adjust it for good tracking.

A noise generator can be used to determine the optimum number of turns on L1, to adjust the coupling between L1 and L2 and to set the taps on L1 and L2 to provide the best signal-to-noise ratio.

## CONVERTING THE G-E 160

*Frequent replacements of the vibrator and 2-volt storage battery in my G-E model 160 a.c.–battery portable radio are expensive and annoying so I'd like to convert it to a three-way type using dry batteries. Please show the circuit modifications.—P. M., South Greenburg, Pa.*

Converting the set for three-way operation would require rewiring the filament circuit for series operation, installation of balancing or filament-shunt resistors and the use of 7.5- or 9-volt A batteries. We suggest two-way conversion for a.c. and dry-battery operation as shown in the diagram.



The job is greatly simplified and filament batteries are less expensive and much easier to obtain. Components enclosed in dashed lines are added to the set. A half-wave a.c.-operated supply replaces the vibrator and its transformer. The output of the charging circuit is filtered and used to light the filaments for a.c. operation.

The vibrator, vibrator transformer and storage battery must be removed to make room for the new components and dry batteries. Study the three-circuit, three-position ON–OFF–CHARGE switch and remove all leads from S1-b, S1-c and from the CHARGE (now BATTERY) position of S1-a.

Disconnect the lead from the center tap on the vibrator transformer secondary and connect it to the arm of S1-b. Remove the vibrator transformer and install a 115-volt power transformer and rectifier connected as in box A. Connect the primaries of the power and charger transformers in parallel. Connect the positive side of the half-wave rectifier to the ON contact of S1-b and a connector for the positive B battery terminal to the BATTERY terminal of S1-b. This completes the new B plus circuit.

Install and wire the low-voltage filter enclosed in box B. Connect the ON contact of S1-c to the output of the filter and the BATTERY contact to a lead for the positive terminal of the 1.5-volt A battery.

Run a lead from the positive charging-cable connector or from the tap on the charger transformer to the choke in the low-voltage filter. This choke is made by winding as many turns of No. 22 enameled wire as possible on the core of an old a.c.–d.c. type filter choke. Remove the three 7.5-ohm filament dropping resistors and run a lead from the arm of S1-c to pin 7 on each tube socket. This completes the filament-circuit modifications.

The filament voltage must be adjusted before operating the set on a.c. Remove the tubes from the sockets and temporarily connect a 5.6-ohm 1-watt resistor from the arm of S1-c or pin 7 of one socket to ground. Adjust the 4-ohm variable resistor for exactly 1.5 volts across the 5.6-ohm unit. Remove this resistor and replace the tubes.

## GOLDEN EAR AMPLIFIER

*An Acrosound TO–300 output transformer was specified for Milady's Golden Ear amplifier described in the April, 1954, and February, 1955, issues. Can I substitute a Stancor A–8072 or Chicago BO–13? Is there any simple way of adding a damping-factor control to this amplifier?—M. M. R., Nashville, Tenn.*

Ordinarily, it is not safe to substitute another make or type of output transformer for one specified by the designer of a high-fidelity amplifier because the circuit is often modified to fit the characteristics of the specific transformer. However, Mr. Marshall reports that he tried both these transformers in the improved versions of

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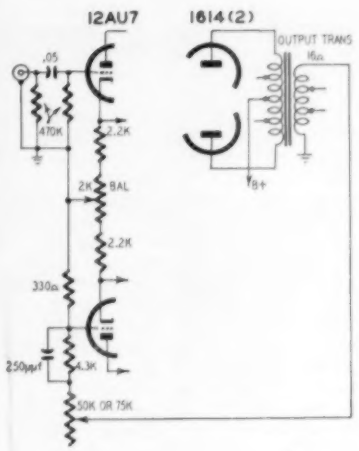
## QUESTION BOX *(Continued)*

Milady's Golden Ear and Junior Golden Ear amplifiers modified as described in the article "Guilding the Golden Ears" in the February, 1955 issue.

Their use did not require any circuit changes or adjustments. Performance differed slightly in the ultra-and subsonic regions but stability was good and performance entirely satisfactory within audible limits.

The improved version of Milady's




Golden Ear amplifier is easily modified to provide a considerable variation in damping factor. Add a variable resistor in series with the feedback resistor as shown in the diagram. As the resistance is increased feedback decreases and the amplifier's resistance and damping factor are varied. The variation in damping factor runs from about 10 to about 1.5. This range is sufficient to take care of almost any combination of speaker, enclosure and room acoustics. The reduction in feedback is not great enough to cause a significant rise in distortion.

Do not take out the fixed resistor in the feedback circuit. It establishes the maximum feedback that can be used with good stability. Any attempt to increase feedback beyond this point may result in oscillation which will endanger the speakers—especially tweeters.

END

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# Technotes

## FUSIBLE RESISTOR

A plug-in type fusible resistor (R501, 7.5 ohms) is used in the V-2342 and V-2343 chassis. The purpose of this resistor is to protect the selenium rectifiers and to act as a fuse in case of an overload.

The resistor may be replaced simply by inserting a new unit in the holder mounted on the TV chassis. Resistor R501 will withstand a peak current surge of approximately 5.6 amperes and will open up in case of an overload.—*Westinghouse Service Manual*

## INTERMITTENT MOVING CURVE

A rather exasperating moving curve was encountered recently in a Du Mont RA-166. The curve would move slowly up or slowly down the picture, depending on both time and the station being received, and for long intervals would remain stationary as a bend in all vertical lines in the picture. The curve resembled a part of a 60-cycle hum wave and is shown in Fig. 1 in its stationary position. This resemblance plus the fact that the symptom would lock at intervals and on certain stations furnished the clue to the diagnosis.

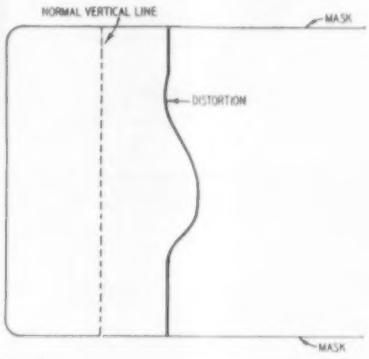

Fig. 1

The trouble was found to be caused by leakage between the grid and the heater terminals of the 6SN7 horizontal oscillator tube socket due to dust and moisture, and excessive heater-to-cathode and grid-to-cathode leakage of the horizontal oscillator. These combined to produce the trouble, which varied with the insertion of different 6SN7's in the horizontal oscillator socket. This tube substitution localized the fault to he 6SN7 circuit or near it.

Resistance checks revealed the trouble. The coupling of the two cathodes together in the cathode-coupled horizontal multivibrator circuit (Fig. 2) caused the leakage to affect the normally on tube although the ohmmeter test re-

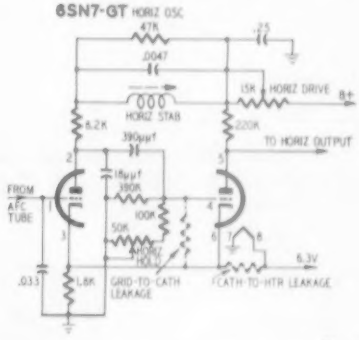

Fig. 2


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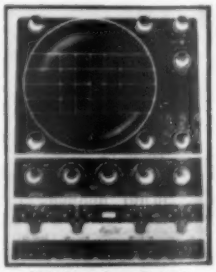

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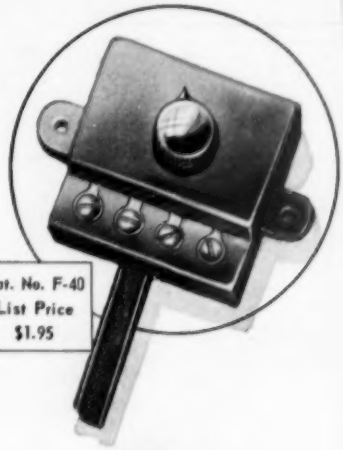

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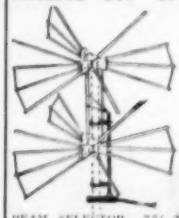

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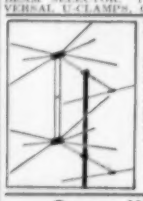

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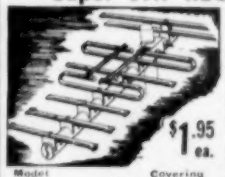

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TECHNOTES *(Continued)*

vealed that the leakage happened in the normally off tube. Apparently some clipping action occurred which removed a part of the 60-cycle wave and resulted in the reproduction of only a part of it. The leakage paths were caused by the location, a bar-and-grill, and consisted of an accumulation of grease and smoke deposits on the socket. The horizontal output and the high-voltage rectifier sockets were cleaned as a precautionary measure. The owner has since installed a duct from his fresh air ventilating system and directed at the rear of the set.—*James A. McRoberts*

## G-E 16C103

A frequent occurrence in this set is a condition of no sound, no raster and tubes not lit. The trouble is usually a defective 20-ohm Globar resistor connected in series with the filament. Replace it with an exact duplicate. This resistor will measure 20 ohms when hot, 250 ohms cold.—*Dee Bramlett, Jr.*

## VERTICAL BARS

Shadow type vertical bars usually at the left of the raster in Admiral chassis 20T1, V1 and 21B1, C1, D1, H1, J1, can be minimized by one or more of the following methods:

Be certain the horizontal drive and width controls are adjusted as outlined in the service manual.

Dress the cathode lead (yellow) so it will not come close to the horizontal output tube.

Install a filter (chassis 20T1, V1) consisting of a variable inductance (width coil), .005-$\mu$f 600-volt capacitor and 470-ohm 1-watt resistor in parallel, to terminal 8 of the horizontal output transformer. The two leads already attached to this terminal should be removed and connected to the other side of the filter. If the Admiral 79C36 output transformer is used, it may be necessary to connect two filters in series. The filter should be placed inside the high-voltage cage and not under the chassis. Then vary the inductance until the bars are eliminated or reduced.

In the remaining chassis the procedure is the same except that terminal 4 is used on the output transformer.—*Admiral Radio & Television Service Bulletin*

## SMALL HORIZONTAL SIZE

At normal line voltages, some Stromberg-Carlson model 421 television receivers produce second-anode voltages in excess of 18 kv, resulting in insufficient picture width. This high voltage can be reduced and sufficient width obtained by connecting a 60-$\mu\mu$f 3-kv mica capacitor in series with a 560-ohm resistor between terminals 3 and 7 of the horizontal output transformer. The resistor must be connected to terminal 3 and the capacitor to terminal 7 to avoid corona.

As an additional aid, the screen dropping resistor for the 6AV5 horizontal output tube should be decreased in value from 15,000 to 12,000 ohms.—*Current Flashes*

END

# Technicians News

## TECHNICIANS SPEAK UP

The Milwaukee Association of Radio and Television Services maintains a bureau to supply speakers for neighborhood clubs, church organizations, labor unions and other interested groups.

MARTS recruits speakers from its membership and supplies them with a "tested" script which incorporates the main MARTS policies and the group's ethical standards as well as other information that "99 out of 100 audiences should appreciate and find interesting."

The title of the basic speech is "How to Save Money on TV Repairs." It is said to have drawn excellent audiences wherever presented.

## ACCREDITATION PROGRAM

RETMA (Radio–Electronics–Television Manufacturers Association) has issued a booklet detailing a plan whereby technically competent TV service technicians can be accredited for easy identification by set owners. RETMA feels that this plan will induce technicians to upgrade themselves to receive recognition and promote their services. The accreditation certificates or diplomas will carry RETMA endorsement.

Two methods of accreditation are suggested. Those who successfully complete the training and upgrading course prepared by RETMA would receive a certificate attesting to their technical competence. For technicians who already possess the necessary degree of proficiency, the booklet suggests that local advisory groups devise tests covering theory and working knowledge. The booklet, "Suggested Accreditation Program for TV Receiver Service Technicians," can be obtained from RETMA, 777 14 St., N. W., Washington 5, D. C.

## PLEADS GUILTY

A New York City service dealer charged with petty larceny, conspiracy and misleading advertising in connection with television repairs reversed his not-guilty plea to the three-count charge in favor of a lesser single-count charge of petty larceny.

The service dealer was apprehended when an employe of his was called to service a "planted" set containing one defective tube; all components were coded under police supervision. The set was returned with an $18 repair bill, and the defective tube had been replaced. The employe turned informer and the charges against him were dismissed.

## FEWER SERVICE COMPLAINTS

The complaint situation in the TV service field has improved generally during the past year, it was revealed at the annual convention of Better Business Bureaus held recently in Minneapolis.

A survey of 78 cities showed that 46 local Better Business Bureaus had received fewer complaints, reported Kenneth Wilson, president of the National BBB and chairman of its radio–TV committee. The situation had deteriorated in 6 cities, he said, while 20 bureaus reported no change from last year. Six did not report.

The business of the convention pointed up the improvement even more than the report. Practically all com-


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**PICTURE TUBES**

● RCA Licensed ● One Year Unconditional Guarantee

| TYPE | PRICE | TYPE | PRICE |
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| 10BP4 | $11.90 | 17BP4 | $20.63 |
| 12LP4 | $14.38 | 19AP4 | $24.81 |
| 14BP4 | $16.86 | 21AP4 | $28.79 |
| 16RP4 | $19.38 | 21EP4 | $28.79 |
| 16LP4 | $19.38 | 24AP4 | $42.50 |

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*With Every $25 Order*
- 1 RCA Cheater Cord
- 10 Assorted resistors
- 10 Assorted 2-Color "blank" tube cartons
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**FREE CLOCK RADIO**
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Wakemaster clock radio with famous Sessions clock movement wakes you to music or alarm. May be purchased outright from MAJOR BRAND for $17.95. In ivory or rust.

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Clip out this ad and attach it to your order. Three 6SN7GT's will be shipped FREE with any order of $10 or more.

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● Each Tube Individually Boxed and Guaranteed for Life
● Over a Half Million Tubes Always in Stock
● Immediate Shipment
● Free Postage On All Orders With Full Remittance

**Here's How LIFETIME GUARANTEED TUBES SAVES YOU PLENTY!**
● There are fewer "call backs"
● There are no "out of date" tubes
● "Peak Performance" testing in our fully equipped Testing Department before shipment guarantees quality

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 0Z4 | .43 | 5AW4 | .75 | 6BL7GT | .75 | 6X4 | .34 | 12SK7 | .45 |
| 1A4P | .33 | 5J6 | .63 | 6BN6 | .58 | 6X5 | .34 | 12SN7GT | .56 |
| 1A7GT | .43 | 5T4 | .69 | 6BQ6GT | .78 | 6X8 | .73 | 12SQ7 | .47 |
| 1B3GT | .65 | 5U4G | .43 | 6BQ7 | .78 | 6Y6G | .55 | 12SR7 | .45 |
| 1C5GT | .41 | 5U8 | .74 | 6BY5G | .58 | 7A4 | .45 | 12V6GT | .45 |
| 1D5GP | .43 | 5V4G | .59 | 6BZ7 | .88 | 7A5 | .51 | 12X4 | .42 |
| 1E7GT | .41 | 5Y3 | .31 | 6C4 | .39 | 7A6 | .45 | 14A7 | .42 |
| 1G6GT | .41 | 5Y4G | .36 | 6C5 | .35 | 7A7 | .43 | 1486 | .38 |
| 1H4G | .43 | 5Z3 | .41 | 6C86 | .49 | 7A8 | .46 | 14Q7 | .50 |
| 1H5GT | .47 | 6A7 | .57 | 6C06G | 1.15 | 7B5 | .39 | 19BG6G | 1.15 |
| 1J6GT | .47 | 6A8 | .45 | 6D6 | .48 | 7B6 | .42 | 19T8 | .65 |
| 1L4 | .45 | 6AB4 | .43 | 6E5 | .44 | 7B7 | .41 | 24A | .39 |
| 1L6 | .55 | 6AC7 | .67 | 6F5 | .77 | 7B8 | .45 | 25AV5GT | .78 |
| 1LA4 | .57 | 6AF4 | .79 | 6F6 | .38 | 7C4 | .39 | 25B06GT | .78 |
| 1LA6 | .47 | 6AG5 | .50 | 6G6 | .40 | 7C5 | .42 | 25L6GT | .47 |
| 1LB4 | .57 | 6AG7 | .69 | 6H6 | .38 | 7C6 | .43 | 25W4GT | .47 |
| 1LC5 | .49 | 6AH6 | .69 | 6J4 | 1.79 | 7C7 | .45 | 25Z5 | .37 |
| 1LC6 | .47 | 6AJ5 | .70 | 6J5 | .39 | 7E5 | .45 | 25Z6 | .37 |
| 1LD5 | .57 | 6AK5 | .54 | 6J6 | .47 | 7E6 | .55 | 27 | .25 |
| 1LE3 | .57 | 6AL5 | .39 | 6J7 | .43 | 7E7 | .70 | 35A5 | .46 |
| 1LG5 | .57 | 6AQ5 | .46 | 6J8G | .85 | 7F7 | .59 | 35B5 | .50 |
| 1LH4 | .64 | 6AR5 | .46 | 6K6GT | .37 | 7F8 | .70 | 35C5 | .50 |
| 1LN5 | .47 | 6AS5 | .48 | 6K7 | .39 | 7G7 | .75 | 35L6GT | .47 |
| 1NSGT | .50 | 6AS6 | 1.70 | 6KR | .65 | 7H7 | .50 | 35W4 | .34 |
| 1RS | .50 | 6AS7G | 2.19 | 6L6 | .68 | 7J7 | .75 | 35Y4 | .34 |
| 1S5 | .42 | 6AT6 | .39 | 6L7 | .42 | 7K7 | .75 | 35Z3 | .39 |
| 1T4 | .50 | 6AU4GT | .65 | 6N7 | .60 | 7L7 | .75 | 35Z5GT | .34 |
| 1U4 | .47 | 6AU5GT | .59 | 6Q7 | .40 | 7N7 | .57 | 37 | .29 |
| 1U5 | .42 | 6AU6 | .42 | 6S4 | .40 | 12AT6 | .37 | 50A5 | .46 |
| 1V2 | .65 | 6AV5GT | .65 | 6SA7 | .45 | 12A77 | .66 | 50B5 | .50 |
| 1X2 | .61 | 6AV6 | .39 | 6SC7 | .48 | 12AZ7 | .63 | 50C5 | .50 |
| 2A3 | .55 | 6AX4GT | .60 | 6SG7 | .41 | 12AU6 | .41 | 50CD6 | .50 |
| 2A5 | .57 | 6AX5GT | .57 | 6SH7 | .42 | 12AU7 | .53 | 50L6GT | .47 |
| 2A7 | .55 | 6B4G | .52 | 6SJ7 | .43 | 12AV6 | .35 | 75 | .42 |
| 3A4 | .51 | 6B8 | .69 | 6SK7 | .45 | 12AV7 | .67 | 76 | .42 |
| 3A5 | .50 | 6BA6 | .47 | 6SL7GT | .45 | 12AX4GT | .65 | 78 | .42 |
| 3AL5 | .45 | 6BA7 | .58 | 6SN7GT | .55 | 12AX7 | .58 | 77 | .38 |
| 3AU6 | .46 | 6BC5 | .47 | 6SQ7 | .39 | 12B4 | .68 | 78 | .38 |
| 3BC5 | .54 | 6BC7 | .80 | 6SR7 | .42 | 12BA6 | .46 | 80 | .34 |
| 3BN6 | .70 | 6BE6 | .45 | 6SS7 | .41 | 12BD6 | .48 | 84-6Z4 | .44 |
| 3CB6 | .52 | 6BF5 | .40 | 6T4 | .95 | 12BE6 | .46 | 117L7GT | 1.09 |
| 3Q4 | .52 | 6BF6 | .40 | 6T8 | .68 | 12BH7 | .60 | 117N7GT | 1.09 |
| 3Q5GT | .57 | 6BG6G | 1.15 | 6U8 | .75 | 12BY7 | .65 | 117P7GT | 1.09 |
| 3S4 | .47 | 6BH6 | .50 | 6V3 | .80 | 17BZ7 | .61 | 117Z3 | .35 |
| 3V4 | .47 | 6BJ6 | .47 | 6V6GT | .46 | 12CU6 | .55 | 117Z6GT | .63 |
| 4BQ7 | .89 | 6BK5 | .68 | 6W4GT | .39 | 12SA7 | .45 | | |
| 4BZ7 | .95 | 6BK7 | .76 | 6W6GT | .53 | 12SJ7 | .45 | | |

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| SPECIFICATIONS | CJ-30 | CJ-14 |
|---|---|---|
| Input pwr (cont.) | 15 w | 5 w |
| Input imp. | 4 or 8 Ω | 4, 8 or 45 Ω |
| Response (cps) | 250-9,000 | 400-10,000 |
| Dispersion | 120° x 60° | 120° x 60° |
| Bell Size | 14" x 6" | 9½" x 5½" |
| Over-all length | 14" | 8½" |

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ment on TV was on selling practices: questionable price comparisons, bait ads, misleading layouts, failure to disclose obsolescence of advertised receivers and questionable trade-in allowances.

## ETHICAL $1 TV SERVICE

The Milwaukee Association of Radio and Television Services reports a $1 television service organization that carried on its business on strictly ethical lines. The operation was run as a survey for MARTS by a local radio–TV service shop.

The "company," Dollar TV Service, was set up on a no-overhead basis, with the bench space, tools and incidentals furnished by the shop. Only the phone number — a customer-pulling WE 3-3333—advertising, wages and actual cost of parts were charged as costs, making the setup resemble that of a home operator.

In the 3 weeks of the survey, 36 phone calls were received, leading to 16 completed jobs, 2 of which required removing sets to the shop for work that could not be done in the home.

Net income for the experiment totaled $54.50. Expenses charged against this sum were: advertising, $150.36; telephone, $24; wages $100; shop labor $16.62; miscellaneous, $11.56. Net loss was $205.69, or $12.85 on each actual service call.

Two conclusions were drawn from the experiment:

1. The response to bargain advertising (36 phone calls in 3 weeks) is not as good as it might seem from the outside.

2. It is impossible to make a profit with both low rates and high ethics—one or the other must inevitably be sacrificed.

## CERTIFICATION PLAN

A plan to certify parts jobbers who do not sell to consumers at wholesale prices and who give service dealers longer discounts than experimenters and students is under way by TISA (Television Installation Service Association), a NATESA (National Alliance of Television and Electronics Service Associations) affiliate well known to our readers.

Frank J. Moch, TISA president, said that the basis of the certification will be shopping of the jobbers. He added that those jobbers that do not fill the requirements of certification will not be named. "We are not attempting to restrict jobber sales. We have no quarrel with ham sales and with industrial sales. We even concede the right of jobbers to sell students and experimenters—so long as they are given shorter discounts than service firms. We do say that the jobbers have no right to sell to the ultimate consumer at wholesale prices."

Mr. Moch thinks it likely that the TISA certification will be adopted by other NATESA affiliates if it proves successful in the Chicago area. END

# Patents

## NULL DETECTOR

**Patent No. 2,702,854**

*William E. Woods, Haddonfield, N. J., (Assigned to RCA)*

At the moment of null, this very sensitive null detector generates and delivers a pulse that can be amplified as desired. The patent description assumes a sawtooth signal but any other waveshape can be applied. As the sawtooth goes through the transition from negative to positive (or vice versa), a sharp pulse occurs to indicate the exact instant.

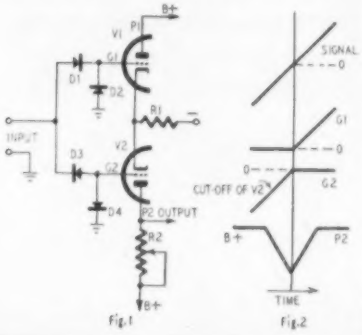


Fig. 1



Fig. 2

The detector includes a double-triode coupled through common cathode resistor R1 (Fig. 1). The signal feeds grids G1, G2 through a network of diodes. Output is taken at P2, the plate of the lower triode. Fig. 2 shows how voltages at G1, G2, P2 vary with signal.

While the input is *negative*, D1 isolates G1 but D3 conducts the negative signal to G2. D2 grounds the upper grid. D4 is blocked and has no effect. When the signal goes *positive*, it passes freely through D1 to grid G1. The positive signal blocks D3. At this time D2 is cut off, and D4 grounds G2. The net result is that a negative signal affects only G2, leaving G1 at ground potential.

The potential at P2 remains equal to that of the B battery except when current flows through the lower triode. Such a current cannot occur when G2 is highly negative since this will block the triode; it cannot occur when G1 is very positive either. A large current through the upper triode means a large voltage drop across R1. This would drive the common cathode very positive and have the effect of a large negative bias on G2.

The lower triode can conduct *only* when G1 and G2 are at or nearly at zero potential. Conduction is greatest when they are both zero.

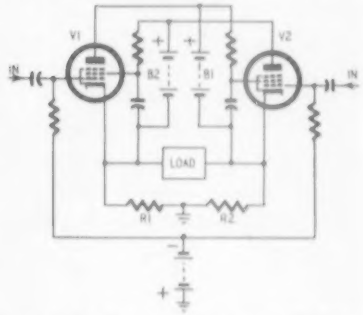
## TRANSFORMERLESS AUDIO OUTPUT

**Patent No. 2,705,265**

*Cecil T. Hall, Mount Lebanon, Pa.*

In this output stage the power tubes are energized in push-pull, but they feed the load in parallel. A low-impedance load is matched without a transformer. This is a worth-while improvement because the transformer is often the biggest and most expensive component and the major source of distortion in the amplifier.

For low-impedance matching, the load is connected in the cathode return leads. The input signals to the grids must be equal and out of




phase as in any push-pull circuit. With zero signal, V1 and V2 have equal conductivity so the stage is balanced. No voltage appears across the load. When one signal goes positive (and the other negative), the balance is destroyed. One tube will pass greater current through the load, while the other tube current decreases. Since these currents flow in *opposite directions* through the load, their effects are additive. The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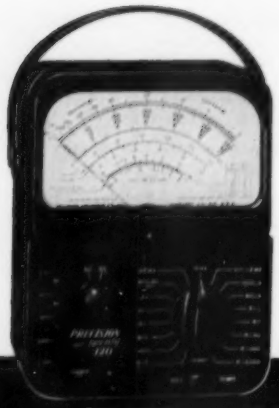

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tubes supply equal power. So far as the load is concerned they are in parallel, thus lowering the output impedance.

Resistors R1, R2 form a center-tapped cathode return for the tubes. If the load itself is center-tapped, they are not needed. Two separate plate supplies (B1, B2) are required.

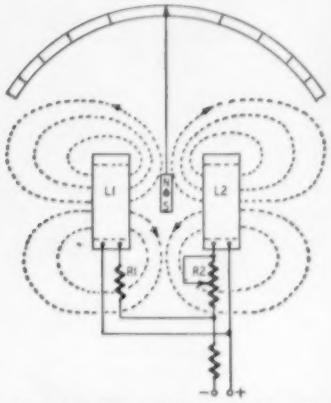
## MAGNETIC RATIO METER

### Patent No. 2,704,827

*Norval P. Millar, Danvers, and Stephen C. Hoare, Manchester, Mass. (Assigned to G-E.)*

A dual magnetic field rather than the usual single field controls this meter. This gives it greater sensitivity and versatility than the ordinary d'Arsonval instrument. Two coils (L1 and L2) produce the fields, L2 being adjustable. A small permanent magnet fixed to the bottom of the pointer provides deflection torque.

The coils are energized oppositely to strengthen the flux between them. When these fields are equal, the magnet assumes a vertical position




(as shown) and the pointer remains at mid-scale. If R2 is reduced, more current flows into L2, strengthening its magnetic field. This deflects the pointer counterclockwise. The instrument may be calibrated in terms of the *ratio* between magnetic fields. The pointer deflects to the right when L1 generates a stronger field than L2.

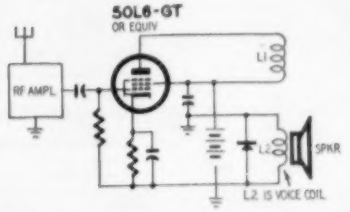
The meter may be used to measure temperature. For this application, R2 is a temperature-sensitive unit. Its resistance varies with temperature, thus changing the ratio between field strengths and deflecting the pointer. To measure magnets, the instrument is modified by substituting a permanent magnet for one of the coils. The meter then compares the field of the remaining coil with that of the magnet.

## ALL-R.F. RADIO RECEIVER

### Patent No. 2,706,245

*Joseph L. Miller, South Haven, Mich.*

Very high selectivity, sensitivity and fidelity are provided by this radio. It also reduces noise to a minimum. The front end, composed of several r.f. stages, is followed by a power r.f. stage. The tube may be type 50L6, for example, and is connected as a cathode follower. Coils




L1, L2 are coupled for negative feedback and output is taken from L2.

The diode across L2 detects the carrier and rectified r.f. is fed to the speaker. Due to its mass, the cone cannot vibrate at such high frequencies, but it can follow the wave envelope, that is, the audio modulation. END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## HELP - FREDDIE-WALK FUND

WE have received some very good news from Herschel Thomason, radio technician of Magnolia, Ark., who, as most readers know, is the father of 7-year-old Freddie Thomason, the little boy who was born without arms or legs. He writes as follows:

"Freddie is scheduled to receive his arm very soon and we are very happy about it. All he talks about it what he is going to do when he gets his arm, and we are confident that he will be able to master it without too much trouble.

"He is still walking quite well and can go all over the house by himself. We had a private teacher with him for his schooling this year and he did fine. He learned to read fairly well and also learned to recognize various colors. He will have the same teacher next year but after that we hope to put him in the public school here.

"When he gets the new arm, he will also get a new set of legs, and altogether they will cost about $1,300; so you can see that we really appreciate the RADIO-ELECTRONICS Help-Freddie-Walk Fund.

We believe the letter speaks for itself. Thanks to the generosity of thousands of readers, Freddie is well on the way to becoming the healthy, constructive member of society we all want him to be. But, and it's a BIG but, the mechanical appliances upon which he will be dependent all his life cost money, *lots* of money. For this reason, we again ask our readers to send in their contributions as often as they can. No amount is too small to receive acknowledgment and the grateful thanks of Freddie and his entire family. *Make out all checks, money orders, etc., to Herschel Thomason.* Send all contributions to

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| Margaret Morrissey, Worcester, Mass. | 2.00 |
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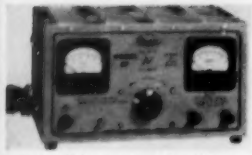

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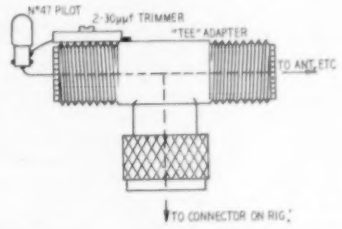
# try This one

## R.F. INDICATOR

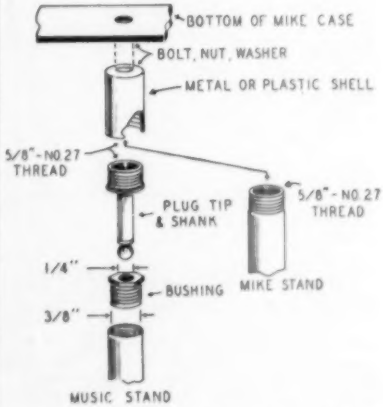
It is not easy to connect any type of r.f. or tuning indicator to a coaxial line feeding a transmitting antenna. I have solved the problem by modifying an Amphenol 83-1T tee adapter as shown. The trimmer is adjusted to vary




the brightness of the bulb. Transmitter controls are adjusted for maximum brightness. I use this method when tuning my Gonset Communicator.—*Joseph Zukauskas*

## MOUNTING HOME MIKES

A standard phone plug and an old metal music rack can be used to make a satisfactory floor stand for nonprofessional type microphones generally used for home recording and amusement. The drawings show the construction details.

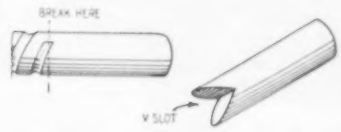



Drill a hole in the bottom of the mike case and bolt it to the shell of the phone plug. Screw or sweat a panel bearing or bushing from an old phone jack or volume control into the top of the music rack. The mike can now be mounted and removed with ease.

If you have a standard floor or table type mike stand, simply screw the phone plug onto it.—*David J. Anaple*

## A SIMPLE PUNCH

Many times it is more desirable to punch than to drill a hole in light sheet metal and other materials. When a punch of the proper size is not available, you can make one from a broken




or worn out twist drill of the correct diameter.

First break off the twist or spiral portion and grind a "V" slot in the shank end as shown in the drawing. A sharp blow with a hammer on the blunt end produces a clean hole.—*Stanley Rubin*

## SERVICING HINT

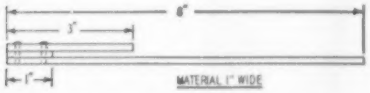
Most radio–television service shops make it a regular practice to clean the cabinet of every set that comes in for servicing. Certainly most of them need it, and all customers appreciate picking up a clean shiny cabinet after a servicing job.

I have found that one of the very best tools for this job is a stiff-bristled plastic brush commonly sold in drug and dime stores as hand or finger brushes. These will clean the dirt from the embossed dials and lettering on plastic cabinets, particularly portables, better than any other device I have yet used.

Knurled dial knobs are the hardest to clean since they usually get the most handling and have sharp grooves where dirt accumulates. They can be cleaned like new by rubbing in the direction of the grooves with the plastic hand brush. No water or other cleaner is necessary, and I have never yet scratched or damaged a cabinet with this method.—*L. H. Wilson*

## TV CHASSIS SUPPORTS

Make a set of these simple chassis supports and use them to prevent tube breakage and other mechanical damage that often occurs when a heavy TV chassis tips over.




You can use any strip steel or other metal that is about 1 inch wide and heavy enough to support the chassis. Turn the chassis on its side in a convenient position and then slide the supports into position so the chassis skirt is firmly in the notch between the long and short strips.—*J. Urbanowicz*

(A somewhat similar commercial support has a hole for fastening the support to the bench, as well as a thumbscrew through the top short piece to hold the chassis.) END

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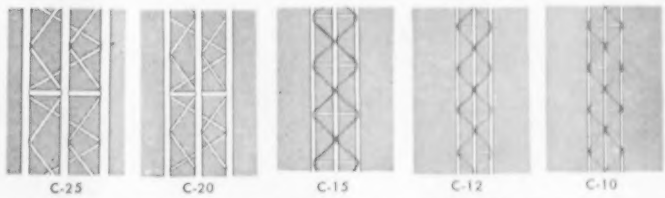


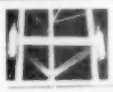
C-25: Width: 25" Legs: 2" pipe Weight per ft.: 20 lbs. Guy Spacing: 80 ft. Max. Height: 320 ft. Diag. Bracing: ¾" pipe Horiz. Bracing: 1 ¼" pipe

C-20: Width: 20" Legs: 1 ½" pipe Weight per ft.: 14 lbs. Guy Spacing: 60 ft. Max. Height: 250 ft. Diag. Bracing: ½" pipe Horiz. Bracing: 1" pipe

C-15: Width: 14" Legs: 1" pipe Weight per ft.: 8 lbs. Guy Spacing: 40 ft. Max. Height: 200 ft. Diag. Bracing: ⅜" rod Horiz. Bracing: ⅝" pipe

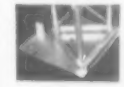
C-12: Width: 10 ½" Legs: ¾" pipe Weight per ft.: 5 ½ lbs. Guy Spacing: 33 ft. Max. Height: 150 ft. Diag. Bracing: 5/16" Rod Horiz. Bracing: ½" Rod

C-10: Width: 10" Legs: ½" pipe Weight per ft.: 4 ½ lbs. Guy Spacing: 27 ft. Max. Height: 120 ft. Diag. Bracing: 5/16" Rod Horiz. Bracing: ½" Rod


C-10, C-12 & C-15 Bolt together 1 ½" fillet on each side.

Work Platform—hooks on C-10, C-12 or C-15 towers.

—Automatic lock for easy raising and lowering of mast when service is required.


Base plate for C-10, C-12 & C-15 has hinge for gin pole and tower.

Connecting point of C-20 and C-25 towers

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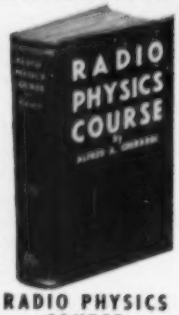


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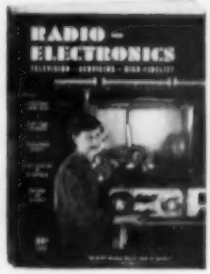


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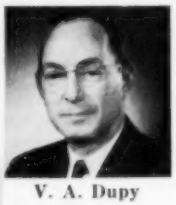
# People

**Alton K. Marsters** was appointed to the new position of general sales manager of CBS-Hytron, Danvers, Mass. He comes to CBS-Hytron from Colt's Manufacturing Co.

A. K. Marsters

**Vernon A. Dupy**, general sales manager of United Motors Service, Division of General Motors, Detroit, Mich., was promoted to director of procurement,


V. A. Dupy

E. L. Lape

scheduling and general merchandising. **Edward L. Lape**, assistant general sales manager, succeeds him as general sales manager.

**Frank Adams** was promoted to Eastern sales manager of ORRadio Industries, Opelika, Ala. He was formerly Mid-Atlantic representative. He will make headquarters in Philadelphia.

F. Adams

**Sam D. Pollack** was elected treasurer of Vaco Products, Chicago. He was heretofore comptroller. **Harry Silverstein**, formerly president and treasurer, was re-elected president. Other officers are **Alvin E. Shugarman**, executive vice president; **James T. Pettengill**, vice president, and **David B. Berger**, secretary.

S. D. Pollack

**W. Walter Jablon** joined Presto Recording Corp., Paramus, N. J., as general sales and advertising manager. He was formerly sales manager of Radio City Products.

W. W. Jablon

J. Bentia

**John Bentia**, former executive vice president of Alliance Manufacturing Co., Alliance, Ohio, was elected president and general manager of the company. He also becomes vice president of Consolidated Electronics Industries Corp., Jackson, Mich., which recently acquired Alliance.

**Obituaries:**

**Rear Admiral Walter A. Buck**, U. S. N. retired, vice president in charge of operating services for Radio Corporation of America, died recently in his home in Wynnewood, Pa.

**Paul C. Smalley**, retired manager of the New York branch of P. R. Mallory, Indianapolis, died in Orange Memorial Hospital, Orange, N. J.

**Personnel Notes**

. . . **Hendrix G. Blue** joined Hallicrafters, Chicago, in the new position of sales promotion manager. He was formerly with Webster-Chicago.

. . . **H. Leslie Hoffman**, Hoffman Electronics Corp., was elected president of the reorganized board of directors of RETMA. Other officers include: **Leslie F. Muter**, Muter Co., treasurer; **Dr. W. R. G. Baker**, General Electric, director of the Engineering Department; **Joseph H. Gillies**, Philco, director of the Government Relations Department; **James D. Secrest**, executive vice president and secretary.

. . . **Larry S. Racine**, president of Chicago Standard Transformer Corp., Chicago, has taken a leave of absence due to ill health. **William J. Shea**, chairman of the board and chief executive officer, assumes the office of president. **Donald Schwennesen**, vice president in charge of engineering, becomes vice president in charge of sales and engineering in Racine's absence. **Ray Gislason** was appointed vice president in charge of all the company's manufacturing plants.

. . . **Ralph B. Austrian** was named West Coast manager of Allen B. Du Mont Laboratories with headquarters in Los Angeles. Since 1927 he has been active in executive capacities in radio, motion pictures and television.

. . . **Isaac Naeye** was appointed assistant treasurer of Philco Corp., Philadelphia. He joined the company in 1931. **John L. Esterhai**, named assistant secretary, joined the Philco Legal Department after service in World War II.

. . . **J. Henry Gardner** joined Jones & Laughlin Steel Corp., Pittsburgh, as administrative assistant to the director of public relations and advertising. He had been with American Radiator & Standard Sanitary Corp. **William J. Troppman**, a staff assistant, was promoted to supervisor of product advertising and promotion, and **Eugene F.**


CASH IN NOW ON CONCORD'S
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...and that's not all...
YOU WILL RECEIVE A SURPRISE FREE GIFT...

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SAMPLE "FESTIVAL OF BARGAINS" SPECIAL

$125 PUSH BUTTON 6 Volt DELCO RADIO
• 8 Tube Circuit
Reg. $125.00 Only $29.95

with 9 section 82" Solid Brass Whip Antenna. Measures Only 14" collapsed. Worth $9.20

• Ideal for Cars, Boats, Trucks, Tractors, Farms, Summer Camps
• Push-Pull 6V6 Output!

There is no finer automobile radio made than GENERAL MOTORS DELCO Radio. Designed originally for use in 1953 and 1954 Packard automobiles, this DELCO Select-O-Matic is small enough and of the right size and shape to fit into the dash of almost any 1951,1952,1953 or 1954 General Motors car. Has 5 Push-Buttons in addition to manual tuning control. Tube line-up includes 2–6SK7, 2–6V6G, 1–6SQ7, 1–6SA7 and 1–0Z4. Large 6 x 9" speaker, push-pull 6V6 output and wide range tone control guarantee that this radio will outperform any competitive radio on the market. Size 9" H. ' x 10" L. x 7½" Max. Depth. Control Head is 4⅞" long x 1⅞" high x 2" Max. Depth. Control Shaft centers are 6-11/16" apart and require ½" diam. holes. Shpg. wt. 19 lbs. Complete with owners' installation manual, all necessary hardware, brackets and knobs. With tubes, less escutcheon.

Stock No. P8TP .....Reg. $125.00.....Only $29.95

DELCO 9 Tube SELECT-O-MATIC AUTO RADIO

Reg. $135.00

9 tube DELCO Custom Auto Radio with Automatic Station Selection in addition to Push-Button and Manual Tuning!! Includes all the excellent features described above Makes an ideal truck radio. Driver need not take eyes from road in order to change stations. Tubes include: 2–6BA6; 2–6AV6; 2–6V6GT; 1–6BE6; 1–12AU7; 1–0Z4 Rect.

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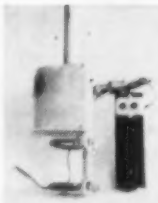

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Uses 2 standard Flashlight Cells. Operates either direction on 2 wire Lamp Cord. Top Mast ready to mount any balanced single Bay Antenna not a toy. Ideal for conicals, QTs, Rainbows, etc. Return if not 100% pleased! Jobbers—Dealers write for more information. Send cash check or M.O.

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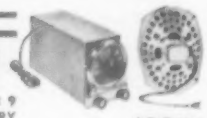
SUPERHETERODYNE • BIG 4 x 9 INCH SPEAKER • LOW BATTERY DRAIN • EASY INSTALLATION PERMEABILITY TUNER



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Changes dull eye-straining black and white pictures into beautiful color tones. Seconds to attach. No tools used. Helps eliminate glare and snow in fringe areas. Order direct. Send $1 for screen size up to 16", $1.25 size 17", $1.50 size 20", $2 size 21", $2.50 size 24", $3 size 27". We pay postage except on C.O.D. orders. Satisfaction guaranteed. Inquiries from dealers also welcomed.

Zingo Electronics, Johnstown 13, New York

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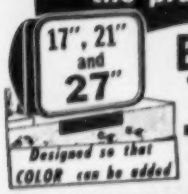
the practical way--

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*THIS MODEST INVESTMENT gets you started on a most fascinating project — assembling the new "E" type Transvision TV Kit in easy stages. For $15 you get PACKAGE #1 (standard first package for all new "E" kits). This package gives you the BASIC CHASSIS and required first-stage TV COMPONENTS, with complete instructions. When ready, you order the *next stage* (pkg. #2), etc.

ONLY $15.00 gets you started*

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2. Save up to 50%
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PEOPLE *(Continued)*

**Jannuzi**, also a former staff assistant, was named supervisor of product publicity and institutional advertising.

. . . **Leslie F. Muter**, president of Muter Co., Chicago, was awarded the 1955 RETMA Medal of Honor at its 31st Annual Convention Dinner in Chicago.

. . . **B. B. Bauer**, vice president and director of research of Shure Brothers, Chicago, received the first Professional Group on Audio Achievement Award of the IRE at its Spring National Convention.

. . . **Gen. Benjamin W. Chidlaw**, U. S. Air Force retired, joined Thompson Products, Cleveland, as vice president.

. . . **Dwight C. Baum**, vice president of the First California Co. was elected a director of Phaostrom Co., South Pasadena, Calif. END

## CORRECTIONS

The single-engine plane on the first page of the article "Servicing Light Plane Radios" in the July issue is a Swift and not a Piper as stated in the caption. On the third page of the article, the photo showing the panel of an Aero Commander was inverted in some of the first issues off the presses.

These errors were spotted by Fred R. Wilson of Pinehurst, N. C., and Robert Matthews of Fort Dodge, Iowa, two sharp-eyed readers who know their planes.

The ⅓- and ¼-watt diagonals are transposed on the resistor wattage chart in the article "How Much Will a Resistor Take" on page 56 of the July issue. We thank C. K. Well of Vallejo, Calif., for this correction.

Mr. Coates reports that the cutting templates illustrated on the third page of his article "A New Loudspeaker Enclosure" (page 32 of the June issue) should be drawn on a grid of ½-inch squares instead of ⅝-inch squares as specified on the drawing. END

## Radio Thirty-Five Years Ago

**In Gernsback Publications**

**HUGO GERNSBACK**
*Founder*

| | |
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| Modern Electrics | 1908 |
| Wireless Association of America | 1908 |
| Electrical Experimenter | 1913 |
| Radio News | 1919 |
| Science & Invention | 1920 |
| Television | 1927 |
| Radio-Craft | 1929 |
| Short-Wave Craft | 1930 |
| Television News | 1931 |

Some of the larger libraries still have copies of ELECTRICAL EXPERIMENTER on file for interested readers.

**In September 1921 *Science and Invention* (formerly *Electrical Experimenter*)**

Dempsey-Carpentier Fight via Radiophone, by Arthur H. Lynch
British Fliers Use Radio
Resonance Wave Coil Antennas, by J. O. Mauborgne, Major, S.C., and Guy Hill, Capt., S.C.
Radiophone and C.W. Set That Works, by Robert E. Lacault


## OPPORTUNITY ADLETS

Rates—45c per word (including name, address and initials). Minimum ad 10 words. Cash must accompany all ads except those placed by accredited agencies. Discount, 10% for 12 consecutive issues. Misleading or objectionable ads not accepted. Copy for November issue must reach us before Sept. 15, 1955.

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COMPLETE HIGH SCHOOL at home in spare time with 58-year-old school; texts furnished; diploma; no classes; booklet free. Write American School, Dept. X69, Drexel at 58th, Chicago 37, Ill.

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TAPE RECORDERS, ACCESSORIES. BEST BUYS. Boynton Studio, 10 E. Pennsylvania, Tuckahoe, N.Y.

BUY Surplus Radio, Electronic Equipment direct from Government. List $1.00. Box 169RAC, East Htfd 8, Conn.

$200 WEEKLY CLEANING Venetian Blinds. Free book. Burtt, 2434BX, Wichita 13, Kansas.

SPEAKER RECONING: Guaranteed workmanship. C&M Recone Co., 255 Tioga St., Trenton 9, N.J.

GEIGER COUNTER KITS $34.50. Geiger Counter & Scintillator Diagrams Catalog Free. R. F. Chambers, 13833 San Antonio Dr., Norwalk, Calif.

RCA, Motorola, Link, GE and Kaar new and used two-way radio equipment bought and sold. Communications Associates, 138-17 Springfield Blvd., Springfield Gardens, N. Y. Phone LA 7-2727.

ALL Types TV tuners serviced within 36 hours. For information write DAN'S TV Laboratory, 2 West 183d St., N.Y. 53, N.Y.

PRINTED Circuits made from your drawings. J. C. Devlin, Trucksville, Pa.

DIAGRAMS FOR REPAIRING RADIOS $1.00. Television $2.00. Give Make, Model. Diagram Service, Box 672-RE, Hartford 1, Conn.

FOUR Gold Plated microphone buttons; Hundred insulated carbon resistors; 6VDC 10 R.P.M. motor or earphone for $1.00 Postpaid. Electronic Outlet, Box 72-A, Lawrence, Mass.

$12.00 BUYS LONG DISTANCE FM ANTENNA NOW 60% OFF. Electronic Supply Co. 128 State St., Schenectady, N.Y.

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U. S. CIVIL SERVICE JOBS: Men-Women, 18-55. Start high as $350.00 month. Qualify NOW! 16,000 jobs open. Experience often unnecessary. Get FREE 36-page book showing jobs, salaries, requirements, sample tests. WRITE: Franklin Institute, Dept. G-54, Rochester, N.Y.

TUBES—TV, RADIO, TRANSMITTING, AND SPECIAL PURPOSE TYPES BOUGHT, SOLD AND EXCHANGED. Send details to B. N. Gensler W2LNI, 512 Broadway, N.Y. 12, N.Y.

WANTED: AN/APR-4, other "APR", "TS-", "IE-", ARC-1, ARC-3, ART-13, BC-348, etc. Microwave Equipment. Everything Surplus. Special tubes, Tec Manuals, Lab Quality Equipment, Meters. Fast Action, Fair Treatment. Top Dollar! Littell, Fairhills Box 26, Dayton 9, Ohio.

COUNT without numbers. Logic Mirror-wise. 4 pages. Send 25c. W. J. Mallory, 616 N. 34th St., Omaha 5, Neb.

SPEAKER RECONING, low prices. Michigan Speaker Reconing Service, 930 Metropolis, Marine City, Michigan.

DIAGRAMS: Professional Model Timers, Counters, Intercoms, Organs, etc. $1.00 each. List free. Parks, 101 S.E. 57th, Portland 15, Oregon.

POWER TRANSFORMERS REBUILT—all makes. TV-Radio or Special. Red Arrow Radio, 924 Metropolis, Marine City, Michigan.

25-50% DISCOUNT, guaranteed, Factory Fresh LP records; 69c and up; pre-recorded tapes. Send 20c for catalogue. SOUTHWEST RECORDS, 1108 Winburn, Houston, Texas.

FREE TRANSISTOR Code practice oscillator kit. See our ad in this issue — or write TRANS-AIRE ELECTRONICS, INC. 149 Broadway Dept. R New York 6, N.Y.

TELEVISION RECEIVERS $28.80 UP. W1APT 1420 South Randolph, Arlington 4, Va.

TV TRADE-IN SETS. Philco, R.C.A., Emerson, others. List available. 10"—$17. 12" to 17"—$20 up. Washtek Service Co., Dept. E, 956 Southern Blvd., Bronx, N.Y.

TV FM ANTENNAS. ALL TYPES INCLUDING UHF. Mounts, accessories. Lowest prices. Wholesale Supply Co., Lunenburg 2, Mass.

# Business

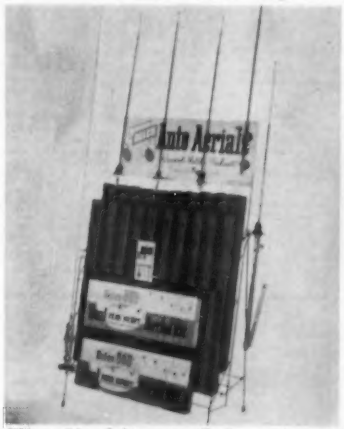
## Merchandising and Promotion

**Simpson Electric Co.**, Chicago, designed a new display board on which

an actual sample of its *Midgetester* model 355 miniature volt-ohmmeter is mounted.

**Permoflux Corp.**, Chicago, announced that its new Stereo-Vox device for simulating stereophonic reproduction from monaural sources has met with considerable success and that the company is planning a full-scale advertising and promotion program on its product.

**United Motors Service**, Division of General Motors, Detroit, Mich., designed a new sales stand capable of




holding 30 of its new *Delco* automobile aerials.

**Jensen Industries**, Forest Park, Ill., designed a new combination needle storage and display cabinet to aid its

distributors and dealers in stocking and selling its phono needles.

**Carter Motor Co.**, Chicago, developed a converter selector chart for wire and tape recorders.

**JFD Manufacturing Co.**, Brooklyn, N. Y., introduced its new *Liberty Bell* antenna at a service meeting in Phila-

**Left. to right: Doug Carpenter, JFD; Al Haas, CRTSA, Philadelphia; Paul F. Harran, WPFH-TV, Wilmington, Del., H. Grassley, JFD Eastern sales manager.**

delphia. The new antenna features a bi-directional response and was designed specifically for the Philadelphia area.

**CBC Electronics**, Philadelphia, is merchandising its high-fidelity interconnecting cables on a rotating counter display merchandiser.

**Kay-Townes Antenna Co.**, Rome, Ga., is sponsoring a Golden Harvest promotion campaign on its *Big Jack* and other antennas for its dealers and their salesmen. A 1956 Cadillac sedan is the first prize.

**Clarostat Manufacturing Co.**, Dover, N. H., is featuring a card kit which holds a selection of its power resistors.

## Production and Sales

**RETMA** reported the production of 3,238,820 TV sets during the first five months of 1955 compared with 2,301,055 for the 1954 period. Also 5,853,954 radios were manufactured compared with 4,048,904 in the 1954 period.

**RETMA** reported manufacturers' sale of 4,207,129 TV picture tubes and 185,682,583 receiving tubes during the first five months of 1955 compared to 3,275,301 picture tubes and 134,677,745 receiving tubes in 1954.

**The NBC Research and Planning Department** reported that there were 36,100,000 TV sets installed in the United States as of June 1.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ALL-PURPOSE FIL. TRANSFORMER
For Model Trains, Welding, Transmitters, etc.
PRI. 117 v. 60 cyc. sec.
6.4 v. ..... 12A
6.4 v. ..... 10A
5 v. ..... 3A
5 v. ..... 3A
5 v. ..... 3A
2.5 v. ..... 1.75A
$4.95

MYSTERY PACKAGE ELECTRONIC PARTS
The Surprise of Your Life
20 pounds of BRAND NEW USABLE GOVT SURPLUS Ideal gift for the ham, etc. Worth $50. Our price
$3.95

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Over 1,000 pieces, 2½ lbs. of assorted RADIO & TV HARDWARE
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KIT 5, RESISTORS
100 ASSORTED TYPES. Range from 1 ohm to 15 meg. ½ to 5 watts.
$1.75

KIT 2, CERAMICONS
100 ASSORTED Range from .75 mmfd. to 6,000 mmfd.
$2.50

KIT 6, R.F. CHOKES
25 ASSORTED Range from .5 mh. to 25 mh.
95c

Kit 3, Volume Controls
25 ASSORTED Range from 2 ohm to 3 meg. Some with switch.
$2.75

KIT 7, TOGGLE & SLIDE SWITCHES
25 ASSORTED DPST, DPDT SPST, etc.
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Kit 4, Rotary Switches
25 ASSORTED TYPES. A Real Buy at only
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KIT 8, PAPER & CAN CONDENSERS
25 ASSORTED Range from 4 mfd. 150 v. to 80 mfd. 450 v.
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BUTTERFLY COND.
TYPE A Freq. Range 106 to 330 MC. 4½" diameter Aluminum plates (open loop type with acorn socket mounted on stator).
TYPE B Freq. Range 135 to 485 MC. 4½" DIAMETER. Silver plated brass plates.
TYPE C Freq. Range 300 to 1000 MC. 2½" diameter. Can use 1616AS Tube. Silver Plated.
TYPE D Freq. Range 300 to 1000 MC. 2½" diameter. Has clip for Xtal Detector.
Note: The wide frequency range available. These units made the finest tuners for ultra-high frequency transmitters, receivers, frequency meters and oscillators.
Your Choice $4.95

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Uses UTC. Transformer and Western Electric Mike. Ideal for Hams, PA. CAP, Recording, Mobile Equip.
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Diagram Furnished
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RELAY SPECIALS
D.P.D.T. 3 VDC. DC Res. 11 ohms ..... $1.45
D.P.D.T. 110 VAC 6 Amp Contacts ..... 1.69
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Plate Sensitive Relay 7½ Ma. 2000 ohm coil ..... 1.95

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## Calendar of Events

**19th Annual Instrument Conference and Exhibit,** Sept. 12–16, Shrine Exposition Hall and Auditorium, Los Angeles, Calif.

**RETMA Symposium on Automation,** Sept. 26–27, Irvine Auditorium, University of Pennsylvania, Philadelphia, Pa.

**High-Fidelity Show,** Sept. 30–Oct. 2, Palmer House, Chicago. (RADIO-ELECTRONICS will exhibit in Room 746.)

**National Electronics Conference,** Oct. 3–5, Hotel Sherman, Chicago.

**Audio Fair,** Oct. 13–16, Hotel New Yorker, New York City. (RADIO-ELECTRONICS will exhibit in room 716.)

**1955 Radio Fall Meeting,** Oct. 17–19, Hotel Syracuse, Syracuse, N. Y.

**First Annual Technical Meeting of the IRE Professional Group on Electron Devices,** Oct. 24–25, Shoreham Hotel, Washington, D. C.

## New Plants and Expansions

**Sylvania Electric Products,** Parts Division, is planning a new 110,000-square-foot plastics plant and warehouse in Warren, Pa.

**Allen B. Du Mont Laboratories,** Clifton, N. J., formed a new Technical Products Division under the direction of Dr. P. S. Christaldi, former manager of the Instrument Division. It will make and sell products formerly handled by the Instrument and Communication Products Divisions. Du Mont is also building a new West Coast headquarters in Los Angeles.

**Vokar Corp.,** Dexter, Mich., is tripling its present plant area to house its enlarged Engineering and Research Departments.

**RETMA** has moved its West Coast office to larger quarters at 7046 Hollywood Blvd., Hollywood, Calif., and its Statistical Department to the Sheraton Building, 711 14th St. N. W., Washington, D. C.

**Service Instruments Co.** is now located at larger quarters in Addison, Ill.

**National Co.,** Malden, Mass., has leased additional space in Melrose, Mass., for its physics and pulse devices laboratories. Within the past year the company has more than doubled its engineering staff.

**Westinghouse Electric** is building an "automatic" factory at Youngwood, Pa., for the production of semiconductor devices.

**Motorola** Communications and Electronics Division has broken ground for a new $1,500,000 transistor manufacturing facility in Phoenix, Ariz.

**James Vibrapowr Co.,** Chicago, is building a new one-story factory which will triple its present space.

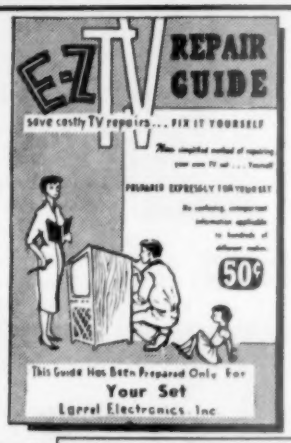
## Mergers

**Siegler Corp.,** Centralia, Ill., purchased the outstanding stock of **Hallamore Manufacturing Co.,** Long Beach, Calif., manufacturer of electronic devices.

**F. L. Jacobs Co.,** Detroit, automotive parts manufacturer, acquired **Eicor Co.,** Oglesby, Ill., as an electronic product subsidiary.

**Consolidated Electronics Industries**

EDLIE for TOP VALUES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save costly TV repairs... FIX IT YOURSELF
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Larrel's E-Z TV REPAIR GUIDE

*The Only FIX-IT-YOURSELF Guide Made expressly for YOUR TV Set!*

Now you can save costly TV repairs with this new, simplified method which includes all necessary data for just YOUR set. No confusing, unimportant information applicable to hundreds of other makes. Simplifies detection of faulty tubes in your TV receiver quickly, accurately.

It's a terrific idea—It's a terrific guide! Order today and have your set back in perfect condition at once. Be sure to send us make and model of your TV when ordering.

*For Most TV Sets—Old & New*

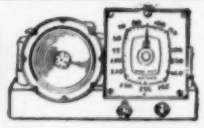
only 50¢

SAVINGS ON KITS

5 TUBE AC/DC Superhet Kit

Kit #1: 5 tube superhet kit, AC/DC includes all quality components required to construct this latest design, highly sensitive superhet broadcast receiver, complete with black, glistening bakelite cabinet (excludes wire & solder). Kit of 5 tubes, 12AT6, 2-12BA6, 12BE6, 35W4, 50B5.

Price, Less Tubes ..... $7.95
Extra for Tubes ..... $3.25



6-TUBE RADIO KIT

Kit #2: Low priced 6-tube kit designed for extra high sensitivity, excellent selectivity and good, rich tone quality. Uses 25L6, 25Z6, 6SQ7, 6SA7, 2-6SK7 in an easily constructed circuit. Includes all parts: punched chassis, resistors, condensers, coils, sockets, PM speaker, hardware, etc.

Special closeout price. (Less tubes & cabinet) ..... $6.95
Matched set of 6 tubes for kit ..... $3.25

3-Way Portable RADIO KIT AC/DC Batteries

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1X2, 1N5, 2A5, 2A6, 5W4, 6A8, 6AL5, 6AT6, 6AU5, 6AV6, 6AQ5, 6BJ7, 6BA6, 6BA7, 6BC5, 6BE6, 6C6, 6CB6, 6D6, 6J5, 6K6, 6SJ7, 6SN7, 6SQ7, 7A7, 7AG7, 7B6, 7B8, 7C5, 7C7, 7C6, 12AV6, 12Q7, 12AU6, 12BA6, 12SN7, 12SQ7, 25L6, 35/51, 35B5, 50B5, 50C5, 35, 45, 71 or 77 ..... ea. 49c

1LA4, 1LA6, 1LE3, 1R5, 1S4, 1T4, 3S4, 3V4, 6A7, 6AG5, 6N7, 12AU7, 12A7, 12BH7, 12SK7, 35Z5 or 58 ..... ea. 59c

0C3, 0D3, 1LC6, 1LH4, 1N5, 2A3, 3Q5, 5T4, 6AS7, 6AC7, 6AG7, 6AK5, 6E5, 6J8, 6L6, 6T8, 7G7, 6907, 12AT7 or 47 ..... ea. 69c

**TUBE CARTONS** ..... Colored or white; prices per 100: Min (1 x 2¼)—$1.20. GT (1¾ x 1¼ x 3¼)—$1.45. Med (1¼ x 1¼ x 4¼)—$1.65. Large (2 x 2 x 5)—$1.98.

**5 RPH HAYDON TIMING MOTOR** (O.D. 2" x 1⅛") ..... CCW rot. 24V 60 cycle ..... 1.95

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BUSINESS *(Continued)*

**Corp.**, Waterbury, Conn., purchased **Alliance Manufacturing Co.**, Alliance, Ohio, following stockholder approval. **Peoples Development Co.**, Columbus, Ohio, acquired a sizable stock interest in Consolidated.

**Stromberg-Carlson**, Rochester, N. Y., merged into **General Dynamics Corp.** following the approval of shareholders of both companies.

**Olympic Radio & Television**, Long Island City, N. Y.; **Victoreen Instrument Co.**, Cleveland, and **Nuclear-Electronics Corp.**, New York City, are planning a three-way merger subject to the approval of stockholders. David H. Cogan, president of Nuclear-Electronics, will be president and director of the new firm. C. W. Haller, president of Victoreen, will become vice president and director and Adolphe A. Juviler, chairman of Olympic, will become chairman and treasurer.

**Shure Brothers**, Chicago, manufacturer of microphone and acoustic devices, is celebrating its 30th anniversary this year.

## Business Briefs

. . . **Hoffman Electronics Corp.**, Los Angeles, purchased **National Fabricated Products**, Chicago electronic component manufacturer.

. . . **The 1956 IRE Show** will again be held in the Kingsbridge Armory and Palace, New York City, March 19–22, due to the delay in construction of the New York Coliseum.

. . . **Allen B. Du Mont Laboratories**, Clifton, N. J., entered the radio and high-fidelity phonograph field.

. . . **Acro Products Co.**, Philadelphia, was issued a patent on its *Ultra-Linear* audio amplifier circuit. The company is arranging for licensing agreements with several high-fidelity amplifier manufacturers.

. . . **RETMA** Service Committee Chairman H. J. Schulman, CBS-Columbia, estimated that the public had paid over $1.5 billions for radio–TV service during the past 12 months. This is the first time gross income from servicing has equaled or exceeded income from retail sales.

. . . **Daystrom Inc.**, Elizabeth, N. J., (parent company of Weston Electrical Instrument and Heath Co.), spent over $5 millions for the acquisition of new companies during the fiscal year ending March 31, 1955, and retired $1,419,000 in long-term debts. Thomas Roy Jones, president of the company, estimated that 70% of the firm's sales this year would be in electronic and allied equipment.

. . . **Phaostron Co.**, South Pasadena, Calif., has established a sales target of 10 times the present volume within the next 3 years due to new products scheduled to be introduced shortly.

. . . **Perfection Mica Co.**, Chicago, formed a new Magnetic Shielding Division.

END


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● All Tubes Individually Boxed ● 400 Types Always In Stock
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| 1B3GT | .73 | 6AU6 | .49 | 7H7 | .79 |
| 1LA4 | .59 | 6AU7 | .61 | 7J7 | .79 |
| 1LA6 | .69 | 6AV5GT | .83 | 7K7 | .69 |
| 1LC5 | .59 | 6AV6 | .49 | 7N7 | .69 |
| 1LC6 | .79 | 6AX4GT | .65 | 7Q7 | .66 |
| 1LE3 | .59 | 6AX7 | .64 | 7S7 | .79 |
| 1LG5 | .69 | 6BA6 | .49 | 7T4 | .69 |
| 1LH4 | .69 | 6BC5 | .54 | 12A4 | .60 |
| 1LN5 | .59 | 6BC7 | .82 | 12AL5 | .37 |
| 1R5 | .59 | 6BE6 | .51 | 12AQ5 | .52 |
| 1S5 | .51 | 6BG6G | 1.25 | 12AT6 | .41 |
| 1U4 | .57 | 6BH6 | .53 | 12AT7 | .72 |
| 1U5 | .50 | 6BJ6 | .49 | 12AU6 | .46 |
| 1X2A | .68 | 6BK5 | .80 | 12AU7 | .60 |
| 2AF4 | .98 | 6BK7 | .80 | 12AV6 | .39 |
| 3A3 | .80 | 6BL7GT | .91 | 12AV7 | .73 |
| 3AL5 | .42 | 6BN6 | .74 | 12AX4 | .67 |
| 3AU6 | .46 | 6BQ6GT | .98 | 12AX7 | .63 |
| 3BC5 | .54 | 6BQ7 | .90 | 12B4 | .60 |
| 3BN6 | .74 | 6BZ7 | .90 | 12BA6 | .49 |
| 3CB6 | .54 | 6C4 | .40 | 12BE6 | .51 |
| 3Q4 | .59 | 6CB6 | .54 | 12BF6 | .39 |
| 3Q5GT | .68 | 6CD6 | 1.11 | 12BH7 | .63 |
| 3S4 | .58 | 6CF6 | .64 | 12BQ6GT | .99 |
| 3V4 | .58 | 6CR6 | .51 | 12BY7 | .65 |
| 4BQ7 | .90 | 6CS6 | .51 | 12BZ7 | .65 |
| 4BZ7 | .98 | 6H6GT | .41 | 12CR6 | .51 |
| 5AMR | .75 | 6J5GT | .48 | 12L6 | .51 |
| 5ANR | .78 | 6J6 | .64 | 12SA7GT | .65 |
| 5AT8 | .75 | 6K6GT | .45 | 12SJ7M | .67 |
| 5AW4 | .59 | 6L6 | .84 | 12SK7GT | .63 |
| 5J6 | .64 | 6Q7 | .45 | 12SL7GT | .57 |
| 5T4 | .79 | 6S4 | .48 | 12SN7GT | .59 |
| 5T8 | .81 | 6SA7GT | .55 | 12SQ7GT | .56 |
| 5U4G | .55 | 6SH7GT | .49 | 12V6GT | .46 |
| 5U8 | .78 | 6SJ7GT | .50 | 12X4 | .98 |
| 5V4 | .71 | 6SK7GT | .53 | 14A7 | .63 |
| 5V6 | .50 | 6SL7GT | .67 | 14B6 | .63 |
| 5X8 | .75 | 6SN7GT | .59 | 14B7 | .75 |
| 5Y3GT | .37 | 6SQ7GT | .46 | 19AU4 | .76 |
| 6AB4 | .46 | 6T4 | .99 | 19BG6 | 1.39 |
| 6AC7M | .86 | 6T8 | .80 | 19T8 | .86 |
| 6AD7 | .89 | 6U8 | .78 | 25AV5GT | .83 |
| 6AF4 | .90 | 6V6GT | .50 | 25BQ7GT | .98 |
| 6AG5 | .56 | 6V8 | .66 | 25CD6 | 1.49 |
| 6AG7M | .99 | 6W4GT | .47 | 25L6GT | .51 |
| 6AH4 | .67 | 6W6GT | .57 | 35B5 | .52 |
| 6AH6 | .73 | 6X4 | .37 | 35C5 | .51 |
| 6AK5 | .95 | 6X5GT | .37 | 35L6GT | .51 |
| 6AK6 | .59 | 6X8 | .75 | 35W4 | .47 |
| 6AL5 | .42 | 7A5 | .59 | 35Y4 | .54 |
| 6AM8 | .78 | 7A6 | .69 | 35Z3 | .59 |
| 6AN4 | .95 | 7A7 | .59 | 35Z5GT | .47 |
| 6ANR | .78 | 7A8 | .68 | 50A5 | .55 |
| 6AQ5 | .50 | 7AG7 | .69 | 50B5 | .52 |
| 6AQ6 | .46 | 7B7 | .69 | 50C5 | .51 |
| 6AQ7 | .70 | 7C5 | .69 | 50L6GT | .61 |
| 6AR5 | .45 | 7C6 | .59 | 80 | .43 |
| 6AS5 | .59 | 7C7 | .69 | 117Z3 | .45 |
| 6AS6 | 1.49 | 7E7 | .59 | 117Z6 | .82 |

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- In original Factory Cartons.
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- $85 seller.

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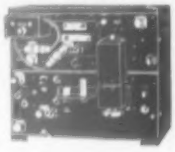

44 tube transceiver with usable parts, tube sockets, relays, coax fittings, condensers, resistors, etc. 24 volt Blower motor, 24V gear train motor. Power transformer 400 to 2400 cycles. Original govt cost $750.00. Less tubes $5.95 ea.

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EDITORIAL *(Continued)*

These totals are impressive. The electronics industry sold $1,400,000,000 in end products for entertainment purposes last year, and this year is expected to attain a volume equally large. But look ahead just a few years! The average annual sale of entertainment devices, we believe, will increase to over $1,600,000,000 a year during the 1958–60 period and by 1964 should come every close to $2,000,000,000, an increase of over 40% in a decade.

By far the largest customer of the industry is the United States Government.

Defense purchases of electronic equipment last year are estimated at $2,300,000,000, and the total may go up another notch to around $2,500,000,000 in 1955. But, as the Army, Navy and Air Force become increasingly electronified, we foresee Government purchases in the vicinity of $3,200,000,000 a year in the 1958–60 period and at over $4,000,000,000 a year by 1964.

There is one area of electronics in which the surface has been barely scratched, where most of the development work lies ahead and which some day will compare favorably with the others in dollar volume. That is the field of electronics equipment for industry, commerce and other nonentertainment, nonmilitary uses. The figures are not too impressive now: For instance, about $570,000,000 of sales in 1954 and an estimated $640,000,000 in 1955. But, by 1958–60, we anticipate annual sales in the industrial-commercial field will be running at the approximate rate of $900,000,000 and by 1964 the sales figure should be around $1,200,000,000 to $1,400,000,000, a gain of 130% in 10 years.

When all the foregoing is lumped together, it shows that the sale of all electronic end products in 1954 totaled about $4,300,000,000 and that this year the aggregate will be slightly higher. In another three years or so, over the 1958–60 period, we expect the end-product total to exceed $5,700,000,000, an increase of 33%, and that by 1964 electronic end products totaling about $7,400,000,000 will be sold. That means an increase—witnin the decade—of more than 70%.

After considering all the end products manufactured in the electronics industry, there still remains a sizable business in the production and sale of components for repair, which amounted to a volume of $670,000,000 last year and which will continue to grow as more and more end products are placed in use. These components include such things as tubes of various types, capacitors, transformers, resistors, speakers, dials, knobs, etc. It is estimated that repair parts sales this year will fall not far short of $800,000,000, while in 1958–60 the total should reach $1,250,000,000. By 1964, we expect this total to be in the neighborhood of $2,300,000,000, an increase of nearly 250% in a decade.

These revenues exceeded $2,000,000,000 in 1954 and will be on approximately the same level in 1955. By 1958–60, "markup" is expected to pass $2,800,000,000 and should rise to around $4,200,000,000 in 1964. At the same time, repairmen's service charges are expected to show a gradual increase from $925,000,000 this year to $1,400,000,000 10 years from now.

To round out the picture of the electronics industry, we must consider the broadcasting end of the business from the point of view of revenue. Television and radio broadcasting revenue in 1954 amounted to about $1,140,000,000 and shows a slight increase this year. It is predicted, however, that they should average around $3,000,000,000 by 1958–60 and at the end of the 10-year period are expected to top $5,000,000,000.

**Thus we see that from the standpoint of sales and revenues, the electronics industry is today virtually a $9,000,000,000 industry. In the three-year period, 1958–60, total sales will come close to $14,000,000,000 a year. And, 10 years from now, in 1964, we are positive we will be justified in calling electronics an industry with sales and revenues totaling over $20,000,000,000 a year.** END

# technical Literature

### WIRE CATALOG

*Catalog 105* covers a complete line of electrical wire, cord sets, television wire and cable and wire accessories in 36 pages.

*Columbia Wire & Supply Co., 2850 Irving Park Rd., Chicago 18, Ill.*

### INDUSTRIAL SOUND

*How RCA Sound in Industry Gets Things Done (Form 3R2478)* is a 12-page brochure describing and picturing a number of sound applications and RCA microphones, amplifiers, control cabinets and speakers.

*Engineering Products Div., Bldg. 15-1, Radio Corp. of America, Camden, N. J.*

### SMALL MOTOR SWITCHES

*Publication EC-79*, a 14-page catalog, describes Cutler-Hammer's line of toggle, rotary, door-operated, push-button, automotive, aircraft and miscellaneous switches.

*Cutler-Hammer, Inc., Milwaukee 1, Wis.*

Any or all of these catalogs, bulletins, or periodicals are available to you on request direct to the manufacturers, whose addresses are listed at the end of each item. Use your letterhead—do not use postcards. To facilitate identification, mention the issue and page of RADIO-ELECTRONICS on which the item appears.

UNLESS OTHERWISE STATED, ALL ITEMS ARE GRATIS. ALL LITERATURE OFFERS ARE VOID AFTER SIX MONTHS.

### TRANSFORMERS

Audio transformers for tubes and transistors, including miniature, subminiature and microminiature, as well as filament, scope, power and vibrator and special transformers; filter reactors, etc. are described in a 12-page catalog.

*Microtran Co., 84-11 Rockaway Beach Blvd., Rockaway Beach, N. Y.*

### CLAROSTAT CONTROLS

*Catalog No. 55*, 28 pages, describes Clarostat's complete line from attenuators to wire-wound controls. Dimensioned drawings, complete technical data, basing diagrams of wire-wound ballast resistors and miscellaneous information are provided.

*Clarostat Mfg. Co., Inc., Dover, N. H.*

### INTERFERENCE ELIMINATION

*Suppressing Radio Interference with Metex Electronic Weatherstrip and R.F. Gaskets* is the title of a 16-page brochure that discusses practical and effective methods of r.f. shielding, using a special knitted braid which makes joints "r.f.-tight."

*Electronics Dept. Metal Textile Corp., Roselle, N. J. Attn.: G. P. Schreiber.*

### ANTENNA CATALOGS

Three catalogs carry information on the RMS line of TV antennas and accessories. *Catalog 55B* is a 29-page annual catalog of all RMS antennas, completely indexed and bound in 2-color cover. *Catalog 55K* describes the company's line of indoor antennas, and *Catalog 55W* is a chart highlighting a number of antennas and accessories. Intended for use as a wall chart, it is printed in three colors.

*Radio Merchandise Sales Inc., 2016 Bronxdale Ave., New York 62, N. Y. Attn.: Clifford Shearer.*

### ELECTRO-VOICE CATALOG

*Condensed Catalog No. 123* describes the company's full line of microphones for professional, amateur and special use, E-V speakers, enclosures and high-fidelity cartridges. Included is information on the Circlotron amplifier, the Compound Diffraction projector and the RME line of communications products.

*Electro-Voice, Inc., Buchanan, Mich.*

### HIGH FIDELITY

Data on speaker enclosures, coaxial and full-range loud-speakers, speaker systems, horns, networks and theatre installations is contained in *Catalog 55*. It is made up of five separate looseleaf sections in a cover with folded ends that form a pocket.

*Stephens Mfg. Corp., 8538 Warner Dr., Culver City, Calif.*

### SPEAKER SYSTEM

Four-page brochure describes the Villchur speaker system. It includes a brief description of the acoustic suspension principle, performance curves on both frequency response and harmonic distortion, model numbers and prices.

*Acoustic Research, Inc., 23 Mt. Auburn St., Cambridge 38, Mass.* END

## CORRECTION

Several readers have pointed out that there is no a.v.c. circuit in the *Midgetape* pocket tape recorder whose diagram appears on page 37 of the June issue. The manufacturer's engineers inform us that the first hundred or so Midgetapes produced had a.v.c., but this feature was discontinued in later production.


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| TYPE | PRICE | TYPE | PRICE | TYPE | PRICE | TYPE | PRICE |
|---|---|---|---|---|---|---|---|
| 0Z4 | .45 | 6AL7GT | .70 | 6SA7GT | .50 | 12SH7 | .47 |
| 1B3GT | .79 | 6AS5 | .50 | 6SC7 | .50 | 12SJ7GT | .50 |
| 1L4 | .56 | 6AS6 | 2.00 | 6SG7 | .43 | 12SK7 | .50 |
| 1L6 | .60 | 6AS7G | 2.25 | 6SH7 | .45 | 12SL7GT | .69 |
| 1LA4 | .66 | 6AT6 | .40 | 6SJ7GT | .45 | 12SN7GT | .60 |
| 1LB4 | .66 | 6AU5GT | .70 | 6SK7 | .50 | 12SQ7GT | .44 |
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| 1V | .57 | 6BL7GT | .77 | 7A5 | .55 | 25Z5 | .38 |
| 1X2A | .79 | 6BQ6GT | .88 | 7A6 | .47 | 25Z6GT | .42 |
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| 2X2A | 1.00 | 6BY5G | .60 | 7B5 | .41 | 35C5 | .51 |
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| 3Q4 | .62 | 6C6 | .50 | 7C4 | .40 | 35Y4 | .40 |
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| 3V4 | .65 | 6CD6G | 1.18 | 7C6 | .45 | 35Z5GT | .39 |
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| 6AK5 | .80 | 6S4 | .48 | 12BY7 | .68 | 117Z6GT | .65 |
| 6AL5 | .44 | 6S7G | .47 | 12SA7 | .52 | | |

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# Books

**ELECTRONIC CIRCUITS, by Thomas L. Martin, Jr. Prentice-Hall, Inc., 70 5th Ave., New York, N. Y. 5½ x 8½ inches, 707 pages. $12.**

Intended for college students, engineers and physicists, this book assumes knowledge of elementary calculus and electronics. Advanced mathematical methods are avoided but, as the author states, "it is unashamedly mathematical" and he feels "under no compulsion to apologize for this." He has done an excellent job in covering such a complex subject so clearly and completely.

The book has three parts. The introduction describes equivalent circuits and theory. Laplace transforms are introduced here to be used later in the book. The reader soon finds that these are not nearly as terrifying as they sound. The second part describes class-A circuits, for example; single and multistage tube amplifiers; transistors; feedback; etc. The last part includes chapters on switches, modulators, rectifiers, triggers, oscillators. A chapter on magnetic amplifiers also appears. —*IQ*

**COYNE TECHNICAL DICTIONARY. Published by Coyne Electrical School, Chicago. Distributed by Howard W. Sams & Co., Inc., 2201 E. 46th St., Indianapolis 5, Ind. 5½ x 8 inches, 160 pages. $2.**

It is disconcerting for a beginner or student of electronics to encounter technical terms he does not understand, and it helps his morale if such words can be looked up and clarified immediately. This dictionary contains 4,000 technical terms used in radio, TV, electronics and radar. They are explained clearly and completely. We noted that the latest color TV terms are well represented.

Naturally a book this size cannot include every possible word used in electronics. Superheterodyne is included but not superregeneration; tube but not transistor; Geissler tube but not Geiger counter; silicon but not germanium; carrier but not sideband. There are two and a half pages of terms beginning with "magnetic" but no sign of magnetic recording.

Much handy reference data appears at the end of the book. There are 45 pages of wire tables, transistor symbols, TV tube characteristics (up to 30-inch) and various charts.

**PRACTICAL ELECTROACOUSTICS, by Michael Regginger. Chemical Publishing Co., Inc., 212 5th Ave., New York, N. Y. 5¼ x 9 inches, 271 pages. $10.**

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technicians and engineers. Advanced hi-fi fans will find useful information also if they like theory and math.

The beginning chapters cover theory and characteristics of mikes and speakers. Next comes information on crossover networks and attenuators. A chapter on magnetic structures leads later to magnetic recording. There is nothing on amplifiers, but one chapter describes specifications of PA systems for churches, schools, hospitals, etc. The Hollywood Bowl system is chosen as an example of an outdoor installation.

One chapter gives suggestions for improving studio and home acoustics.

Only *tape* recording is covered here. The effects of various sizes and shapes of heads are shown, together with the variations due to bias, etc.

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**TRANSISTOR APPLICATIONS, published by Raytheon. Distributed by local Raytheon tube suppliers, or direct from Dept. P-7, Raytheon Mfg. Co., Tube Operations, 55 Chapel St., Newton 58, Mass. 8 x 11 inches, 116 pages. 50¢.**

Because of their small size and the simple circuits in which they operate, transistors are a "natural" for home experimenting. A corner of the kitchen table is ample space to build useful instruments and carry on interesting work. Thus, many amateurs and experimenters have done work with transistors and have developed practical devices using them. This book contains over 50 articles on actual transistorized equipment, written by experimenters for experimenters. Many are reprinted from leading radio magazines (including RADIO-ELECTRONICS).

These articles include timers, voltmeters, i.f. oscillators, modulators, a.f. filters, ham radio aids, and, of course, straight audio amplifiers. Each article contains detailed instructions and descriptions. The book should help and inspire experienced technicians as well as beginners.—*IQ*

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**ELEMENTS OF TELEVISION SERVICING, for Bench and Field, by Abraham Marcus and Samuel E. Gendler, Prentice-Hall, Inc., 70 5th Ave., New York, N. Y. 587 pages. $7.35.**

The field man will welcome the first servicing book to recognize him as an essential part of the servicing setup. For the term "bench and field" in the title means what it says. Section II of the book, running from page 59 to 212 and comprising Chapters 3, 4 and 5, is devoted to field servicing.

The next nine chapters deal with bench servicing of black-and-white receivers; three chapters on color TV and its service problems follow. Illustrations for the color servicing section are in full color. Two chapters in Section I describe the fundamentals of color television and reception, treating the TV signal from the viewpoint of the transmitter and receiver and describing the features and functions of the TV receiver.—*FS*

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BOOKS *(Continued)*

**PROBES, by Bruno Zucconi and Martin Clifford. Gernsback Publications, Inc., 25 W. Broadway, New York 7, N. Y. 5½ x 8½ inches, 224 pages. Soft-cover edition $2.50, hard cover $4.**

Sweeping aside the veil of mystery so long associated with this subject, a long step has been taken by the authors in exposing the probe in its every practical form. Taking nothing for granted, the text runs the gamut from the simple crystal detector as it demodulates AM signals to the Chromatic probe and its color TV applications.

The book discusses, individually, the many probe types applicable to electronics, while simultaneously integrating them so as to maintain a very interesting continuity. The probes discussed, chapter by chapter, include the simple crystal demodulator, voltage-doubler, balanced, low-capacitance, high-voltage, isolation and direct, specialized, Chromatic and vacuum-tube types.

The probes themselves form only part of the story. Each probe discussion is expanded to include the many applications, advantages and disadvantages of that particular unit with regard to various equipment. In addition, each probe is put to work. Radio and television waveforms and circuitry are plentiful, and the authors, ever mindful of the problems of the service technician, suggest numerous techniques, do's and don't's. The chapter on specialized probes covers the less common and infrequently used types.—*JK*

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**THE NEW HIGH-FIDELITY HANDBOOK, by Irving Greene and James R. Radcliffe. Crown Publishers, Inc., 419 4th Ave., New York, N. Y. 193 pages. $4.95.**

Described as a practical guide for the assembly, installation, maintenance and enjoyment of high-fidelity music systems, this is one of the few books written by people who know the subject and yet express the viewpoint of the lay listener to good music. The result is that the weight of the material sometimes falls in unexpected places. For example, the where and how of the installation process may well be the most important feature of the layman's adventure in high fidelity --and it gets corresponding recognition. Fifty pages are devoted to the subject, broken down into planning the installation, problems of fashion and interior decoration, and high-fidelity furniture.

The beginner is given—in the first 70 pages of the book—an idea of what high fidelity is, what components produce it and how they work. The advanced enthusiast will be interested in the chapter devoted to plans of speaker enclosures, as well as the material on constructing crossover networks in the appendix.

There are two introductions: "Deems Taylor on High Fidelity" and "Harold C. Schonberg on The High-Fidelity Record."—*FS* END

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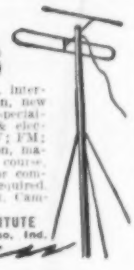

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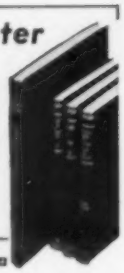

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# ADVERTISING INDEX

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| | |
|---|---|
| Alliance Mfg. Co. | 117 |
| Allied Radio Corp. | 15 |
| American Microphone Co. | 98 |
| American Phenolic Corp. | 128 |
| Approved Electronics | 129 |
| Arkay Radio Kits, Inc. | 136 |
| Astron Corp. | 23 |
| Atlas Sound Corp. | 148 |
| Audel Publishers | 163 |
| B & K Mfg. Co. | 151 |
| Barjay Co. | 124 |
| Bell Telephone Labs. | 26 |
| Blonder-Tongue Labs. | 98 |
| Book-of-the-Month Club, Inc. | 13 |
| Brooks Radio & TV Corp. | 127 |
| CBS-Hytron | 109 |
| Cabinart | 18 |
| Capitol Radio Engineering Institute | 103-104 |
| Channel Master Corp. | 17 |
| Chicago Standard Transformer Co. | 124 |
| H. G. Cisin | 132 |
| Cleveland Institute of Radio Electronics | 9 |
| Collins Audio Products | 126 |
| Concord Radio | 115 |
| Cornell-Dubilier Electric Corp. | 30-31, 160 |
| Coyne Electrical School | 139, 149, 156 |
| DeVry Technical Institute | 7 |
| Edlie Electronics | 158 |
| Electro Products Labs. | 152 |
| Electro-Voice, Inc. | 6, Inside Back Cover |
| Electronic Instrument Co. (EICO) | 32, 139 |
| Electronic Measurements Corp. | 133 |
| Erie Resistor Corp. | 152 |
| E-Z Way Towers, Inc. | 153 |
| Fenton Company | 141 |
| Finney Co. | 125 |
| G. & H. Wood Products Co. | 18 |
| General Cement Manufacturing Co. | 101 |
| Grantham | 161 |
| Heath Co. | 67-78 |
| Hershel Radio | 157 |
| Huckert Electronics | 146 |
| Hudson Radio & TV | 162 |
| Hughes Research & Development Labs. | 108 |
| Indiana Technical College | 144 |
| Instructograph Co. | 144 |
| Instruments for Service, Inc. | 148, 160 |
| International Rectifier Corp. | 16 |
| Jensen Industries | 148 |
| Jones & Laughlin Steel Corp. | 121 |
| Keltner Mfg. Co. | 155 |
| Kuehne Manufacturing Co. | 166 |
| Lafayette Radio | 167 |
| La Pointe Electronics | 131 |
| Leotone Radio Corp. | 159 |
| McGraw-Hill Book Co. | 166 |
| Major Brand Tube Co. | 147 |
| Mallory, P. R., & Co. | 123 |
| Merit Coil & Transformer Co. | 115 |
| Mosley Electronics | 146 |
| Moss Electronics Distributing Co. | 110-111 |
| Musical Masterpiece Society | 109 |
| National Electronics of Cleveland | 146 |
| National Radio Institute | 3, 19-20 |
| National Schools | 5 |
| Newark Electric Co. | 154 |
| Newcomb Audio Prod. Co. | 150 |
| Nordic Radio Co. | 155 |
| Opportunity Adiets | 156 |
| Oxford Electric | 130 |
| PermaPower Co. | 122 |
| Permo Inc. | 161 |
| PermaRux Corp. | 14 |
| Philco Corporation | 90-91 |
| Pickering & Co., Inc. | 12 |
| Precision Apparatus Co. Inc. | 150 |
| Prentice-Hall, Inc. | 164 |
| Progressive "Edu-Kits," Inc. | 134 |
| Pyramid Electric Co. | 10 |
| Quam-Nichols | 144 |
| Quietrole Co. | 162 |
| RCA Institutes, Inc. | 11, 99, 135 |
| Rad-Tel Tube Co. | 159 |
| Radiart Corp. | 30-31 |
| RCA Tube Div. (Radio Corporation of America) | 82 |
| Radio Receptor, Inc. | 143 |


## RADIO SCHOOL DIRECTORY PAGE 165


Baltimore Technical Institute
Candler System Co.
Capitol Radio Engineering Institute
Grantham School of Electronics
Indiana Technical College
Indianapolis Electronic School
Milwaukee School of Engineering
RCA Institutes, Inc.
Tri-State College
Valparaiso Technical Institute
Wayne School
Western Television Institute



| | |
|---|---|
| Radio-Television Training Association | 25 |
| Radion Corporation | 4 |
| Raytheon Manufacturing Co. | 27 |
| Reference Handbooks | 157 |
| Rek-O-Kut Co. | 140 |
| Rider, J. F., Publisher | 142 |
| Rinehart Books, Inc. | 110, 146, 154 |
| Rockbar Corp. | 158 |
| Rohn Manufacturing Co. | 93 |
| Sams, Howard W., & Co., Inc. | 21, 24 |
| School International Inc. | 163 |
| Seco Manufacturing Inc. | 131 |
| Shure Brothers, Inc. | 16 |
| Simpson Electric Co. | 97 |
| Sprague Products Co. | 28-29 |
| Stanburn Radio & Electronics | 164 |
| Stanley Electronics Corp. | 161 |
| Supreme Publications | 137 |
| Sylvania Electric Products, Inc. | 82-83, 89 |
| Tab | 166 |
| Technical Appliance Co. | 138 |
| Telecom | 164 |
| Teleparts Co. | 151 |
| Telvac | 146 |
| Telrex Inc. | 119 |
| Trans-Aire Electronics, Inc. | 151 |
| Transvision Inc. | 156 |
| Trio Mfg. Co. | 107 |
| Tung-Sol Electric Co. | 8 |
| Turner | 14 |
| U.S. Electronic Research & Dev. Corp. | 81 |
| Universal Television School | 151 |
| Vig Avionics Corp. | 157 |
| Ward Products Corp. | 114 |
| Weyco, Inc. | 95 |
| Webster Electric Corp. | 106 |
| Weston Electrical Instrument Co. | 22 |
| Wholesale Radio Parts Co. | 145 |
| Winegard Co. | 85 86 |
| Zingo Electronics | 158 |



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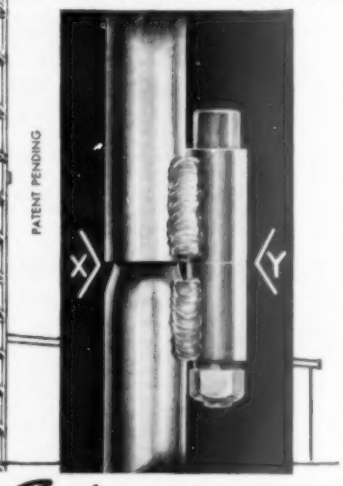


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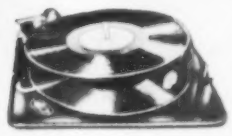

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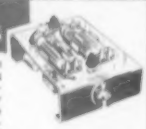

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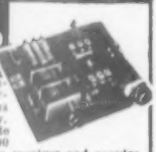

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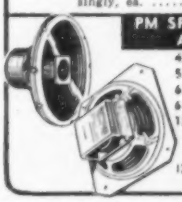

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50 Amp* ..... $59.00; 2 $112
100 Amp* ..... $108.00; 2 $210
15 Volt 2 Amps $1.98; 2 $3.50
Secondary (Dual†) 18-18-9-0-9-18-18 Volts (Windgs in Series at ratings shown; Parallel 2xAmps, Voltage ½ max * Dual Pri 115 & 220V 60 cy; Tapped 36VCT

**Write For New "TABTRON" Rectifier & Power Supply Catalog PR655**

### New Rectifier Chokes

| | |
|---|---|
| CR5001 1AMP/0.1HY/1.4R/3# | $3.95 |
| CR5002 2AMP/0.1HY/.67R/5# | $5.95 |
| CR5003 5AMP/.07HY/.6R/10# | $7.95 |
| CR5004 12AMP/.01HY/.1R/12# | $14.95 |
| CR5005 24A/.004HY/.025R/20# | $29.95 |

### 230 to 115V Autotformers

For 220-240 V/50-60 cy in. To 110-120 v or step-up. 1 w. Cord, Plug & Receptacle.

| | |
|---|---|
| TPA050/50W* | $2.55 |
| TPA075/75W* | $3.95 |
| TPA100/100W† | $4.00 |
| TPA200/200W† | $4.75 |
| TPA250/250W† | $7.75 |
| TPA300/300W† | $7.25 |

TPA500/500WSB 25, TPA750/750WSB $11.75
Model TPA1000/1000W/1KW ..... $15.95
Model TPA2000/2000W/2KW ..... $34.00
$100 Order Take 10% Disc. *Less C, P&R

### New Variable 0 to 6 & 12 Volt/12A DC Power Supply

Battery Eliminator, Charger, Model RR, Plater, Aircraft, Marine or any DC Req. Extra Hvy Duty Selenium Rectifier, 2 Meters V & A. Designed for Cont. Service & up to 20 Amps intermittent overload.

**New Model T612V12AC ....$29.95**

# TABTRON

## NEW HIGH CURRENT POWER SUPPLIES—ONE YEAR GTD

Variable 0-28VDC. Completely Built, Full Wave Selenium Rectifier, Transformer, Variac, Volt & Amp Meters, Switch, Terminals & Fuse, Housed in Heavy Duty Steel Cabinet. 115V/60cy Input 110 or 220V† and 3 phase to order. Specify

| Stk No | Cont. Rating | W. Meters |
|---|---|---|
| T28V5A | 0-28 VDC at 5 Amp | $ 45 |
| T28V5ACC | 5 Amp (5% Ripple) | $ 75 |
| T28V12A | 0-28 VDC at 12 Amp | $108 |
| T28V12ACC | 12 Amp (5% Ripple) | $145 |
| T28V24A† | 0-28 VDC at 24 Amp | $135 |
| T28V24ACC† | 24 Amp (5% Ripple) | $195 |
| T28V50A† | 0-28 VDC at 50 Amp | $260 |
| T28V50ACC† | 50 Amp (5% Ripple) | $370 |
| T28V100A† | 0-28 VDC at 100 Amp | $460 |

### New! Basic Supplies, 115 VAC in

| | |
|---|---|
| B115P5A | 115 WDVC at 5 Amp $90.00 |
| B115P10A | 115 VDC at 10 Amp 190.00 |
| B230P5A | 230 WVDC at 5 Amp 188.00 |
| B230P10A† | 230 VDC at 10 Amp 283.00 |

Less Meters. † 115 or 230 VAC and 3 Phase

### New Variable Voltage Xfmrs

| Superior—Gr—Staco—Utc | |
|---|---|
| 0-132V 1.25A | $ 7.99 |
| 0-135V 3A | 21.95 |
| Cased 0-135V 7.5A | 31.95 |
| Uncased 0-135V 7.5A | 17.25 |
| Cased 0-270V 3A | 24.95 |
| Uncased 0-270V 3A | 41.95 |
| Cased 0-135V 15A | 41.98 |
| Cased 0-270V 9A | 41.98 |

5% or more 10% Disc

### NEW! Quality VOLTAGE REGULATOR

**$ $ Popularly Priced $ $**
**ONLY $16.98**
LINE VOLTAGE STABILIZER
Automatically Regulates line voltage for TV, RADIO or Industrial use. Insures full life, strength, & sync of TV picture regardless of live voltage. Automatically operated . . . regulator turns on & off with set or equipment.
TROUBLE FREE, QUIET, needs no adjustment. Universal use from 100 to 300 watts. Input 100-125V/Output 115V plus or minus 5% 50-60 cy. SOLD WITH "TAB" MONEY BACK GUARANTEE
Order Six and Take 10% Discount

**Money Back Guarantee (Cost of Mdse. Only) $5 Min. Order F.O.B. N.Y.C. Add Shpg. Charges or for C.O.D. 25% Dep. Tubes Gtd. via R-Exp. only. Prices subject to Change Without Notice. Phone Rector 2-6245. CABLE: "TABPARTS"**

## OIL CONDENSER BUY

4MFD 1200 VDC or 10 MFD 600 VDC
**$1.25** Lots of 24
Or Any Assortment of 24
12 Lots @ $1.50 ea.; Singly @ $1.79

## TRANSFORMER SPECIAL

6.3 Volt 3½ Amp. CONTINUOUS DUTY
**95¢** ea. LOTS OF 25
115 VAC In, size 2-5/16H 2L 1¾W Hvy Duty, Channel Mtg, 8" Wire Leads
Lots of 12 @ $1.00 ea.; Singly @ $1.75 ea.

# SPECIAL "TAB" BARGAINS

Power Rheostat, 250 Ohm, 25 Watt ..... ea. .69; 10 for $5
856A Kit (2) 866A Tubes, Sockets and Transformer ..... Special @ $4.98
Feeler Gauge, Precision made, .003 to 0.05 ..... ea. .59; 2 for 98
Hookup Wire, Asstd. 5 Colors, 100 ft. /roll; 500 ft. @ $1.98 ea. ..... 6 for $10
Sound Power Headset, Chest & Throat Mike U.S.N. ..... Per Pair @ $30
Planetary Drive, 5:1&11to1 @ $2; 3 for $5
Microswitch Kit, Assorted @ 4 $1; 20 $4
GTD Vinyl Electric Tape, Hi Volt 2" x 30 ft. ..... @ .40 ea.; 6 $2
TV Cap 500 mmfd/20KV @ .49ea.;20for$10
Tubetester Socket Saver, 7, 8, 9 Pins ..... @ $1.60 ea.; 3 $4.50
Plastic Utility Boxes, Size 10¾" x 6.4" x 2¼", 1/12 18 Compartments @ $1.59 ea. ..... Any seven @ $10
Electrolytic 50mfd/350VDC Gtd. @ 5 for $1

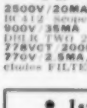
ORSA Wood Saw, Swedish Steel, non-breakable, double action cutting edge. Reg. $12 to $18 ea. ..... @ $4; 6 for $16
1-222-A Signal Generator, Xtal @ $59
Crystal Diode 1N21 @ .20; 100/$5
Clamp Lamp, Adjustable, w/Bulb & Reflector ..... @ $1.00
Wrench, INCA Quickie, 10 Way ¼" to 9/16" Sq. & Hex head nuts & bolts, rustproof, lifeproof @ .59; 10 $5
Vacuum Tube Data Relays, Octal base 28 or 120V @ $1.49; ass'td 10 @ ..... $12
RG59U 100 ft. @ $3; 500 ft. @ $22
300 Ohm Twinlex, 65 Mil Hvy Duty, 100 ft. @ $1.19; 1000 ft. @ $10.25
AB "J" Potentiometers, Ass'td Kit 12 popular values ..... @ 12/$4
Global Resistor, T2FD/3500 Ohm 50 Watt RF, w/clips ..... @ $2
Snooperscope, Infra Red Tubes ..... @ $6.99 ea.; 2 for $11
Mica Cap. .006 at 2500 WVDC @ .39; 4for$1

## DEALERS WRITE FOR DISCOUNTS

### MICRO & MU Switches Switchettes

A Mu/Leaf Sw. 3½" DPSO & NC 15A @ 50¢ ..... Special 12/$10
B Micro Sw. Pin Plunger SPDT/10A @ 39c ..... Special 12/$3
C Micro sw. Plung. SPDT/10A ..... 39; 10/$3
D Micro sw. Plung SPNO/10A ..... 35; 12/$3
E Push Tyle, AH&H DPST/12A ..... 35; 12/$3
F Micro sw. Roller SPNC/10A ..... 59; 12/$5
G CR SPDT A/Bo ..... 98; 6/$5
H Mu & Micro sw. SPDT & reset @ .59; **"TAB" Buy** ..... 12/$5
I Micro Plunger Button SPNT ..... 69; 12/$6
J Micro sw. Cased Hvydty & Arc sup. magnets Plunger SPNO ..... @ .79; 12/$7
K Sw. Switchette DPSO & NC @ .59; 12/$5
K Switchette SPNO ..... @ .49; 15/$5
Start & Stop push button control @ .79
Special Deal ..... @ 12/$7
Kit-B Ass'td Types @ $3.00
Qtys 100 Additional 20% Discount

### TRANSFORMERS



All 115 V 60 Cyc Input TV, & Rec. Xfmrs. Pri 105 to 125 Volts; Hi VOLTS to 20KV (w/quadrupler ckt.) ALL tubes, PL & Picture tube sockets. **SOCKET SAVER.** 300 VDC @ 27; Mo Full-Wave, 6.4V/10.3A,5.4V/8A,2.5V/3A, Hypersil Cores; 6ft PIG **$4.98;** 2 for $8.50. 6 for **$22.00**
2500V/20MA, 6.3V/6A, 2.5V/1.75A, for 10-12 screen Reprint ..... **$7.98**
900V 35MA 2½ 5V 2A, XCLENT ..... Unonly
DUBLR TWO 2X2 FIL WNDGS ..... $1.98
778VCT 200MA, 5V/3A & 6.3VCT/3A $4.98
**770V-250MA**, 2.5V/3A, HVINS HMSLD to choice FILTER PARTS, 4/scope ..... $3.69

### RHEOSTAT BUY

15 Ohm 25W ..... 98c; 12/$7
50 Ohm 25W ..... $1.10; 10/$7
75 Ohm 25W $1.98; 10/$14
125 Ohm 25W ..... $1.10; 10/$7
250 Ohm 25W ..... $1.10; 10/$6
500 Ohm 25W ..... $1.10; 10/$7
1200 Ohm 225W $2.98; 2/$5
5000 Ohm 25W $1.25; 10/$9

### NEW 212W/SEC PHOTOFLASH AC & Dry Battery Kit

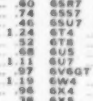
Includes four 525MFD-450V Condensers, Total 212W/sec/de. Resistor, capacitors, rectifiers, flash tube in indicating flash green, guide 280 Daylight Kodachrome, 24A on Ektachrome. Less Batteries.
**"TAB" Special** ..... AC @ $42.98
(5) 90V (N60) Batteries & Box @ $14.98

### FOTOFLASH & STROBE LAMPS

| No. | "TAB" Replaces | W-Sec. Max | Each |
|---|---|---|---|
| TLW | FA 104/FT118 | 150 | $ 5.98 |
| THI | AMGLO 5804X | 100 | 10.98 |
| 225T | GE | 200 | 9.98 |
| THVA | SYLV. 4330 | 200 | 9.98 |
| V4X4 | X400 | 200 | 10.98 |
| TLX | DX & FA10Q | 150 | 9.00 |
| TDX | DXC/250-350 | 150 | 10.00 |
| 353GTQ | FT 503 | 2000 | 49.98 |

Trigger Coil for LO Volt Flash $1.47
Write for "TAB" Flash Vdc Data ..... 80c

### CIRCUIT BREAKERS



Heinmann Magn Bkrs—Amps: 3, 5, 7, 9, 12, 15, 25, 35, 40, 50, @ $1.98 ea.; 12/$20; **"TAB" Special** ..... 50/$75
Su D&CH Toggle Sw Bkrs—Amps: 5, 10, 15, 20, 25 @ 98c ea.
Klixon Therma Push Button Bkrs —Amps: 5, 10, 15, 20, 30, 35—@ 89c ea.; 10/$7.98

• 1st Quality • No Electrical or Mechanical Rejects

# TUBES!!

**"TAB" TESTED & GUARANTEED**
• Individually Boxed • Hickock Mu Tested •
**WE WHOLESALE TO SERVICEMEN, DEALERS & INDUSTRY**

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 0A2 | .74 | 2E5 | .92 | 6B8 | .64 | 6SN7 | .56 | 12BE6 | .62 |
| 0A3 | .98 | 2V3 | 2.90 | 6BA6 | .48 | 6SQ7 | .56 | 12BH7 | .69 |
| 0B2 | .74 | 2X2A | 1.15 | 6BC5 | .60 | 6SR7 | .60 | 12C8 | .62 |
| 0B3 | 1.19 | 4A4 | .97 | 6BD3 | .74 | 6SS7 | .60 | 12CA5 | .48 |
| 0C3 | .88 | 384 | 2.70 | 6BE6 | .46 | 6SU7 | 4.20 | 12J5 | .48 |
| 0D3 | .78 | 3B7 | .56 | 6BQ6 | 1.24 | 6T4 | 1.15 | 12K8 | .48 |
| 0Z4 | .50 | 3C6 | .48 | 6BR8 | .52 | 6T8 | .78 | 12SA7 | .64 |
| 1A5GT | .64 | 3Q5 | .68 | 6BJ6 | .68 | 6U5 | .99 | 12SF7 | .78 |
| 1A7GT | .96 | 3S4 | .49 | 6BK7A | 1.11 | 6U7 | .64 | 12SH7 | .62 |
| 1AB2 | 1.25 | 5U4 | .46 | 6BN6 | .52 | 6V6GT | .56 | 12SJ7 | .54 |
| 1AE4 | 3.75 | 4BZ7 | 1.55 | 6BN6 | 1.19 | 6W4 | .38 | 12SK7 | .48 |
| 1AH4 | 1.07 | 5AX4 | 1.22 | 6BQ6 | .98 | 6X4 | .42 | 12SL7 | .56 |
| 1AX2 | 1.25 | 5AT4 | .58 | 6C4 | .38 | 6X5 | .48 | 12SN7 | .56 |
| 1B3 | .46 | 5R4GYW | 1.50 | 6C5 | .68 | 6Z7 | 2.11 | 12SQ7 | .54 |
| 1C6 | .49 | 5T4 | 1.48 | 6C6 | .56 | 7A4 | .78 | 12SR7 | .48 |
| 1D8GT | .89 | 5U4 | .46 | 6C8 | .82 | 7A5 | .74 | 12Z3 | .89 |
| 1E5 | 1.28 | 5V4 | 1.25 | 6CB6 | .52 | 7A7 | .74 | 14A7 | .92 |
| 1E7 | .49 | 5X4G | .78 | 6CD6 | 1.08 | 7A8 | .68 | 14AF7 | .95 |
| 1G4GT | .60 | 5Y3 | .36 | 6D6 | .84 | 7AD7 | 1.41 | 19BG6 | 1.38 |
| 1G5 | .74 | 5Z3 | .52 | 6E5 | .78 | 7B4 | .81 | 19T8 | 1.19 |
| 1G6GT | .69 | 6A3 | 1.29 | 6E5 | 1.09 | 7B6 | .72 | 19V8 | 1.06 |
| 1H4G | .49 | 6A5 | 2.98 | 6F5 | .91 | 7B8 | .82 | 24A | .92 |
| 1H5GT | .72 | 6A6 | .81 | 6F6 | .76 | 7C4 | .86 | 25A6 | 1.70 |
| 1H6 | .89 | 6A7 | 1.09 | 6F8 | .80 | 7C7 | .68 | 25BQ6 | .99 |
| 1J6G | .79 | 6AB7 | 1.09 | 6G6 | .92 | 7E5 | .54 | 25L6 | .42 |
| 1L4 | .48 | 6AC7 | .42 | 6H6 | .57 | 7E7 | .74 | 25Z5 | .84 |
| 1LA4 | 1.01 | 6AB7 | .78 | 6J4 | 4.59 | 7F7 | .76 | 25Z6 | .80 |
| 1LB4 | 1.09 | 6AC6 | 1.15 | 6J5 | .42 | 7F8 | 1.18 | 26 | .79 |
| 1LC6 | .98 | 6AC7 | .46 | 6J7 | .48 | 7H7 | .72 | 28D7 | 1.29 |
| 1LD5 | .98 | 6AF6 | 1.18 | 6J7 | .72 | 7N7 | .90 | 35 | .59 |
| 1LE3 | .69 | 6AG5 | .50 | 6K6 | .49 | 7S7 | 1.29 | 35/51 | .60 |
| 1LH4 | 1.01 | 6AG7 | 1.14 | 6K7 | .46 | 7V7 | 1.09 | 35A5 | .71 |
| 1LN5 | .78 | 6AH6 | .81 | 6L5 | 1.09 | 7X6 | .64 | 35B5 | .84 |
| 1P5 | .78 | 6AK5 | .62 | 6L6 | .98 | 7Y4 | .64 | 35C5 | .71 |
| 1Q5 | 1.19 | 6AK6 | .74 | 6L7 | .80 | 10 | .49 | 35Y4 | .68 |
| 1R4 | .42 | 6AL5 | .42 | 6N7 | .74 | 12A6 | .79 | 35Z3 | .68 |
| 1R5 | .82 | 6AL7 | 1.22 | 6P5 | .99 | 12A8 | .79 | 35Z4 | .64 |
| 1S4 | .88 | 6AQ5 | .46 | 6Q7 | .81 | 12AH7 | .92 | 35Z5 | .46 |
| 1S5 | .68 | 6AQ6 | .74 | 6R7 | 1.09 | 12AT6 | .54 | 50 | .96 |
| 1T4 | .52 | 6AR6 | 2.74 | 6S4 | .48 | 12AT6 | .42 | 45Z3 | .68 |
| 1T5 | .98 | 6AS6 | 1.75 | 6S7 | 1.30 | 12AT7 | .68 | 49 | 1.19 |
| 1U4 | .46 | 6AS7 | 3.49 | 6S8 | .92 | 12AU6 | .44 | 80AS | .54 |
| 1U5 | .48 | 6AT6 | .42 | 6SA7 | .54 | 12AU7 | .84 | 80C5 | .42 |
| 1V2 | .62 | 6AU6 | .46 | 6SC7 | .74 | 12AV6 | .38 | 80L6 | .60 |
| 1X2A | .62 | 6AV5 | .84 | 6SD7 | .74 | 12AW6 | .84 | 71A | .74 |
| 2A4 | 3.37 | 6AV6 | .46 | 6SG7 | .62 | 12AX7 | .82 | 75 | .64 |
| 2A5 | .76 | 6AX4 | .81 | 6SH7 | .42 | 12AY7 | .68 | 76 | .64 |
| 2A6 | 1.49 | 6B4 | 1.12 | 6SJ7 | .42 | 12BA6 | .52 | 77 | .64 |
| 2A7 | .89 | 6B7 | 1.16 | 6SK7 | .42 | 12BA7 | .84 | 117L7 | 1.24 |
| 2B7 | .89 | 6B7 | .91 | 6SL7 | .56 | 12BD6 | .69 | 117Z3 | .68 |

**THAT'S A BUY "TAB" THAT'S A BUY**

Dept. 9RE5 — 111 LIBERTY STREET, NEW YORK 6, N.Y., U.S.A.

## NEW 6KV HI SENSITIVITY DC & AC 27 Range MULTITESTER

**"TAB" $21.95** Lots of 3
(Not A Kit)

A complete precision test instrument. 20,000 Ohms per Volt DC-10,000 Ohms p/v AC. 38 micro ammere movement, 8 easy to read scales: DC 0-6, 30, 120, 600, 1200, 6000 Volts. AC 0-6, 30, 120, 600, 1200 Volts. Current 0-60 ua, 6, 60, 600 ma. Resistance 0-8K, 80K, 800K, 8 megohms. Decibels Cal 600 ohm —20 to +6, 20, 34, 46, 60 DBS. Capacity 250 mmfd to 10 mfd. Inductance 10 to 1000 millihys. Hi accuracy, Versatile 1% Precision Resistors, Scale 3". Plastic engraved panel. Rugged metal case. Lrth. 4¼" x 6¼" x 2¾". Complete w/batteries & leads. RF Diode Probe included for signal measurement. Sold Singly ..... @ $22.95 ea.
HV 30,000 Volt Probe. Special $5.95 ea.

**Pocket AC-DC MULTITESTER "TAB" 27C**
**$9.45** Lots of 3
Hi-accuracy precision VOM 1000 Ohms per Volt. Reads AC & DC Volts 0, 5, 25, 250, 1000 V. DCMA: 0, 1, 10, 100 MA. Ohms 0, 2K, 100 K. Size 1¼" D, 4⅝" L, 3¼" W. Test Leads
Singly $9.95 (plus 40c ship in U.S.A.)

### NEW "Clip In Tip" GE Cartridges *GE Original Boxed, $ $ $ Back Gtd

| | |
|---|---|
| RPX050A* | .001 & .003 $6.98 |
| RPX052A* | Gold Tress $19.98 |
| RPX053A* | Gold Tress $28.98 |
| RPX040A* | Single (S) .003 $5.25 |
| RPX041A* | Single (S) .001 $5.25 |

★★★★★★★★★★★★★★★★★★★★★★★★

### Repic'ment Needles "TETRAD" Diamond†

| | |
|---|---|
| RPJ010A | Dual (S) .001 & .003 GE ..... $1.98 |
| RPJ012A | Dual (D) .0011&.0031 ..... $18.99 |
| RPJ013A | Dual (DS) .0011&.003 ..... $10.99 |

Repic'mnts for New A Cartridges Only

| | |
|---|---|
| RPJ01D or RPJ03D | Sing (D) Tetrad† $9.99 |
| RPJ015 or RPJ075 | Single (S) $5.15 |

Repic'mnt Styli for RPX040 & 041 Only

| | |
|---|---|
| RPJ001 or RPJ005 | Single (S) GE ..... $1.35 |
| RPJ003 or RPJ004 | Single (D) $9.99 |

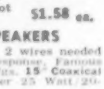
Complete Stock of Repic'mnt Needles
MG or 78 Single Sapphire Styli ..... $1.15
MG and 78 Dual Sapphire $1.98 ..... 4/$7.50
MG or 78 Single Dia. "TETRAD"† ..... $9.89
MG and 78 Dual Dia. "TETRAD"† ..... $20.89

### ALL NEW DUAL VOLTAGE PHONO CARTRIDGE

**$1.55 ea.** LOTS OF 6
Replaces 127 Popular Make & Type Cartridges
95% OF ALL 78 RPM'S
Output of 4½ or 2 volts. A terrific Deal. Singly $1.65 ea.

### HI-FI RECORDING TAPE Finest, $, $, $, Back Gtd

PRECISION COATED & SLIT, Gtd Splice free. Quality Controlled. Plastic Base, Gtd Constant Output, Freq. 7½ IPS 40-15KC Oxide Wnd In 7½" reel; 1200 ft. per reel



Sold Singly **$1.80** Twelve Lot Special **$1.58 ea.**

### HI-FI SPEAKERS



Inbuilt network, 2 wires needed for HF & LF Response. Famous Hi Fi Speaker Mfgs. 15" Coaxial PM & 2½" Tweeter 25 Watt 20-17500 cycles.
MODEL P25CO ..... $19.50
12" Coaxial PM & 2½" Tweeter 12 Watt/45-15000 cy.
Special $12.75; 3 for $35
8" Coaxial PM & 2½" Tw/4w/70-15Kc
MODEL P8CO ..... $7.98; 2 for $15
12" HI-FI PM 10w/35-14KC ..... $10; 2 $18
8" HI-FI PM 7w/45-14KC ..... $7.25; 2 $13

# CBS TUBES

ALL BRAND NEW
IN FACTORY SEALED CARTONS
**50% OFF** ON LOTS OF 1.24
**50% + 10% OFF** On Lots of 25 or More
Same Deal on All CBS Receiving Tubes
Prices Shown are 50% off List

| | | | |
|---|---|---|---|
| 3AL5 | .80 | 5J6 | 1.27 |
| 3AU6 | .87 | 5U8 | 1.37 |
| 3BC5 | 1.00 | 5V6GT | .98 |
| 3BN6 | 1.35 | 5X8 | 1.35 |
| 3CB6 | 1.00 | 6AW8 | 1.55 |
| 4BQ7A | 1.82 | 6SN7GTB | 1.55 |
| 4BZ7 | 1.72 | 12AX4GTA | 1.20 |
| 5AM8 | 1.42 | 12BH7A | 1.27 |
| 5AN8 | 1.42 | 12BY7A | 1.27 |
| 5AT8 | 1.32 | 12CU6 | 1.27 |
| 5AV8 | 1.47 | 12L6GT | .95 |

### Famous Soldering Guns

TA-S-4 Gun 135W ..... $7.80
TA-D-4 100-150w ..... $9.65
TA-D-5 200-275w ..... $10.53
TA-10 Gun 180w ..... $5.83
Lenk Gun (Terrific) ..... $7.45

### Thor Electric Speed Drills

325 ⅜" Electric Speed Drill w/Jacobs chuck. 2400 RPM/115 VAC ..... "TAB" @ $14.95
325¼" Electric Speed Drill w/geared chuck. 1000 RPM 115 VAC ..... Only $23.25

### Chrome Vanadium Speed Drills

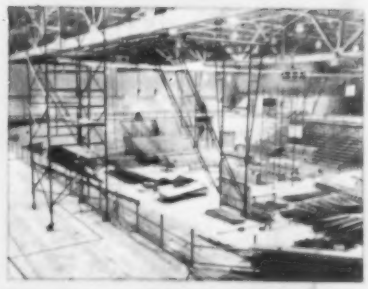
60pc #1 to 60 C.V. ..... $5.95
39pc 1/16" to ½" by 64ths ¼" shank. Wood case $9.95
13pc 1/16" to ¼" with index ..... Special $1.98
8pc Wood Bit Set ¼" shank $1.98

# No dead spots No hot spots

*Partial view of CDP installation at modern Lincoln Fields Race Track, located just south of Chicago at Crete, Illinois*

## OFF AXIS and ON AXIS
**Coverage is Clear, Penetrating, Uniform**

# CDP®
## COMPOUND DIFFRACTION PROJECTOR*



*Electro-Voice CDP Public Address Loudspeaker System was chosen for the 8,248 seat North Side Gym, Elkhart, Indiana, one of the nation's largest high school gyms. Cluster of stacked CDP's can be seen in photo taken during construction.*

**Model 848 CDP.** 25 watts. 16 ohms. Conservatively rated ±5 db from 175 to 10,000 cps. Crossover at 1000 cps. Variable polar patterns. Size: 10½ in. wide, 20½ in. high, 20 in. deep over-all. List Price: $69.50 **Net Price: $41.70**

Outdoors or indoors, everyone can comfortably hear everything when you use the CDP. Listeners off the axis, where the majority of audiences are, do not have to strain to hear, while those on the axis are not assaulted by blasts of sound. The CDP provides smooth peak-free wide-range response, with 120° sound distribution at all frequencies up to 10,000 cps. Unit energy is far more efficient—there's no wasted power. You can do a better job with fewer units at less cost. CDP utilizes two coaxially mounted diffraction horns, working from both sides of a single diaphragm, plus optical slit diffraction for smooth sound dispersion. CDP delivers 2½ octaves more musical range than comparative units. Molded of glass fibers, CDP is weather-proof, blast-proof, splash-proof. Compare the CDP with any other unit in the environment in which it actually will be used—in the field or in an auditorium. Prove to yourself why it is so superior, why it is the best value ever!

*Pat. D169,904 and Pat. Pend.

*Send for CDP Public Address Handbook Bulletin No. 19. Gives complete and helpful information*

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